Durham-Orange Light Rail Transit Project



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Draft



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List of Acronyms and Abbreviations

| Acronym/Abbreviation | Definition |
|----------------------|-------------------------------------------------------------|
| AA | Alternatives Analysis |
| AM | Ante meridian/before noon |
| DEIS | Draft Environmental Impact Statement |
| D-O | Durham-Orange |
| D-O LRT | Durham-Orange Light Rail Transit |
| DTCC | Durham Technical Community College |
| EB | Eastbound |
| FHWA | Federal Highway Administration |
| I-40 | Interstate 40 |
| INRIX | A mobile computer application that pertains to road traffic |
| LOS | Level of Service |
| LPA | Locally Preferred Alternative |
| LRT | Light Rail Transit |
| MOE | Measures of Effectiveness |
| NB | Northbound |
| NC | North Carolina |
| NCCU | North Carolina Central University |
| NCDOT | North Carolina Department of Transportation |
| NCRR | North Carolina Railroad |
| NHC | New Hope Creek |
| PM | Post meridian/after noon |
| ROMF | Rail Operations Maintenance Facility |
| SB | Southbound |
| TRM | Triangle Transit Regional Demand Model |
| TSM | Transportation System Management |
| UNC | University of North Carolina |
| US | United States |
| VA | Veteran Affairs |
| WB | Westbound |



1. Executive Summary

The primary study area in this Downtown Durham Traffic Simulation Report is a corridor, approximately 3.2 miles long that runs along Pettigrew Street within Durham city limits from Erwin Road in the northwest through Alston Avenue in the southeast. It also includes intersections on Main Street and Duke Street. A secondary study area analyzed additional intersections to the north and south of Pettigrew Street between E Chapel Hill Street and Dillard Street to determine the traffic impacts associated with closing westbound Pettigrew Street to general traffic.

Traffic analysis was conducted using Synchro and Vissim. The following scenarios were analyzed in this report:

- Existing Conditions
- 2040 No-Build Conditions
- Build LRT Conditions with at-grade alignment at Swift Avenue (Option 1)
- Build LRT Conditions with aerial alignment at Swift Avenue (Option 2)
 [It should be noted that of the Build Conditions scenarios evaluated in this report, only Option 2 was carried forward for study in the DEIS]

Under the Build Conditions, right-of-way constraints would require that Pettigrew Street be converted from two-way operation today to one-way eastbound operation between E Chapel Hill Street and Dillard Street, where the LRT would run along the north side of Pettigrew Street east of Chapel Hill Street. The 2040 Build LRT Option 1 requires the closure of Pettigrew Street between Case Street and east of Swift Avenue due to the limited right-of-way in this section. Build LRT Option 2 elevates the LRT at Swift Avenue and keeps Pettigrew Street open with operations similar to No-Build Conditions.

The overall intersection results of the No-Build versus Build Vissim analysis are shown in Table ES-2 below. During the analysis, roadway modifications to improve traffic operations were incorporated into the LRT Options analysis models in order to mitigate impacts in accordance with the NCDOT and City of Durham criteria. The modifications proposed as part of the LRT Options are presented in Table ES-1. The overall intersection results of the No-Build versus Build Vissim analysis are shown in Table ES-2. The Build analysis results include the modifications presented in Table ES-1.

Under the 2040 LRT At-Grade Swift Avenue Option 1, traffic impacts were observed in the area bounded by Main Street, Pettigrew Street, 9th Street and Broad Street. As this subarea is composed of short blocks arranged in a grid network that would already experience significant congestion under No-Build Conditions, several movements would be impacted significantly in Option 1. These traffic impacts are due to the at-grade crossing of the LRT at Broad Street/Swift Avenue which causes additional delays to the north/south running streets. In addition, the closure of Pettigrew Street between Case Street and east of Swift Avenue requires traffic to be rerouted to these already congested roadways to reach their destinations. In Option 2, when the LRT is elevated and Pettigrew Street is open between Case Street and east of Swift Avenue, most of these impacts would be removed. At Main Street and Broad Street under Option 2, the northbound Broad Street left turn would experience a degradation of LOS from D to E due to network signal timing changes aimed at improving the major east/west approaches.



In the downtown area east of Swift Avenue for both Build Options, all intersections would operate in accordance with applicable level of service thresholds with the exception of the following locations:

- Mangum Street and Main Street would experience an overall LOS degradation in the PM peak hour by worsening from LOS D to E.
- Pettigrew Street & Fayetteville Street would meet the overall delay/LOS intersection criteria, however, two movements would experience degradation of LOS in the PM peak hour with the southbound Pettigrew Street left and through movements both worsening from LOS C to E.
- Chapel Hill Street & Willard Street, which is an unsignalized intersection, would meet the overall/delay LOS intersection criteria; however, the stop-controlled Willard Street approach would degrade from LOS E to LOS F in the PM peak hour.

All three intersections would experience LOS impacts due to LRV signal preemption events and the network signal timing changes aimed at providing better east/west progression for the LRT. Mangum Street and Main Street is expected to operate at a high LOS D in the No-Build PM peak hour, and with preemption events the overall delay increases to LOS E. If the loss of on-street parking along Mangum Street is deemed acceptable by the City, a third southbound Mangum Street travel lane could be tested during the Engineering phase of the project to determine if traffic impacts would be mitigated at Mangum Street and Main Street.

The LOS movement impacts at Pettigrew Street and Fayetteville cannot be practically mitigated with roadway modifications due to right-of-way constraints and the location of the NCRR corridor that crosses the southbound approach upstream of the stop bar.

Due to preemption events, there are fewer acceptable gaps for vehicles on the stop-controlled Willard Street approach at Chapel Hill Street. The signalization of Willard Street and Chapel Hill Street was discussed with the City of Durham. However, due to the proximity of signals along Chapel Hill Street at Duke Street and Pettigrew Street, the city requested that the intersection remain stop-controlled.

Maximum queues would exceed available storage in several locations; however this is an infrequent occurrence and additional roadway modifications are not recommended at these locations due to the limited operational benefits that would require large capital expenditures via impractical right-of-way acquisitions and the reconstruction of bridges. Many of the turn bay maximum queues would also be contained within their overall approaches' storage space and therefore would not impact upstream intersections.

The expected average queues would be accommodated by the available storage at all locations except the southbound approach of Main Street at Mangum Street. As noted previously, the addition of a third southbound travel lane can be studied during Engineering if the City of Durham were to allow the existing parking lane to be rededicated as a travel lane.



Table ES-1: LRT Options Geometric Mitigations

| Downtown Durham Segment | | | | |
|----------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|--|
| Pettigrew Street at Swift Avenue | Pettigrew is closed between Case St and Swift Ave (Opt 1 only) | | | |
| Pettigrew Street at Chapel Hill Street | Remove westbound Pettigrew St general traffic lanes | | | |
| Pettigrew Street at Blackwell Street | Remove westbound Pettigrew St general traffic lanes Remove dedicated eastbound Pettigrew St left turn bay to provide a single left/through/right lane | | | |
| Pettigrew Street at Mangum Street | Remove westbound Pettigrew St general traffic lanes Restripe southbound Mangum St right turn lane to a through lane Add dedicated eastbound Pettigrew St right turn lane | | | |
| Pettigrew Street at Dillard Street | Eliminate dedicated northbound Dillard St left turn lane Restripe westbound Pettigrew St lane to prohibit through traffic to provide a left/right only lane Restripe southbound Dillard St left/through lane to a through lane | | | |
| Pettigrew Street at Roxboro Street | Remove westbound Pettigrew St general traffic lanes Add dedicated eastbound Pettigrew St left turn lane Restripe northbound Roxboro St left/through to a through lane | | | |



Table ES-2: VISSIM Overall Intersection Analysis Summary – 2040 LRT Options vs 2040 No-Build

| la base a state | No-l | Build | Opti | Option 1 | | Option 2 | |
|--------------------------------------------------------|------|-------|------|----------|----|----------|--|
| Intersection | AM | PM | AM | PM | AM | PM | |
| Main Street at 9th Street | С | D | С | Е | С | С | |
| Main Street at Iredell Street (Unsignalized) | А | D | А | С | А | С | |
| Main Street at Broad Street | С | D | D | Е | С | D | |
| Pettigrew Street at 9th Street (Unsignalized) | В | F | А | F | В | F | |
| Pettigrew Street at Swift Avenue (Unsignalized) | D | F | F | E | В | F | |
| Main Street at Buchanan Boulevard | D | D | D | D | D | D | |
| Maxwell Street at Buchanan Boulevard (Unsignalized) | А | F | А | F | Α | F | |
| Duke Street at Main Street | С | С | В | С | В | С | |
| Duke Street at Peabody Street (Unsignalized) | Α | А | Α | А | Α | А | |
| Memorial Street at Duke Street (Unsignalized) | А | А | А | А | А | А | |
| Chapel Hill Street at Duke Street | С | С | С | С | С | С | |
| Chapel Hill Street at Willard Street (Unsignalized) | Α | А | С | D | В | D | |
| Pettigrew Street at Chapel Hill Street | Α | В | В | С | В | С | |
| Blackwell Street at Pettigrew Street | В | В | В | В | В | В | |
| Blackwell Street at Ramseur Street | В | В | В | В | В | В | |
| Main Street at Corcoran Street | В | В | В | В | В | С | |
| Mangum Street at Main Street | С | D | D | Е | D | Е | |
| Mangum Street at Ramseur Street | В | С | С | С | С | С | |
| Mangum Street at Pettigrew Street | В | В | Α | Α | Α | Α | |
| Roxboro Street at Pettigrew Street | В | В | В | С | В | В | |
| Pettigrew Street at Dillard Street | В | В | В | С | В | С | |
| Fayetteville Street at Pettigrew Street | С | С | С | D | С | D | |
| Fayetteville Street at Jackie Robinson Drive | В | В | В | С | В | С | |
| Morehead Avenue at Fayetteville Street | А | Α | А | А | А | А | |
| Pettigrew Street at Grant Street | В | В | В | В | В | В | |
| Gann Street at Pettigrew Street (Unsignalized) | А | А | А | А | А | А | |
| Alston Avenue at Gann Street | С | В | С | В | С | В | |

Indicates traffic Impact

Indicates traffic Impact Below Mid-D



2. Introduction

Through the Alternatives Analysis (AA) process completed in April 2012 prior to preliminary design, which included extensive public outreach, a Locally Preferred Alternative (LPA) was selected to address the purpose and need of the Durham-Orange (D-O) Corridor. The proposed project is a 17.1 mile double-track light rail transit (LRT) line with 17 proposed stations that will greatly expand transit service in Durham and Orange Counties. The Durham-Orange Light Rail Transit (D-O LRT) project extends from its western terminus at the University of North Carolina at Chapel Hill (UNC) at the UNC Hospitals Station to the eastern terminus in Durham at the Alston Avenue Station. The proposed D-O LRT Project improves public transportation access to a range of educational, medical, employment, and other important activity centers, in the D-O Corridor including: UNC; UNC Hospitals; the William and Ida Friday Center for Continuing Education; Duke University; Durham Veterans Affairs (VA) Medical Center and Duke University Medical Center (DUMC); downtown and east Durham.

2.1 Description of the Proposed D-O LRT

The proposed D-O LRT alignment generally follows North Carolina (NC) Highway 54 (NC 54), Interstate 40 (I-40), United States (US) 15-501, and parallel to North Carolina Railroad (NCRR) Corridor in downtown Durham and east Durham. The proposed alignment begins in Chapel Hill at UNC Hospitals, parallels Fordham Boulevard, proceeds eastward adjacent to NC 54, travels north along I-40, parallels US 15-501 before it turns east towards Duke University and runs within Erwin Road, and then follows the NCRR Corridor that parallels NC Highway 147 (NC 147) through downtown Durham, before reaching its eastern terminus in Durham near Alston Avenue. A total of 17 stations are planned, and up to 3,900 parking spaces along the D-O LRT alignment will be provided. In addition, a rail operations maintenance facility (ROMF) will be constructed to accommodate the D-O LRT fleet (12 cars, including spares).

2.2 Proposed Project Alternatives

Consistent with the September 2012 Scoping Report, and as described herein, the Draft Environmental Impact Statement (DEIS) will examine the potential environmental impacts of the LRT alternative as well as a small number of alignment, station, and ROMF siting options, including the following:

- Crossing of Little Creek between the Friday Center and the proposed Leigh Village Development (i.e., Alternatives C1, C1A, C2, C2A and associated station location)
- Crossing of New Hope Creek (NHC) and Sandy Creek between Patterson Place and South Square (i.e., NHC Alternatives 1 and 2 and associated station locations)
- Station options at Duke and Durham VA Medical Centers
- Five proposed locations for the ROMF

2.3 Purpose of Downtown Durham Traffic Simulation Report

The roadway network is one of the most critical elements of the transportation network, serving as a means to safely move people and goods and to support the economic development of an area. In an effort to balance safety and mobility with economic development and access, many owners of public roads have developed standards for determining the impacts of development on the roadway network



and the level to which those impacts must be mitigated. The standards and mitigation levels governing projects in Durham and Orange Counties of North Carolina have been identified in the *Traffic Methodology Report*.

The purpose of this technical memorandum is to analyze the traffic operations for the Downtown Durham section of the proposed D-O LRT in light of the policies identified in the *Traffic Methodology Report*. The proposed D-O LRT project would integrate the LRT along Pettigrew Street generally.

The goal of the study is to provide decision makers with an evaluation of the ability of the transportation system to accommodate the future travel demand and to help determine which improvements are necessary to accommodate that demand. As noted previously, improvements to the roadway network will be included in this evaluation to determine if reasonable improvements can be made to accommodate the forecasted traffic volumes for 2040 in accordance with the guiding policies. This study will also aim to determine which projects are necessary to accommodate the background growth in traffic and which are necessary to mitigate any additional impacts caused by the proposed D-O LRT project.

2.4 Downtown Durham Traffic Simulation Description

This report describes the approach and summarizes the findings and results of the traffic analysis conducted on the section of the D-O LRT alignment in Downtown Durham.

Preliminary designs were developed for the proposed downtown D-O LRT alignment and are included in the *Basis for Engineering Design* (Appendix D). The design converts Pettigrew Street to one-way eastbound only operation between E Chapel Hill Street and Dillard Street with the LRT running along the north side of the Pettigrew Street east of Chapel Hill Street. Five LRT stations are proposed for implementation along this section of the project. The westernmost of the five is elevated and located west of 9th Street and Pettigrew Street. The second of the LRT stations is located east of Buchanan Boulevard between Maxwell Avenue and NC 147. The third is located at the intersection with Pettigrew Street and E Chapel Hill Street. The fourth station is located along Pettigrew Street between Dillard Street and Fayetteville Street, and the easternmost of the five is located on the western side of Pettigrew Street's intersection with Alston Avenue. In the analysis, these five stations are referred to as the Ninth Street Station, Buchanan Boulevard station, Durham Station, Dillard Street Station, and Alston Avenue Station respectively.

The implementation of the proposed D-O LRT along the Pettigrew Street corridor would require the reconstruction of the roadway from Chapel Hill Street to Alston Avenue. Please see Section 3 for a discussion of the Build Options and refer to Appendix D for the preliminary design drawings.

To analyze the potential impacts brought by the LRT, Vissim micro-simulation models were developed to cover the area of the LRT corridor and the nearby intersections. The models aim to capture the direct impact of the LRT operation to the roadway system during both the 2040 weekday AM and PM peak hours. The LRT is assumed to operate with 10 minute peak period frequencies in the eastbound and westbound directions. Every train is assumed to have 20 seconds of dwell time at each station for passenger boarding and alighting.

The following Primary Study Area intersections were analyzed in the Vissim models and are also shown in Figure 1:



- Main Street and 9th Street (signalized)
- Main Street at Iredell Street (unsignalized)
- Main Street and Broad Street (signalized)
- Pettigrew Street and 9th Street/Erwin Road (unsignalized)
- Pettigrew Street and Swift Avenue/Broad Street (unsignalized)
- Main Street and Buchanan Boulevard (signalized)
- Maxwell Street and Buchanan Boulevard (unsignalized)
- Duke Street and Main Street (signalized)
- Duke Street and Peabody Street (unsignalized)
- Duke Street and Memorial Street (unsignalized)
- Duke Street and Chapel Hill Street (signalized)
- Chapel Hill Street and Willard Street (unsignalized)
- Chapel Hill Street and Pettigrew Street (signalized)
- Main Street and Corcoran Street (signalized)
- Ramseur Street and Blackwell Street (signalized)
- Pettigrew Street and Blackwell Street (signalized)
- Main Street and Mangum Street (signalized)
- Ramseur Street and Mangum Street (signalized)
- Pettigrew Street and Mangum Street (signalized)
- Pettigrew Street and Roxboro Street (signalized)
- Pettigrew Street and Dillard Street (signalized)
- Pettigrew Street and Fayetteville Street (signalized)
- Jackie Robinson Drive and Fayetteville Street (signalized)
- Morehead Avenue and Fayetteville Street (signalized)
- Pettigrew Street and Grant Street (signalized)
- Pettigrew Street and Gann Street (unsignalized)
- Alston Avenue and Gann Street (signalized)

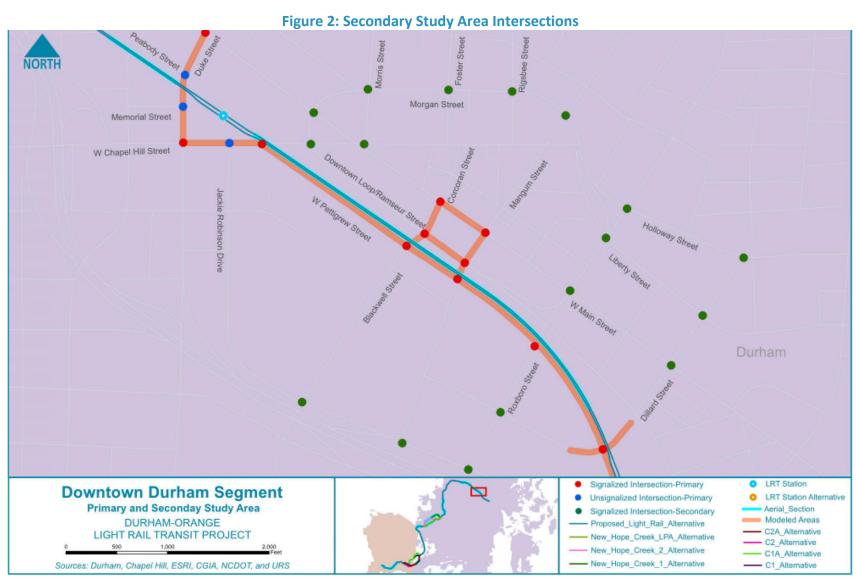
As Pettigrew Street would be converted to one-way eastbound vehicular operation between Chapel Hill Street and Dillard Street to accommodate the LRT, westbound general traffic must find alternate routes to complete their trips. Public transit buses will be permitted to travel in the westbound LRT transit lane from Dillard Street in the east to the Durham Station Transit Center Driveway in the west. The potential impacts caused by the detoured traffic were identified in a regional demand model, and then Synchro models were developed to analyze the potential impacts brought by the detoured traffic outside the primary LRT corridor study area. This secondary study area Synchro network covers the area from Holloway Street/Morgan Street in the north to Jackie Robinson Drive in the south, Duke Street in the west and Dillard Street in the east. The secondary study area intersections are shown in Figure 2.



W Chapel Hill Street LRT Station **Downtown Durham Segment** Unsignalized Intersection LRT Station Alternative Aerial Section Modeled Areas DURHAM-ORANGE - Proposed_Light_Rail_Alternative C2A_Alternative LIGHT RAIL TRANSIT PROJECT New_Hope_Creek_LPA_Alternative C2_Alternative New_Hope_Creek_2_Alternative - C1A Alternative New_Hope_Creek_1_Alternative - C1_Alternative Sources: Durham, Chapel Hill, ESRI, CGIA, NCDOT, and URS

Figure 1: Primary Study Area Intersections







3. Description of Scenarios

Four scenarios were analyzed for this study. Those scenarios included an Existing Conditions scenario that was also used for model calibration, a Future Year 2040 No-Build Alternative, and two options for the Future Year 2040 Build condition.

A brief description of the scenarios evaluated in the Vissim microscopic traffic simulation software follows.

3.1 2011 Base Year Scenario

The 2011 Base Year Scenario simulated traffic conditions as they existed in 2011. The goal of the 2011 Base Year Scenario was to develop a calibrated model that would serve as the basis for the creation of the models for future year No-Build and Build scenarios. As discussed in the *Traffic Methodology Report*, travel time and speed were calibrated.

3.2 2040 No-Build Alternative

This alternative determined what the traffic operations would be in the vicinity of the proposed D-O LRT project if the proposed project is not constructed. The No-Build Scenario assumed the local transportation system would evolve as currently planned, but without implementation of the proposed project and associated improvements. As part of the No-Build improvements, it was assumed the NCRR tracks would be grade-separated between Blackwell Street and Mangum Street. The Vissim models do not include NCRR rail traffic due to their rare occurrences during the AM and PM peak hours and therefore the status of the NCRR grade-separation project would not affect this analysis.

3.3 2040 Build Alternative— One-Way Eastbound Pettigrew Street

The 2040 Build Alternative determined what the traffic operations would be in the vicinity of the proposed project if the light rail is constructed and the stations are constructed in downtown Durham.

The Build analysis was based on a preliminary design as well as the currently planned improvements within the study area. Please refer to the Appendix D for the Preliminary Design drawings for Option 1 and Option 2.

Under both options, Pettigrew would be converted to one-way eastbound between Chapel Hill Street and Dillard Street, and the LRT runs along the north side of Pettigrew Street east of Chapel Hill Street.

The 2040 Build Option 1 would close Pettigrew Street between Case Street and east of Swift Avenue to provide exclusive right-of-way for the LRT to cross Swift Avenue at-grade.

The 2040 Build Option 2 elevates LRT at Swift Avenue and keeps Pettigrew Street open from Case Street to east of Swift Avenue.

In terms of the LRT's signal operation, for the purpose of this analysis it was assumed that traffic signals along Pettigrew Street will be programmed to operate with traffic signal pre-emption. Traffic signal pre-emption takes place when traffic signal timing is interrupted to allow trains to remain on schedule. In the case of Downtown Durham, it is assumed the normal traffic signal timing is altered to allow the train to proceed uninhibited. While the train is in the intersection, all conflicting movements must stop



although traffic traveling parallel to the tracks can proceed with the train. Any difference in signal phase length as a result of the passing train is made up within one traffic signal cycle after the train passes.



4. Methodology

The use of microscopic traffic simulation was completed using Vissim (version 5.4). Vissim is a microscopic, behavior-based multi-purpose traffic simulation program that evaluates each vehicle individually every model time step and then assigns the appropriate behavior logic according to the traffic operations that the specific vehicle encounters. For many engineering disciplines, simulation has become an indispensable instrument for the optimization of complex technical systems. This is also true for transportation planning and traffic engineering, where simulation is an invaluable and cost-reducing tool. The microscopic simulation model was developed for the studied section of the project and was based on a calibrated base model for the area.

The methodology for microscopic simulation begins with a base model developed from data collected for the transportation network. The base model is then calibrated against data measured in the field to arrive at a calibrated base model. Once the base model is calibrated, future year alternatives can be developed and analyzed for impact study. As in real-life operations, microscopic simulation models are constrained to the capacity of a given roadway, and as such the model can only load traffic up to the capacity of a facility, with excess vehicles being denied entry and queue up outside the model network. This can happen for future scenarios when demand has been forecasted to outgrow the capacity of the existing roadways.

4.1 Measures of Effectiveness

Measures of effectiveness (MOE) are system performance statistics that best characterize the degree to which a particular alternative meets the project objectives. The MOEs for microscopic simulation can be abundant due to the nature of the analysis. The primary MOEs for urban arterials are typically average speed and vehicle density for individual segments as well as average travel time and speed for individual origin-destination pairs within the network. On an overall network level, MOEs such as average system speed, average system delay, and number of stops can provide overall indications of the operations of a network.

As discussed in the *Traffic Methodology Report*, corridor-level MOEs including average speed and travel time were used as the method for calibrating the base year model. Control delay, which is utilized to determine intersection LOS, and queuing were the MOEs for the future year models. The concept of Highway Capacity Manual's Level of Service was adopted here for the purpose of simply categorizing the delays. Please note that the calculation methods of HCM delay and VISSIM delay are different, as Vissim delay includes control delay as well as queue delay, whereas, HCM includes control delay only, The LOS grades are based on Vissim delays, which will provide a more conservative result than the HCM-based delays.

The acceptable levels for the future year MOEs were enumerated in the *Traffic Methodology Report*. Additional information regarding the base year MOEs can be found in Section 6.1. Both NCDOT and City of Durham have established guidelines that specify when chosen MOEs meet the required thresholds. The NCDOT's "Policy on Street and Driveway Access to North Carolina Highways" states that when comparing base network conditions to project conditions, mitigation improvements to the roadway network are required if at least one of the following conditions exist:



- The total average delay at an intersection or an individual approach increases by 25% or greater, while maintaining the same Level of Service
- The Level of Service degrades by at least one level
- Or Level of Service is F
- For turning lanes, mitigation improvements shall be identified when the analysis indicates that the 95th percentile queue exceeds the storage capacity of the existing lane.

For the purposes of this analysis, traffic impacts were considered significant if the Build Alternative delay was at or above a middle LOS D or 45.0 seconds or greater for a signalized intersection. Those overall intersections or movements that reported delays greater than 45.0 seconds and experienced an LOS degradation or increase in delay greater than 25% compared to the No-Build were highlighted in the Vissim LOS tables with orange. For those intersections or movements that reported a Build LOS better than middle D or less than 45.0 seconds, the impacts were not considered as significant and were highlighted with yellow.

To be considered a queue impact, the maximum queue length for any Build movement would exceed both the respective No-Build movement's maximum queue length and the build movement storage length by 10 feet.

Table 1: City of Durham Traffic Level of Service Standards

| Application | Level of Service Standard |
|---------------------------|---------------------------|
| Downtown Tier | LOS E |
| Compact Neighborhood Tier | LOS E |
| Urban Tier | LOS D |
| Suburban Tier | LOS D |
| Rural Tier | LOS C |

For the Downtown Durham segment, those intersections under the jurisdiction of the City of Durham utilized the "Downtown Tier" criteria for MOE evaluation and traffic impact analysis.

4.2 Vissim Network Development

4.2.1 Geometry

The basis for developing the geometric data was a combination of aerial photographs and contour maps. Aerial photography was used as a background to digitize the network into the simulation model. The three-dimensional attributes and grades were determined based on a contour map of the study area.

The geometry in the 2011 Base Year network and the 2040 No-Build network are based on the current geometry of Downtown Durham. The network was created using aerials from NC OneMap, Google Maps, field verification, and contour maps from the North Carolina Department of Transportation (NCDOT).



4.2.2 Traffic Control

Signal timing and coordination plans were obtained from City of Durham for the nineteen signals included in the study area. These plans were used to input timing, phasing, and detectors for the following intersections in the base year:

- Main Street at 9th Street
- Main Street at Broad Street
- Main Street at Buchanan Boulevard
- Duke Street at Main Street
- Duke Street at E Chapel Hill Street
- E Chapel Hill Street at Pettigrew Street
- Blackwell Street/Corcoran Street at Pettigrew Street
- Mangum Street at Pettigrew Street
- Roxboro Street at Pettigrew Street
- Dillard Street at Pettigrew Street
- Grant Street at Pettigrew Street
- Alston Street at Gann Street
- Blackwell Street/Corcoran Street at Downtown Loop/Ramseur Street
- Mangum Street at Downtown Loop/Ramseur Street
- Corcoran Street at Main Street
- Mangum Street at Main Street
- Fayetteville Street at Pettigrew Street
- Fayetteville Street at Jackie Robinson Drive
- Fayetteville Street at Morehead Avenue

The signalized intersections for the future year networks were input into Synchro for signal optimization prior to being input into Vissim. The future year signalized intersections included the previously listed intersections. The future year signal timings were composed from the base year timing, and then reoptimized based on the 2040 traffic volumes.



4.2.3 Speed Data

The average speed data in the area were collected using the floating car technique during off-peak periods with low volumes. This data was used to develop desired speed distributions for the network. Weekday peak periods speed data was collected from INRIX (a mobile application pertaining to road traffic). This data was used to determine the average speed during the peak periods from the approximate time the initial count data was collected. This data was used in calibration of the model. The desired speed distribution for turning vehicles at intersections was assumed to be 12.6 mph with a standard deviation of 1.2 mph for right turns and 21 mph with a standard deviation of 2 mph for left turns. There were two main speed distributions used for roadways: 1) 25 mph posted, with a range of 19 to 31 mph in Vissim, and 2) 35 mph posted with a range of 32 to 48 mph.

4.2.4 Driving Behavior Parameters

The driving behavior parameters were used to guide vehicles through the network during the simulation models. Both the car-following and lane-change models in Vissim use an extensive range of parameters. Some of these may be adapted by the user to change basic driving behavior. Vissim uses five driving behavior models, of which only one was used in the base model: Urban (motorized). The Urban (motorized) parameters were used to model the surface streets within the network and were based on the Wiedemann 74 model. The Wiedemann 74 model includes three parameters which can be calibrated based on the data collected. Default values were used in developing the base model and any modifications made to the parameters were documented in the calibration section of this report.

4.2.5 Estimated Traffic Volumes

Simulation models are capable of using unbalanced input volumes and their own internal algorithms to balance the network; however using this method of traffic volume input can produce inaccuracies in actual processed volumes at particular locations. To accurately model the network, the volumes were developed into a balanced network. The traffic volumes for the proposed project were based on peak hour count data that was balanced along Pettigrew Street by adjusting through volumes and adding sink and source nodes to correspond to mid-block locations that could serve as origins and destinations of traffic. These locations included parking lots for commercial establishments as well as parking areas for residential development along the corridor.

Volumes for the 2011 Existing Condition were developed based on the 2011 count data. The projection of the future volumes for no-build and build conditions were based on Triangle Regional Travel Demand Model (TRM) v5 as outlined in the *Traffic Methodology Report*.

Due to the introduction of the LRT, including park & ride lots and a modal demand shift from personal vehicles to public transit, the 2040 No-Build and Build volumes were based on separate TRM roadway growth rates. Separate future 2040 Build balanced volumes were developed for Build Option 1 and Build Option 2 in the vicinity of Pettigrew Street and Main Street between Erwin Road/9th Street and Broad Street/Swift Avenue due to the closure of Pettigrew Street between Case Street and east of Swift Avenue under LRT Option 1. Due to the localized closure of Pettigrew Street, the east/west volumes were rerouted to Main Street via Erwin Street/9th Street and Broad Street/Swift Avenue.

Both LRT Option 1 and Option 2 assumed that westbound Pettigrew Street would be closed to general traffic between Chapel Hill Street and Dillard Street, which would require vehicles to find alternative



paths to complete their westbound trips. As a result, Build volumes would increase on Main Street, Holloway Street/Morgan Street, and to a lesser extent Jackie Robinson Drive. Similarly, the north/south running roadways including Roxboro Street and Dillard Street that connect to the alternate westbound roadways are expected to accommodate additional Build volumes compared to No-Build Conditions.

The balanced AM and PM peak hour volumes for the 2011 Existing, 2040 No-Build, 2040 LRT Option 1, and 2040 LRT Option 2 scenarios are shown in Appendix A.

4.2.6 Simulation Settings and Repetitions

Each simulation was run for one hour with 15 minutes of seeding time for the network to load. The number of simulation runs was based on the process described in Appendix B of the Federal Highway Administration (FHWA) Traffic Analysis Toolbox. The average speed of each simulation run was used as a basis for determining the number of required repetitions, with a confidence level of 95% and a confidence interval of 5 mph. It was calculated that each alternative/option would need to be run with 16 repetitions each for both the AM and PM peak periods.

4.2.7 Output

The output data was extracted from the model using the Travel Time evaluation, Data Collection, and the Analyzer Reports modules. The Travel Time evaluation provided average travel times for user defined start and end points within the network. The Analyzer Report module provided delay data which was utilized to determine the LOS. The Analyzer Report module provides queuing information as well.

4.2.8 Base Year Calibration

The base year model was calibrated by comparing modeled travel times versus historic INRIX speed data as described in the *Traffic Analysis Methodology Report*. Historic data was extracted for Pettigrew Street within the study area for AM and PM peak one hour periods during all weekdays for the month of May in 2011. The average speed and corresponding travel time for each direction along Pettigrew Street was determined from the data. It should be noted that INRIX speed data is composed of link-based speeds (as opposed to spot speeds taken at a fixed point); therefore, the model network was developed to match the same extents as the INRIX speed data. For this study this included the Pettigrew Street segments between Chapel Hill Street and Alston Avenue for both directions during the AM and PM peak hours.

For the calibration effort, the average travel time was determined by averaging a statistically adequate number of model runs (see Section 6.1). Speed calibration targets of ±2.5 mph (desirable) and ±5 mph (acceptable) were set as described in the *Traffic Analysis Methodology Report*.



5. Synchro Network Development

In addition to the Vissim analysis addressing the direct impact along the LRT corridor, as Pettigrew Street is converted to one-way eastbound operation for general traffic between Chapel Hill Street and Dillard Street, the potential impacts brought by the detoured traffic outside the LRT corridor were analyzed in Synchro models by comparing the Build scenario to No-Build scenario. The Synchro model was developed for three future scenarios – 2040 No-Build and the two 2040 Build Options. This secondary Synchro network covers an area from Holloway Street/Morgan Street in the north to Jackie Robinson Drive in the south, Duke Street in the west and Dillard Street in the east. As a result, the following intersections were analyzed in Synchro:

- Downtown Loop at Chapel Hill Street
- Great Jones Street at W Main Street
- Great Jones Street at Morris Street
- E Chapel Hill Street/Main Street at Morris Street
- Morgan Street at Foster Street
- Blackwell Street at Jackie Robinson Drive
- Morgan Street at Rigsbee Avenue
- Morgan Street at Mangum Street
- Mangum Street at Jackie Robinson Drive
- Holloway Street at Roxboro Street
- Liberty Loop at Roxboro Street
- Main Street at Roxboro Street
- Dillard Street at Roxboro Street
- Jackie Robinson Drive at Roxboro Street
- Dillard Street at Holloway Street
- Dillard Street at Liberty Street
- Dillard Street at Main Street

5.1 Estimated Traffic Volumes

The field peak hour traffic counts for the intersections above were obtained from City of Durham. The counts year ranges from 2007 to 2010. First these counts were aligned to the year of 2011 by applying aggregated growth factors derived from the regional demand model. The traffic volumes were then balanced by adjusting through volumes and adding sink and source nodes to correspond to mid-block locations that could serve as origins and destinations of traffic.

The projection of the future volumes for no-build and build conditions was based on the Triangle Regional Travel Demand Model (TRM) v5. Link growth rates derived from the TRM were applied to the existing



balanced volumes to provide realistic traffic patterns in the future conditions. The resulting future scenarios' balanced volumes were adjusted to provide feasible Volume-to-Capacity ratios in an effort to avoid supersaturated roadways.

5.2 Traffic Control

The existing signal and coordination plans were obtained by Synchro models provided by City of Durham. The future year signal timings were composed from the base year timing, and then re-optimized based on the projected 2040 traffic volumes for the No-Build and Build alternatives. To accommodate the multi-modal users of the Downtown Durham area and minimize pedestrian waiting times, future signal cycle lengths were limited to a maximum of 120 seconds at locations not directly impacted by the LRT. Maximum cycle lengths of 140 seconds were proposed at intersections directly impacted by LRT crossings to accommodate the green time lost to preemption events.



6. Simulation Results

Based on the above model network elements and the methodologies defined under MOEs, the results from Vissim and Synchro can be determined.

6.1 2011 Existing Conditions

The 2011 Existing Conditions Vissim model was developed and calibrated, as described in Section 4.2.89 above. The INRIX speed data, taken from a 1.3 mile corridor along Pettigrew Street showed the following average speeds and corresponding travel times. The results of the calibrated base model are shown in Table 2 below.

Based on the data included in Table 2 and the calibration criteria of \pm 5 mph with a desired target range of \pm 2.5 mph, the base model is considered to be calibrated and can be utilized as the basis for developing the future year alternatives/options. All four travel time values fell within the acceptable range. In general, the speeds in the model were lower than those from the INRIX data.

Table 2: 2011 Existing Conditions - Calibrated Base Model Summary

| | | | Calibrate | ed Model | INF | RIX | | Speed Difference (MPH) | Calibration Range | |
|----------------|--------|----------------|------------------------------------|---------------------------|---------------------------------|---------------------------|------------------------------------|------------------------------|----------------------|-------|
| Direction | Length | Peak Period | Average Travel Time (min) | Average Speed (MPH) | Average Travel Time (min) | Average Speed (MPH) | Travel Time Difference (min) | | | |
| | | | | Eastbo | und Travel Tir | ne Summary | | | | |
| EB Corridor | 1.31 | AM | 3.99 | 19.69 | 3.73 | 21.78 | 0.26 | -2.09 | Within Desirable | |
| Wide | | 1.51 | 1.51 | PM | 3.99 | 19.69 | 3.67 | 22.18 | 0.32 | -2.49 |
| | | | | Westbo | ound Travel Ti | me Summary | | | | |
| WB Corridor | 1.16 | AM | 3.60 | 19.36 | 3.22 | 22.45 | 0.38 | -3.08 | Within Acceptable | |
| Wide | 1.10 | PM | 3.82 | 18.22 | 3.27 | 22.10 | 0.55 | -3.89 | Within Acceptable | |



6.2 2040 No-Build Alternative

The 2040 No-Build Alternative model was developed based on the calibrated Existing Conditions model. The signals optimized in the Synchro model for the 2040 No-Build volumes were incorporated and the 2040 No-Build volumes were then input into the Vissim model.

The Highway Capacity Manual defines LOS for signalized and unsignalized intersections as a function of the average vehicle control delay. LOS may be calculated per movement or per approach for any intersection configuration, but LOS for the intersection as a whole is only defined for signalized and all-way stop configurations. Table 3 and Table 4 demonstrate the different levels of service for signalized and unsignalized intersections based on delay and volume to capacity ratio.

Table 3: Level of Service – Signalized Intersections

| Level of Service | Delay (seconds) | Description |
|---------------------|--------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| А | ≤10 | This level is typically assigned when the volume-to capacity ratio is low and either progression is exceptionally favorable or the cycle length is very short. If it is due to favorable progression, most vehicles arrive during the green indication and travel through the intersection without stopping. |
| В | >10-20 | This level is typically assigned when the volume-to-capacity ratio is low and either progression is highly favorable or the cycle length is short. More vehicles stop than with LOS A. |
| С | >20-35 | This level is typically assigned when progression is favorable or the cycle length is moderate. Individual <i>cycle failures</i> (i.e., one or more queued vehicles are not able to depart as a result of insufficient capacity during the cycle) may begin to appear at this level. This number of vehicles stopping is significant, although many vehicles still pass through the intersection without stopping. |
| D | >35-55 | This level is typically assigned when the volume-to-capacity ratio is high and either progression is ineffective or the cycle length is long. Many vehicles stop and individual cycle failures are noticeable. |
| E | >55-80 | This level is typically assigned when the volume-to-capacity ratio is high, progression is unfavorable, and the cycle length is long. Individual cycle failures are frequent. |
| F | >80 | This level is typically assigned when the volume-to-capacity ratio is very high, progression is very poor, and the cycle length is long. Most cycles fail to clear the queue. |



Table 4: Level of Service – Unignalized Intersections

| Level of Service | Delay (seconds) |
|---------------------|--------------------|
| Α | ≤10 |
| В | >10-15 |
| С | >15-25 |
| D | >25-35 |
| E | >35-50 |
| F | >50 |

The Downtown Durham Primary Study Area 2040 No-Build Vissim MOEs are presented in Table 5 for the AM and PM peak hours.

Table 5: 2040 No-Build Alternative Vissim Summary

| | | | AM Peak | | | PM Peak | |
|---------------------------|----------|-----------------|--------------|-----|-----------------|--------------|-----|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS |
| | EBL | 84 | 28.7 | С | 63 | 41.1 | D |
| | EBR | 62 | 26.8 | С | 58 | 50.5 | D |
| | EBT | 348 | 30.8 | С | 599 | 53.8 | D |
| | NBL | 78 | 29.3 | С | 47 | 32.4 | С |
| | NBR | 111 | 18.6 | В | 302 | 48.9 | D |
| | NBT | 176 | 27.4 | С | 300 | 50.8 | D |
| Main Street at 9th Street | SBL | 127 | 27.8 | С | 240 | 65.2 | E |
| Street | SBR | 96 | 33.8 | С | 76 | 32.7 | С |
| | SBT | 384 | 37.2 | D | 198 | 39.5 | D |
| | WBL | 128 | 18.8 | В | 216 | 70.0 | E |
| | WBR | 114 | 13.2 | В | 245 | 14.2 | В |
| | WBT | 274 | 16.7 | В | 452 | 17.7 | В |
| | All | | 27.0 | С | | 43.4 | D |
| | EBL | 119 | 3.3 | Α | 176 | 17.9 | С |
| | EBT | 467 | 3.2 | Α | 965 | 16.9 | С |
| Main Street at Iredell | SBL | 37 | 17.0 | С | 33 | 225.0 | F |
| Street | SBR | 20 | 11.5 | В | 77 | 175.0 | F |
| (Unsignalized) | WBR | 145 | 2.6 | Α | 25 | 11.6 | В |
| | WBT | 496 | 3.7 | Α | 836 | 15.7 | С |
| | All | | 3.9 | Α | | 26.8 | D |



| | | | AM Peak | | PM Peak | | | |
|----------------------------------|----------|-----------------|--------------|-----|-----------------|--------------|-----|--|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS | |
| | EBL | 14 | 57.2 | E | 113 | 37.9 | D | |
| | EBR | 143 | 6.9 | А | 255 | 7.9 | Α | |
| | EBT | 347 | 37.3 | D | 630 | 34.4 | С | |
| | NBL | 252 | 30.1 | С | 283 | 51.0 | D | |
| | NBR | 243 | 2.7 | А | 185 | 1.5 | Α | |
| Main Street at Broad | NBT | 299 | 17.3 | В | 448 | 16.1 | В | |
| Street | SBL | 66 | 60.5 | Е | 116 | 107.6 | F | |
| Street | SBR | 52 | 28.8 | С | 65 | 78.8 | Е | |
| | SBT | 412 | 43.7 | D | 625 | 93.0 | F | |
| | WBL | 175 | 68.3 | Е | 167 | 49.3 | D | |
| | WBR | 32 | 21.7 | С | 87 | 48.9 | D | |
| | WBT | 337 | 26.9 | С | 513 | 53.7 | D | |
| | All | | 30.9 | С | | 47.3 | D | |
| | NBR | 29 | 9.0 | А | 82 | 128.0 | F | |
| | NBT | 220 | 14.5 | В | 596 | 141.6 | F | |
| Pettigrew Street at | SBL | 25 | 1.6 | А | 42 | 12.4 | В | |
| 9th Street | SBT | 549 | 0.4 | А | 430 | 1.9 | Α | |
| (Unsignalized) | WBL | 79 | 39.4 | Е | 26 | 19.7 | С | |
| | WBR | 145 | 38.7 | Е | 53 | 46.6 | Е | |
| | All | | 11.9 | В | | 59.4 | F | |
| | EBL | 6 | 104.7 | F | 53 | 373.3 | F | |
| | EBR | 31 | 32.2 | D | 166 | 316.2 | F | |
| | EBT | 2 | 42.6 | Е | 3 | 345.7 | F | |
| | NBL | 191 | 25.1 | D | 48 | 118.5 | F | |
| | NBR | 19 | 27.9 | D | 9 | 67.0 | F | |
| Pettigrew Street at | NBT | 777 | 47.1 | Е | 820 | 122.4 | F | |
| Swift Avenue (Unsignalized to | SBL | 22 | 48.7 | Е | 16 | 133.0 | F | |
| Signalized to | SBR | 42 | 1.9 | А | 45 | 1.3 | Α | |
| Signalized/ | SBT | 666 | 0.7 | А | 986 | 1.0 | Α | |
| | WBL | 1 | 38.6 | Е | 17 | 854.1 | F | |
| | WBR | 11 | 100.9 | F | 43 | 941.6 | F | |
| | WBT | 2 | 106.4 | F | 6 | 928.8 | F | |
| | All | | 26.2 | D | | 92.5 | F | |



| | | | AM Peak | | PM Peak | | | |
|--------------------------------------|----------|-----------------|--------------|-----|-----------------|--------------|-----|--|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS | |
| | EBL | 128 | 52.8 | D | 187 | 118.9 | F | |
| | EBR | 86 | 7.5 | Α | 69 | 12.4 | В | |
| | EBT | 475 | 24.4 | С | 554 | 24.5 | С | |
| | NBL | 79 | 67.5 | E | 97 | 117.9 | F | |
| | NBR | 63 | 13.1 | В | 67 | 18.6 | В | |
| Main Charatan | NBT | 177 | 48.2 | D | 350 | 60.1 | Е | |
| Main Street at Buchanan Boulevard | SBL | 170 | 80.7 | F | 107 | 154.1 | F | |
| buchanan boulevaru | SBR | 170 | 24.4 | С | 179 | 43.1 | D | |
| | SBT | 327 | 56.1 | E | 312 | 95.5 | F | |
| | WBL | 51 | 62.5 | E | 36 | 93.5 | F | |
| | WBR | 44 | 26.8 | С | 181 | 26.1 | С | |
| | WBT | 293 | 27.6 | С | 689 | 27.2 | С | |
| | All | | 39.8 | D | | 52.0 | D | |
| | EBL | 52 | 24.8 | С | 40 | 1273.0 | F | |
| | EBR | 74 | 15.1 | С | 49 | 984.3 | F | |
| | EBT | 0 | 0.0 | Α | 0 | 0.0 | Α | |
| | NBL | 13 | 7.9 | А | 57 | 96.3 | F | |
| | NBR | 0 | 0.0 | Α | 0 | 0.0 | Α | |
| Maxwell Street at | NBT | 267 | 7.5 | Α | 474 | 107.1 | F | |
| Buchanan Boulevard | SBL | 0 | 0.0 | Α | 0 | 0.0 | Α | |
| (Unsignalized) | SBR | 17 | 0.6 | Α | 50 | 2.3 | Α | |
| | SBT | 447 | 0.6 | Α | 367 | 1.3 | Α | |
| | WBL | 0 | 0.0 | Α | 0 | 0.0 | Α | |
| | WBR | 0 | 0.0 | Α | 0 | 0.0 | Α | |
| | WBT | 0 | 0.0 | Α | 0 | 0.0 | Α | |
| | All | | 5.6 | Α | | 85.8 | F | |
| | EBL | 170 | 40.1 | D | 172 | 49.1 | D | |
| | EBT | 374 | 36.7 | D | 446 | 37.8 | D | |
| | NBL | 251 | 11.4 | В | 274 | 13.9 | В | |
| Duke Street at Main | NBR | 40 | 11.1 | В | 28 | 12.8 | В | |
| Street | NBT | 956 | 12.1 | В | 1133 | 14.1 | В | |
| | WBR | 22 | 21.0 | С | 24 | 28.9 | С | |
| | WBT | 93 | 33.6 | С | 270 | 35.2 | D | |
| | All | | 20.4 | С | | 23.6 | С | |



| | | | AM Peak | | PM Peak | | | |
|----------------------------------|----------|-----------------|--------------|-----|-----------------|--------------|-----|--|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS | |
| | EBL | 16 | 10.5 | В | 28 | 16.0 | С | |
| | EBT | 3 | 10.4 | В | 15 | 20.6 | С | |
| | NBL | 59 | 0.6 | Α | 104 | 0.8 | Α | |
| Duke Street at Peabody Street | NBR | 1 | 0.5 | Α | 4 | 3.1 | Α | |
| (Unsignalized) | NBT | 1218 | 3.1 | А | 1399 | 6.2 | А | |
| (Onsignanzea) | WBR | 13 | 10.5 | В | 8 | 13.2 | В | |
| | WBT | 31 | 14.7 | В | 30 | 17.1 | С | |
| | All | | 3.5 | Α | | 6.4 | Α | |
| | EBL1 | 0 | 0.7 | А | 0 | 3.5 | А | |
| | EBL2 | 5 | 8.9 | Α | 15 | 15.5 | С | |
| Memorial Street at Duke Street | NBL | 20 | 3.6 | Α | 10 | 6.8 | А | |
| (Unsignalized) | NBT1 | 1273 | 4.8 | Α | 1492 | 8.4 | А | |
| (01101811411204) | NBT2 | 0 | 2.8 | Α | 0 | 6.9 | А | |
| | All | | 2.9 | Α | | 7.1 | Α | |
| | EBL | 193 | 20.3 | С | 161 | 61.5 | E | |
| | EBT | 690 | 15.1 | В | 388 | 17.0 | В | |
| | NBL | 117 | 26.4 | С | 189 | 38.0 | D | |
| Chapel Hill Street at | NBR | 132 | 12.4 | В | 111 | 7.7 | Α | |
| Duke Street | NBT | 1039 | 27.8 | С | 1318 | 40.8 | D | |
| | WBR | 61 | 13.6 | В | 23 | 15.7 | В | |
| | WBT | 383 | 16.5 | В | 749 | 17.2 | В | |
| | All | | 21.1 | С | | 31.3 | С | |
| | EBR | 137 | 1.6 | А | 52 | 1.3 | Α | |
| | EBT | 685 | 1.7 | А | 447 | 1.6 | Α | |
| Chapel Hill Street at | NBL | 15 | 15.5 | С | 42 | 47.4 | Е | |
| Willard Street | NBR | 29 | 11.4 | В | 93 | 26.3 | D | |
| (Unsignalized) | WBL | 47 | 7.9 | А | 57 | 4.0 | Α | |
| | WBT | 429 | 1.0 | А | 730 | 9.5 | Α | |
| | All | | 2.0 | Α | | 8.7 | Α | |



| | | | AM Peak | | PM Peak | | | |
|-------------------------------------------|----------|-----------------|--------------|-----|-----------------|--------------|-----|--|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS | |
| | EBR | 260 | 3.6 | Α | 167 | 3.3 | Α | |
| | EBT | 454 | 3.8 | Α | 373 | 4.1 | Α | |
| 5 6 | NBL | 86 | 17.1 | В | 246 | 47.3 | D | |
| Pettigrew Street at Chapel Hill Street | NBR | 69 | 8.9 | Α | 41 | 36.5 | D | |
| Chaper Hill Street | WBL | 42 | 13.7 | В | 37 | 15.1 | В | |
| | WBT | 390 | 8.5 | А | 541 | 13.9 | В | |
| | All | | 6.7 | Α | | 16.6 | В | |
| | EBL | 13 | 32.4 | С | 26 | 26.4 | С | |
| | EBR | 36 | 11.1 | В | 53 | 11.9 | В | |
| | EBT | 121 | 20.8 | С | 143 | 18.1 | В | |
| | NBL | 21 | 16.8 | В | 43 | 20.1 | С | |
| | NBR | 7 | 9.2 | А | 47 | 12.1 | В | |
| Dia alawali Chanah ah | NBT | 139 | 15.3 | В | 200 | 16.2 | В | |
| Blackwell Street at Pettigrew Street | SBL | 51 | 3.0 | Α | 74 | 12.8 | В | |
| Tettigiew Street | SBR | 33 | 1.0 | Α | 44 | 2.4 | Α | |
| | SBT | 164 | 1.4 | Α | 187 | 7.1 | Α | |
| | WBL | 9 | 16.6 | В | 35 | 5.8 | Α | |
| | WBR | 51 | 15.7 | В | 49 | 10.9 | В | |
| | WBT | 205 | 14.3 | В | 126 | 6.3 | Α | |
| | All | | 11.9 | В | | 12.2 | В | |
| | EBL | 16 | 14.6 | В | 111 | 18.6 | В | |
| | EBR | 7 | 5.0 | Α | 190 | 14.3 | В | |
| | EBT | 385 | 16.2 | В | 371 | 17.0 | В | |
| Blackwell Street at | NBR | 7 | 4.0 | Α | 57 | 2.7 | Α | |
| Ramseur Street | NBT | 196 | 8.7 | А | 218 | 6.8 | А | |
| | SBL | 27 | 16.5 | В | 81 | 14.7 | В | |
| | SBT | 241 | 15.0 | В | 115 | 13.3 | В | |
| | All | _ | 14.0 | В | | 13.5 | В | |



| | | | AM Peak | | PM Peak | | | |
|------------------------------------|----------|-----------------|--------------|-----|-----------------|--------------|-----|--|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS | |
| | EBL | 52 | 28.2 | С | 41 | 33.3 | С | |
| | EBR | 50 | 21.7 | С | 24 | 24.7 | С | |
| | EBT | 176 | 26.7 | С | 223 | 31.6 | С | |
| | NBL | 20 | 7.2 | Α | 38 | 9.8 | Α | |
| | NBR | 9 | 3.9 | А | 16 | 7.4 | А | |
| Main Street at | NBT | 183 | 5.7 | Α | 275 | 8.8 | Α | |
| Corcoran Street | SBL | 24 | 12.6 | В | 57 | 14.9 | В | |
| Corcoran Street | SBR | 22 | 7.1 | А | 35 | 8.0 | Α | |
| | SBT | 187 | 12.5 | В | 154 | 11.0 | В | |
| | WBL | 31 | 11.2 | В | 18 | 32.8 | С | |
| | WBR | 42 | 6.2 | Α | 66 | 21.2 | С | |
| | WBT | 174 | 8.7 | Α | 165 | 30.8 | С | |
| | All | | 13.9 | В | | 19.1 | В | |
| | EBR | 7 | 36.9 | D | 24 | 36.9 | D | |
| | EBT | 202 | 42.8 | D | 272 | 31.8 | С | |
| | SBL | 173 | 16.6 | В | 92 | 34.5 | С | |
| Mangum Street at | SBR | 7 | 5.3 | Α | 14 | 8.7 | Α | |
| Main Street | SBT | 1099 | 17.7 | В | 985 | 33.4 | С | |
| | WBL | 84 | 53.4 | D | 281 | 179.1 | F | |
| | WBT | 240 | 23.3 | С | 235 | 79.9 | E | |
| | All | | 23.0 | С | | 53.6 | D | |
| | EBR | 117 | 45.6 | D | 176 | 46.6 | D | |
| Managuna Chuach at | EBT | 302 | 20.8 | С | 333 | 9.4 | Α | |
| Mangum Street at Ramseur Street | SBL | 91 | 17.8 | В | 61 | 29.3 | С | |
| Namsear Street | SBT | 1099 | 16.8 | В | 1229 | 28.2 | С | |
| | All | | 19.7 | В | | 26.5 | С | |
| | EBR | 52 | 26.1 | С | 122 | 15.8 | В | |
| | EBT | 127 | 40.8 | D | 142 | 23.5 | С | |
| | SBL | 54 | 0.7 | А | 58 | 0.6 | Α | |
| Mangum Street at | SBR | 67 | 0.5 | Α | 29 | 0.3 | А | |
| Pettigrew Street | SBT | 1095 | 0.2 | А | 1318 | 0.3 | А | |
| | WBL | 77 | 58.6 | Е | 123 | 68.3 | Е | |
| | WBT | 198 | 37.5 | D | 181 | 33.7 | С | |
| | All | _ | 11.4 | В | _ | 10.7 | В | |



| | | AM Peak | | | PM Peak | | | |
|---------------------------------------|----------|-----------------|--------------|-----|-----------------|--------------|-----|--|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS | |
| | EBL | 15 | 12.4 | В | 26 | 11.6 | В | |
| | EBR | 25 | 5.9 | А | 27 | 9.7 | Α | |
| | EBT | 75 | 9.3 | Α | 197 | 12.2 | В | |
| | NBL | 0 | 0.0 | Α | 51 | 25.0 | С | |
| | NBR | 34 | 8.2 | Α | 69 | 14.1 | В | |
| Dottigrow Ctroot at | NBT | 100 | 17.6 | В | 251 | 16.6 | В | |
| Pettigrew Street at Dillard Street | SBL | 45 | 21.3 | С | 96 | 24.6 | С | |
| Dillard Street | SBR | 98 | 9.9 | Α | 16 | 13.4 | В | |
| | SBT | 110 | 18.5 | В | 238 | 16.9 | В | |
| | WBL | 25 | 6.1 | Α | 69 | 17.8 | В | |
| | WBR | 18 | 3.6 | Α | 32 | 11.7 | В | |
| | WBT | 87 | 6.0 | Α | 78 | 16.3 | В | |
| | All | | 12.3 | В | | 16.5 | В | |
| | EBL | 7 | 61.4 | E | 10 | 38.7 | D | |
| | EBR | 26 | 5.6 | Α | 124 | 29.3 | С | |
| | EBT | 57 | 53.9 | D | 180 | 45.2 | D | |
| | NBL | 35 | 5.9 | А | 19 | 5.2 | Α | |
| | NBR | 61 | 0.3 | Α | 133 | 0.5 | Α | |
| | NBT | 388 | 1.3 | А | 436 | 1.1 | Α | |
| Fayetteville Street at | SBL | 41 | 21.1 | С | 42 | 25.8 | С | |
| Pettigrew Street | SBR | 7 | 13.4 | В | 4 | 24.9 | С | |
| | SBT | 445 | 22.4 | С | 667 | 27.0 | С | |
| | WBL | 90 | 59.8 | Е | 131 | 143.1 | F | |
| | WBR | 50 | 31.3 | С | 40 | 65.4 | Е | |
| | WBT | 127 | 47.2 | D | 83 | 64.0 | Е | |
| | All | | 21.3 | С | | 31.1 | С | |
| | NBL | 185 | 14.2 | В | 308 | 17.8 | В | |
| | NBT | 367 | 11.7 | В | 567 | 10.8 | В | |
| | SBR | 40 | 2.1 | Α | 31 | 6.9 | Α | |
| Fayetteville Street at | SBT | 521 | 6.8 | А | 891 | 7.2 | Α | |
| Jackie Robinson Drive | WBL | 144 | 40.5 | D | 151 | 43.9 | D | |
| | WBR | 117 | 6.7 | А | 21 | 41.5 | D | |
| | WBT | 13 | 36.8 | D | 8 | 42.9 | D | |
| | All | | 12.9 | В | | 13.2 | В | |



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| | | | AM Peak | AM Peak | | PM Peak | | |
|---------------------|----------|-----------------|--------------|---------|-----------------|--------------|-----|--|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS | |
| | EBL | 33 | 45.3 | D | 130 | 54.5 | D | |
| | EBR | 130 | 6.6 | Α | 17 | 6.7 | Α | |
| | EBT | 0 | 0.0 | Α | 0 | 0.0 | Α | |
| Morehead Avenue at | NBR | 18 | 1.8 | Α | 3 | 2.6 | А | |
| Fayetteville Street | NBT | 519 | 2.6 | Α | 745 | 3.2 | Α | |
| | SBL | 71 | 3.2 | Α | 146 | 6.2 | А | |
| | SBT | 594 | 1.5 | Α | 896 | 2.4 | А | |
| | All | | 3.5 | Α | | 6.5 | Α | |
| | EBL | 0 | 0.0 | А | 27 | 17.5 | В | |
| | EBR | 13 | 3.2 | А | 0 | 0.0 | А | |
| | EBT | 146 | 6.2 | Α | 328 | 15.9 | В | |
| | NBL | 0 | 0.0 | Α | 54 | 25.5 | С | |
| | NBR | 73 | 9.8 | А | 185 | 21.4 | С | |
| Pettigrew Street at | NBT | 51 | 19.6 | В | 119 | 25.0 | С | |
| Grant Street | SBL | 86 | 25.2 | С | 134 | 25.9 | С | |
| Grant Street | SBR | 0 | 0.0 | Α | 0 | 0.0 | Α | |
| | SBT | 68 | 23.0 | С | 59 | 21.4 | С | |
| | WBL | 127 | 7.8 | Α | 140 | 16.2 | В | |
| | WBR | 121 | 5.4 | Α | 92 | 8.3 | Α | |
| | WBT | 267 | 7.0 | А | 200 | 11.0 | В | |
| | All | | 10.5 | В | | 18.0 | В | |
| | EBR | 72 | 2.7 | Α | 121 | 2.9 | Α | |
| | EBT | 287 | 2.9 | Α | 496 | 2.8 | Α | |
| Gann Street at | NBL | 102 | 9.4 | Α | 172 | 15.7 | С | |
| Pettigrew Street | NBR | 12 | 7.1 | Α | 43 | 13.1 | В | |
| (Unsignalized) | WBL | 23 | 8.4 | Α | 63 | 10.1 | В | |
| | WBT | 437 | 0.4 | Α | 357 | 0.5 | Α | |
| | All | | 2.6 | Α | | 4.7 | Α | |



| | | AM Peak | | | PM Peak | | | |
|-------------------|----------|-----------------|--------------|-----|-----------------|--------------|-----|--|
| Intersection | Movement | Volume (vph) | Delay (s) | LOS | Volume (vph) | Delay (s) | LOS | |
| | EBL | 69 | 57.6 | E | 31 | 56.0 | E | |
| | EBR | 182 | 13.1 | В | 186 | 7.2 | Α | |
| | NBL | 14 | 18.4 | В | 137 | 18.6 | В | |
| | NBT | 875 | 12.0 | В | 1500 | 9.7 | Α | |
| Alston Avenue at | SBR | 46 | 12.2 | В | 22 | 10.2 | В | |
| Gann Street | SBT | 1440 | 14.0 | В | 1355 | 13.4 | В | |
| | WBL | 457 | 59.5 | Е | 150 | 55.3 | Е | |
| | WBR | 315 | 41.9 | D | 147 | 11.9 | В | |
| | WBT | 52 | 58.9 | E | 1 | 24.4 | С | |
| | All | | 23.1 | С | | 13.8 | В | |
| | EBL | 90 | 57.0 | E | 77 | 26.4 | С | |
| | EBT | 91 | 43.3 | D | 123 | 14.7 | В | |
| | NBL | 188 | 9.1 | А | 205 | 20.9 | С | |
| Roxboro Street at | NBR | 24 | 2.6 | А | 127 | 7.9 | Α | |
| Pettigrew Street | NBT | 1524 | 9.0 | А | 1244 | 20.5 | С | |
| | WBR | 98 | 67.6 | E | 46 | 19.5 | В | |
| | WBT | 87 | 81.0 | F | 99 | 28.5 | С | |
| | All | | 18.4 | В | | 20.0 | В | |

Overall, as indicated in Table 5 for the No-Build Vissim outputs, the downtown Durham corridor is relatively less congested compared to other corridors studied as part of the D-O LRT project. All of the overall intersections report an LOS D or better during the AM peak hour. Several individual movements in the area bounded by Main Street, Pettigrew Street, Broad Street, and 9th Street operate at LOS E or F in the future. This is not unexpected as the only planned improvement for these intersections would grade separate the NCRR track between Blackwell Street and Mangum Street and the demand is expected to increase by approximately from 30% to 60% in this dense grid area. The overall LOS at Pettigrew Street and Swift Ave and at Pettigrew Street and 9th Street are F during the PM peak hour. This is partially due to the traffic demand growth at the intersections themselves and partially due to the demand growth at the downstream intersections. The demand at the intersection of Main Street and 9th Street is expected to increase from 1,798 vehicles per hour in 2012 to 2,796 vehicles per hour in 2040. The demand at Main Street and Broad Street is expected to increase from 2,652 vehicles per hour in the year of 2011 to 3,487 vehicles per hour in 2040. Because it is a dense grid network, the queues are expected to spill back from the downstream intersections and cause further delay. In addition, the Smith Warehouse driveway at Buchanan Boulevard also operates at LOS F under 2040 No-Build conditions due to the queue spillback from the intersection of Main Street and Buchanan Boulevard.

A 2040 No-Build Synchro-based model was developed to further investigate the potential signal optimization in the micro-simulation area to improve traffic operation. In addition to covering the same



network area as in the Vissim model along the LRT corridor, a secondary study area Synchro network, as described in Section 5, was developed to analyze the effects of traffic detoured due to Pettigrew Street's one-way eastbound conversion. Refer to Appendix C for Synchro model outputs for the No-Build scenario.

It is important to note that there are No-Build background issues that would exist regardless of the potential D-O LRT project. These areas of congestion will also have an impact on meeting the thresholds laid out in NCDOT's "Policy on Street and Driveway Access to North Carolina Highways".

Based on the results of the Vissim analyses, the following intersections in the primary study area are anticipated to operate at LOS E or LOS F in at least one No-Build peak hour:

- Pettigrew Street and 9th Street
- Pettigrew Street and Swift Avenue
- Maxwell Street and Buchanan Boulevard

In the secondary study network, all intersections are expected to operate at LOS C or better for both AM and PM peak hours.



6.3 2040 Build Conditions Option 1 - LRT at-grade at Swift Avenue

As it has been described in Section 3.3, the 2040 LRT Option 1 would close Pettigrew Street between Case Street and east of Swift Avenue to provide for an exclusive right-of-way for the LRT to cross Swift Avenue at-grade. In addition, Pettigrew Street would be converted to one-way eastbound general traffic operation between E Chapel Hill Street and Dillard Street, and the LRT would run along the north side of the Pettigrew Street east of Chapel Hill Street.

Based on the above model network elements and the methodologies defined under MOEs, the results from Vissim for the 2040 Build Conditions were determined. Detailed traffic delay at individual movement level and overall intersection level was compared to No-Build scenarios in Table 10 (AM peak hour) and Table 11 (PM peak hour) in Section 7. Queuing information for 2040 LRT Option 1 is also included in the comparison tables.

6.4 2040 Build Conditions Option 2 – Elevated LRT at Swift Avenue

Option 2 would elevate the LRT at Swift Avenue and keep Pettigrew Street open from Case Street to east of Swift Avenue. Similar to Option 1, Pettigrew Street would be converted to one-way eastbound general traffic operation between E Chapel Hill Street and Dillard Street, and the LRT would run along the north side of the Pettigrew Street east of Chapel Hill Street.

Based on the above model network elements and the methodologies defined under MOEs, the results from Vissim for the 2040 Build Conditions were determined. Detailed traffic delay at the individual movement level and overall intersection level were compared to No-Build scenarios in Table 12 (AM peak hour) and Table 13 (PM peak hour) in Section 7. Queuing information for 2040 LRT Option 2 is also included in Table 12 (AM peak hour) and Table 13 (PM peak hour).

Proposed geometric mitigations that have been applied to both the 2040 LRT Option 1 and 2040 LRT Option 2 are listed in Table 6.

Intersection signal timing changes from 1) Existing to No-Build and from 2) No-Build to Build including traffic signal cycle length and phasing modifications are shown in Table 7 for LRT Option 1, and LRT Option 2 from Buchanan Boulevard to Alston Avenue. Table 8 shows the scenario changes for the single intersection under LRT Option 2 that would have a different geometry than LRT Option 1. Tables 7 and 8 also indicate the lane configuration modifications that are proposed between Existing to No-Build, and No-Build to Build conditions.

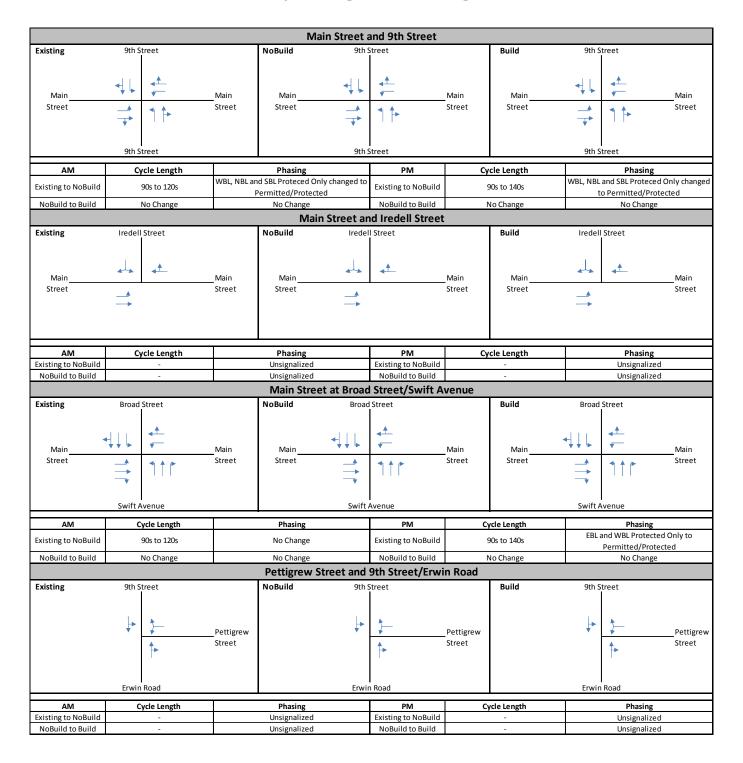


Table 6: LRT Options Geometric Mitigation Measures

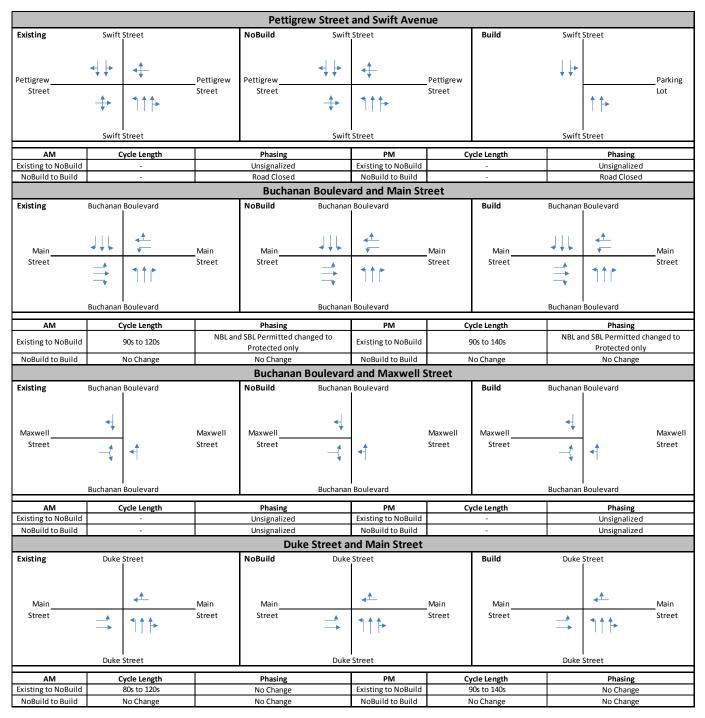
| Downtown Durham Segment | |
|----------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Pettigrew Street at Swift Avenue | Pettigrew is closed between Case St and Swift Ave (Opt 1 only) |
| Pettigrew Street at Chapel Hill Street | Remove westbound Pettigrew St general traffic lanes |
| Pettigrew Street at Blackwell Street | Remove westbound Pettigrew St general traffic lanes Remove dedicated eastbound Pettigrew St left turn bay to provide single left/through/right lane |
| Pettigrew Street at Mangum Street | Remove westbound Pettigrew St general traffic lanes Restripe southbound Mangum St right turn lane to a through lane Add dedicated eastbound Pettigrew St right turn lane |
| Pettigrew Street at Dillard Street | Eliminate dedicated northbound Dillard St left turn lane Restripe westbound Pettigrew St lane to prohibit through traffic to provide a left/right only lane Restripe southbound Dillard St left/through lane to a through lane |
| Pettigrew Street at Roxboro Street | Remove westbound Pettigrew St general traffic lanes Add dedicated eastbound Pettigrew St left turn lane Restripe northbound left/through to a through lane |



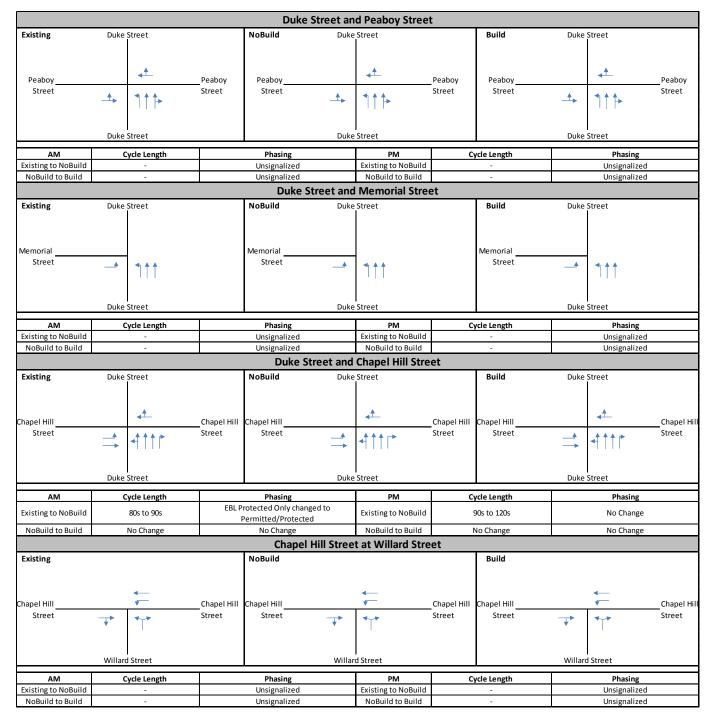
Table 7. 2040 LRT Option 1 Signal & Lane Configuration Modifications



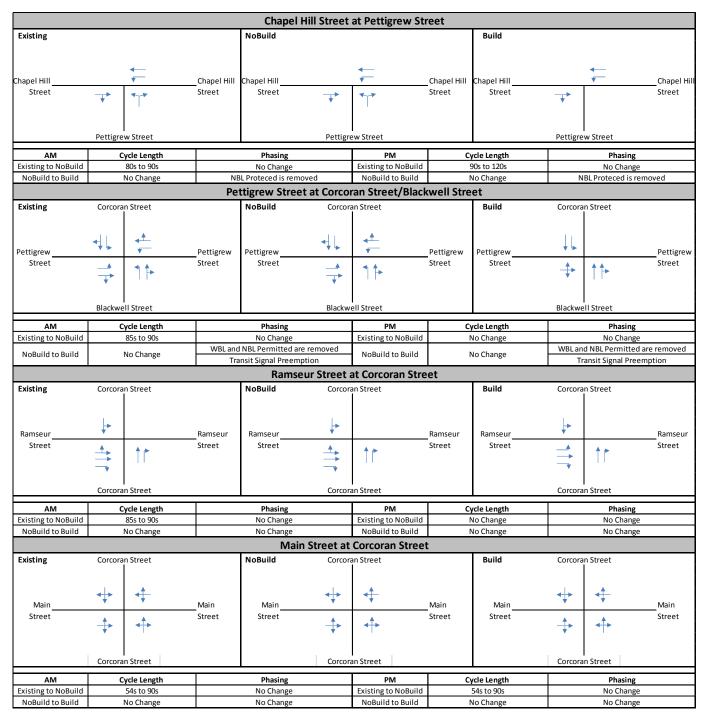




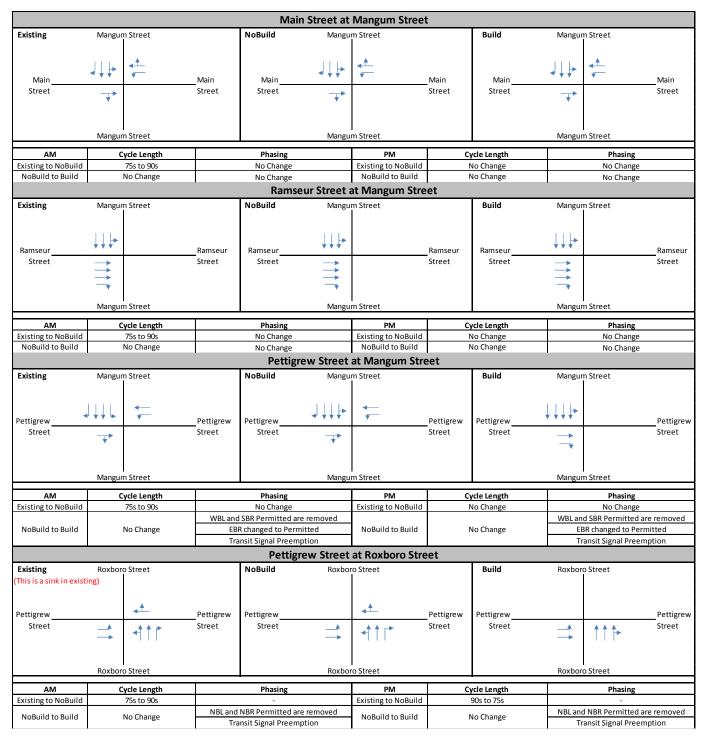














| | | | Pettigrew Stree | et at Dillard Stree | et | | | | |
|-------------------------------------------------------------------|----------------------------------------------------------|-----------------------------|----------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------|------------|---------------------------------------------------------------|-------------------------------------|
| Existing | Dillard Street | | _ | rd Street | | Build | Dillard | Street | |
| Pettigrew Street | Dillard Street | Pettigrew Street | Pettigrew Street Dilla | ↑ | Pettigrew Street | Pettigrew Street | Dillard | \$\frac{1}{2} \tag{5} \tag{5} | Pettigrew Street |
| | 1 | | - | | | .1. 1 | Dillara | | |
| AM Existing to NoBuild | Cycle Length 75s to 60s | + | Phasing No Change | PM Existing to NoBuild | | rcle Length 60s to 65s | | Phasing No Change | |
| NoBuild to Build | No Change | NB | L Permitted is removed | NoBuild to Build | | lo Change | NB | L Permitted is re | |
| Nobulia to Bulia | No Change | Tra | insit Signal Preemption | | L | vo Change | Tra | nsit Signal Pree | mption |
| | | | Pettigrew Street | - | oad | | | | |
| Existing | Fayetteville Road | | NoBuild Fayette | eville Road | | Build | Fayettevi | lle Road | |
| PettigrewStreet | Fayetteville Road | Pettigrew Street | Pettigrew Street Favett | * A A A A A A A A A A A A A A A A A A A | Pettigrew Street | Pettigrew Street | Fayettevi | 1 1 1 | Pettigrew Street |
| 404 | | | • | | | ala I a aash | 1 | | |
| AM Existing to NoBuild | Cycle Length 100s to 120s | + | Phasing No Change | PM Existing to NoBuild | | rcle Length 10s to 120s | | Phasing No Change | |
| NoBuild to Build | No Change | SBL Permit | ted changed to Protected Only | NoBuild to Build | | lo Change | SBL Permit | | Protected Only |
| Nobulia to bulia | No change | Tra | insit Signal Preemption | | | vo change | Tra | nsit Signal Pree | mption |
| | | | Fayetteville Road at | | n Drive | | | | |
| Jackie Robinson Drive | Fayetteville Road | Jackie Robinson Drive | Jackie Robinson Drive | eville Road | Jackie _Robinson | Jackie Robinson | Fayettevi | <u>+</u> | Jackie Robinson |
| | | | 5 | 1 1 | Drive | Drive | | 111 | Drive |
| | Fayetteville Road | | | eville Road | Drive | Drive | Fayettevi | ¶ ↑ ↑ | Drive |
| AM | | | Fayettı | * A A A A A A A A A A A A A A A A A A A | | Drive | Fayettevi | Ile Road Phasing | Drive |
| AM Existing to NoBuild | Fayetteville Road Cycle Length 100s to 120s | | | | c, | | NBL F | | hanged to |
| | Cycle Length | | Fayetti Phasing Protected Only changed to Permitted/Protected No Change | PM Existing to NoBuild NoBuild to Build | C ₁ | rcle Length | NBL F | Phasing rotected Only o | hanged to ected |
| Existing to NoBuild NoBuild to Build | Cycle Length 100s to 120s | | Fayetti Phasing Protected Only changed to Permitted/Protected | PM Existing to NoBuild NoBuild to Build | C ₁ | rcle Length 10s to 120s | NBL F | Phasing rotected Only of Permitted/Prote | hanged to ected |
| Existing to NoBuild | Cycle Length 100s to 120s No Change Fayetteville Road | | Phasing Protected Only changed to Permitted/Protected No Change Fayetteville Road NoBuild Fayett Morehead Avenue | PM Existing to NoBuild NoBuild to Build at Morehead Average eville Road | C ₁ | rcle Length 10s to 120s | RBL F | Phasing rrotected Only of Permitted/Prote No Change | hanged to ected |
| Existing to NoBuild NoBuild to Build Existing Morehead Avenue | Cycle Length 100s to 120s No Change Fayetteville Road | Morehead | Phasing Protected Only changed to Permitted/Protected No Change Fayetteville Road NoBuild Fayette Morehead Avenue Fayette | PM Existing to NoBuild NoBuild to Build at Morehead Ave eville Road | enue Morehead Avenue | rcle Length 10s to 120s Io Change Build Morehead Avenue | RBL F | Phasing rrotected Only of Permitted/Prote No Change Ille Road | hanged to ected Morehead |
| Existing to NoBuild NoBuild to Build Existing Morehead | Cycle Length 100s to 120s No Change Fayetteville Road | Morehead | Phasing Protected Only changed to Permitted/Protected No Change Fayetteville Road NoBuild Fayett Morehead Avenue | PM Existing to NoBuild NoBuild to Build at Morehead Average eville Road | Company of the control of the contro | rcle Length 10s to 120s No Change Build Morehead | RBL F | Phasing rrotected Only of Permitted/Prote No Change | hanged to ected Morehead Avenue |



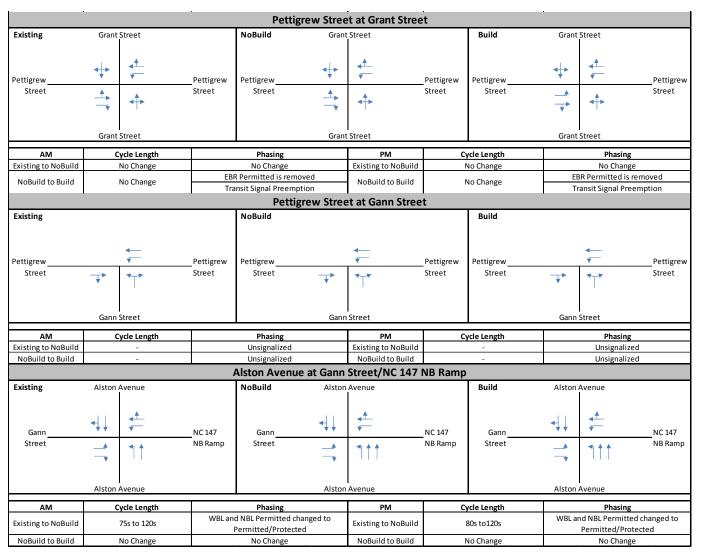
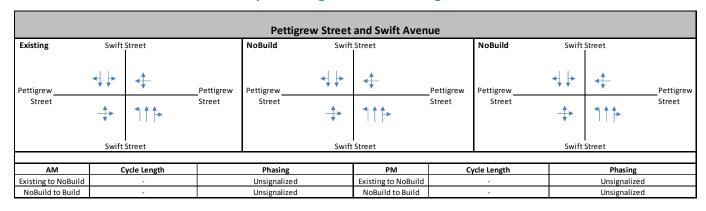


Table 8. 2040 LRT Option 2 Signal & Lane Configuration Modifications





7. Summary of Results

The following section summarizes the Vissim simulation results for the 2040 No-Build versus the two 2040 Build LRT Alternatives in a side by side manner. Table 9 through Table 12 include individual movement and overall intersection delays, LOS and queuing information as reported by Vissim for all future scenarios.

Table 13 and Table 14 compare the 2040 No-Build versus 2040 Build LRT Options Scenarios' Synchro results for the secondary study area outside of the Pettigrew Street LRT corridor.



Table 9: D-O LRT: Downtown Durham Segment – VISSIM Intersection Analysis Output Summary - 2040 Build Option 1 vs. 2040 No-Build AM Peak Hour 8:00 - 9:00 AM

| | | | Volume | e (VPH) | Volume | · (VPH) | | Dela | y (Seconds) | | LC | os | | Avg (| Queue Length | ı (ft) | | Max | x Queue | Length (ft) | |
|------|-------------------------------------------|----------|--------|---------|--------|---------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 84 | 84 | 81 | 84 | 24.8 | 28.7 | -3.9 | -13.6% | С | С | 10 | 12 | -2 | -15.90% | 625 | 115 | 111 | 4 | 3.5% |
| | | EBR | 63 | 64 | 61 | 62 | 26.2 | 26.8 | -0.6 | -2.2% | С | С | 68 | 77 | -9 | -12.22% | 900 | 439 | 428 | 11 | 2.6% |
| | | EBT | 366 | 364 | 343 | 348 | 29.0 | 30.8 | -1.9 | -6.0% | С | С | 78 | 88 | -10 | -11.28% | 900 | 456 | 445 | 11 | 2.4% |
| | | NBL | 73 | 76 | 72 | 78 | 31.6 | 29.3 | 2.3 | 8.0% | С | С | 33 | 83 | -51 | -60.76% | 106 | 237 | 223 | 14 | 6.1% |
| | | NBR | 119 | 119 | 111 | 111 | 18.0 | 18.6 | -0.7 | -3.7% | В | В | 19 | 66 | -47 | -70.89% | 106 | 213 | 199 | 13 | 6.7% |
| | Main Ctroot at | NBT | 60 | 59 | 173 | 176 | 35.2 | 27.4 | 7.7 | 28.2% | D | С | 33 | 83 | -51 | -60.76% | 106 | 237 | 223 | 14 | 6.1% |
| 1 | Main Street at 9th Street ¹ | SBL | 145 | 143 | 127 | 127 | 27.0 | 27.8 | -0.8 | -3.0% | С | С | 114 | 125 | -12 | -9.46% | 330 | 514 | 485 | 28 | 5.8% |
| | July 3th cet | SBR | 84 | 83 | 95 | 96 | 33.9 | 33.8 | 0.1 | 0.3% | С | С | 91 | 104 | -12 | -11.87% | 330 | 484 | 456 | 28 | 6.2% |
| | | SBT | 349 | 354 | 375 | 384 | 38.5 | 37.2 | 1.4 | 3.7% | D | D | 114 | 125 | -12 | -9.46% | 330 | 514 | 485 | 28 | 5.8% |
| | | WBL | 200 | 233 | 125 | 128 | 18.9 | 18.8 | 0.2 | 0.8% | В | В | 17 | 10 | 7 | 63.29% | 190 | 226 | 139 | 87 | 62.8% |
| | | WBR | 210 | 244 | 111 | 114 | 10.5 | 13.2 | -2.7 | -20.3% | В | В | 25 | 27 | -2 | -8.88% | 300 | 365 | 328 | 37 | 11.1% |
| | | WBT | 226 | 257 | 265 | 274 | 14.7 | 16.7 | -1.9 | -11.6% | В | В | 32 | 35 | -3 | -7.57% | 300 | 387 | 350 | 37 | 10.4% |
| | | All | 1979 | 2080 | 1940 | 1982 | 25.5 | 27.0 | -1.5 | -5.7% | С | С | 53 | 70 | -17 | -24.35% | | 515 | 487 | 28 | 5.8% |
| | | EBL | 119 | 117 | 118 | 119 | 5.0 | 3.3 | 1.7 | 52.4% | Α | Α | 2 | 8 | -5 | -70.18% | 60 | 168 | 91 | 77 | 85.2% |
| | | EBT | 512 | 509 | 462 | 467 | 3.6 | 3.2 | 0.5 | 15.5% | Α | Α | 2 | 8 | -5 | -70.18% | 290 | 168 | 91 | 77 | 85.2% |
| | Main Street at | SBL | 44 | 42 | 38 | 37 | 22.3 | 17.0 | 5.3 | 31.4% | С | С | 0 | 3 | -3 | -87.07% | 370 | 44 | 40 | 4 | 11.1% |
| 2 | Iredell Street ¹ | SBR | 22 | 21 | 21 | 20 | 14.6 | 11.5 | 3.1 | 27.2% | В | В | 0 | 3 | -3 | -87.07% | 370 | 44 | 40 | 4 | 11.1% |
| | (Unsignalized) | WBR | 119 | 141 | 138 | 145 | 3.5 | 2.6 | 0.9 | 33.9% | Α | Α | 5 | 1 | 4 | 776.67% | 290 | 316 | 97 | 218 | 224.5% |
| | | WBT | 615 | 713 | 481 | 496 | 5.1 | 3.7 | 1.4 | 38.9% | Α | Α | 5 | 1 | 4 | 776.67% | 290 | 316 | 97 | 218 | 224.5% |
| | | All | 1432 | 1543 | 1258 | 1284 | 5.1 | 3.9 | 1.2 | 31.9% | Α | Α | 3 | 4 | -1 | -33.28% | | 322 | 140 | 182 | 129.4% |



| | | | Volume | e (VPH) | Volume | e (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Length | ı (ft) | | Max | x Queue | Length (ft) | |
|------|----------------------------|----------|--------|---------|--------|---------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 13 | 14 | 13 | 14 | 101.2 | 57.2 | 44.0 | 76.9% | F | E | 30 | 43 | -12 | -29.09% | 198 | 393 | 390 | 3 | 0.7% |
| | | EBR | 169 | 166 | 144 | 143 | 5.6 | 6.9 | -1.4 | -19.8% | Α | Α | 0 | 3 | -3 | -98.39% | 317 | 23 | 54 | -31 | -58.0% |
| | | EBT | 374 | 371 | 342 | 347 | 33.5 | 37.3 | -3.8 | -10.2% | С | D | 88 | 101 | -13 | -12.60% | 317 | 452 | 444 | 8 | 1.9% |
| | | NBL | 381 | 461 | 241 | 252 | 21.6 | 30.1 | -8.5 | -28.2% | С | С | 100 | 202 | -102 | -50.68% | 121 | 184 | 275 | -91 | -33.1% |
| | | NBR | 223 | 270 | 237 | 243 | 1.2 | 2.7 | -1.4 | -53.2% | Α | Α | 0 | 0 | 0 | -62.82% | 116 | 33 | 48 | -15 | -31.3% |
| | Main Street at | NBT | 238 | 285 | 290 | 299 | 23.9 | 17.3 | 6.6 | 37.8% | С | В | 100 | 202 | -102 | -50.68% | 121 | 184 | 275 | -91 | -33.1% |
| 3 | Broad Street ¹ | SBL | 87 | 83 | 69 | 66 | 50.7 | 60.5 | -9.8 | -16.1% | D | Е | 26 | 24 | 2 | 8.35% | 130 | 183 | 180 | 3 | 1.7% |
| | Broad Street | SBR | 90 | 89 | 50 | 52 | 31.8 | 28.8 | 3.0 | 10.3% | С | С | 40 | 66 | -26 | -39.59% | 450 | 410 | 466 | -56 | -12.1% |
| | | SBT | 335 | 329 | 411 | 412 | 45.1 | 43.7 | 1.4 | 3.2% | D | D | 69 | 96 | -27 | -27.70% | 450 | 453 | 508 | -55 | -10.8% |
| | | WBL | 139 | 161 | 171 | 175 | 266.1 | 68.3 | 197.8 | 289.6% | F | E | 449 | 92 | 357 | 387.86% | 412 | 677 | 463 | 214 | 46.1% |
| | | WBR | 37 | 40 | 33 | 32 | 48.6 | 21.7 | 26.9 | 123.7% | D | С | 53 | 23 | 30 | 126.54% | 560 | 576 | 390 | 186 | 47.8% |
| | | WBT | 265 | 304 | 328 | 337 | 57.0 | 26.9 | 30.1 | 112.1% | Е | С | 81 | 57 | 24 | 41.34% | 560 | 657 | 473 | 185 | 39.1% |
| | | All | 2352 | 2573 | 2328 | 2372 | 44.6 | 30.9 | 13.7 | 44.2% | D | С | 86 | 76 | 10 | 13.84% | | 677 | 578 | 99 | 17.1% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 5.6 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBR | 23 | 24 | 28 | 29 | 2.9 | 9.0 | -6.1 | -68.2% | Α | Α | 1 | 11 | -10 | -90.03% | 720 | 116 | 174 | -58 | -33.3% |
| | | NBT | 238 | 241 | 213 | 220 | 3.0 | 14.5 | -11.5 | -79.5% | Α | В | 1 | 11 | -10 | -90.03% | 720 | 116 | 174 | -58 | -33.3% |
| | Pettigrew Street | SBL | 30 | 32 | 24 | 25 | 1.0 | 1.6 | -0.6 | -36.0% | Α | Α | 0 | 0 | 0 | -71.43% | 105 | 55 | 53 | 3 | 5.3% |
| 4 | at 9th Street ¹ | SBT | 582 | 619 | 537 | 549 | 0.3 | 0.4 | 0.0 | -11.5% | Α | Α | 0 | 0 | 0 | -71.43% | 105 | 55 | 53 | 3 | 5.3% |
| | (Unsignalized) | WBL | 14 | 13 | 75 | 79 | 18.6 | 39.4 | -20.8 | -52.8% | С | Е | 0 | 33 | -33 | -99.96% | 185 | 23 | 298 | -275 | -92.3% |
| | | WBR | 14 | 13 | 143 | 145 | 12.8 | 38.7 | -25.9 | -66.9% | В | Е | 0 | 33 | -33 | -99.96% | 185 | 23 | 298 | -275 | -92.3% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 912 | 942 | 1019 | 1047 | 1.6 | 11.9 | -10.3 | -86.6% | Α | В | 0 | 15 | -14 | -97.97% | | 125 | 310 | -185 | -59.7% |



| | | | Volume | · (VPH) | Volume | · (VPH) | | Dela | y (Seconds) | | LC | os | | Avg (| Queue Length | (ft) | | Max | (Queue | Length (ft) | |
|------|------------------------------|----------|--------|---------|--------|---------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bui | ild | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | | | 6 | 6 | | 104.7 | | | | F | | 5 | | | 506 | | 73 | | |
| | | EBR | | | 32 | 31 | | 32.2 | | | | D | | 5 | | | 506 | | 73 | | |
| | | EBT | | | 1 | 2 | | 42.6 | | | | Е | | 5 | | | 506 | | 73 | | |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | | | 186 | 191 | | 25.1 | | | | D | | 49 | | | 443 | | 440 | | |
| | | NBR | | | 19 | 19 | | 27.9 | | | | D | | 204 | | | 443 | | 684 | | |
| | Pettigrew Street | NBT | 843 | 1016 | 752 | 777 | 101.1 | 47.1 | 53.9 | 114.5% | F | E | 716 | 204 | 512 | 250.87% | 443 | 851 | 684 | 167 | 24.4% |
| 5 | at Swift Avenue ¹ | SBL | | | 21 | 22 | | 48.7 | | | | E | | 12 | | | 137 | | 188 | | |
| | (Unsignalized) | SBR | | | 40 | 42 | | 1.9 | | | | Α | | 12 | | | 137 | | 188 | | |
| | | SBT | 643 | 656 | 662 | 666 | 0.8 | 0.7 | 0.1 | 20.9% | Α | Α | 3 | 12 | -9 | -76.26% | 137 | 201 | 188 | 13 | 6.9% |
| | | WBL | | | 1 | 1 | | 38.6 | | | | E | | 2 | | | 515 | | 9 | | |
| | | WBR | | | 10 | 11 | | 100.9 | | | | F | | 2 | | | 515 | | 9 | | |
| | | WBT | | | 2 | 2 | | 106.4 | | | | F | | 2 | | | 515 | | 9 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 1.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 137 | N/A | N/A | N/A |
| | | All | 1498 | 1672 | 1733 | 1770 | 57.1 | 26.2 | 30.9 | 118.0% | F | D | 180 | 43 | 137 | 318.76% | | 851 | 684 | 166 | 24.3% |
| | | EBL | 134 | 127 | 134 | 128 | 51.8 | 52.8 | -1.0 | -1.8% | D | D | 40 | 42 | -3 | -6.19% | 215 | 329 | 421 | -92 | -21.8% |
| | | EBR | 86 | 86 | 87 | 86 | 7.2 | 7.5 | -0.3 | -3.8% | Α | Α | 0 | 0 | 0 | 50.00% | 267 | 9 | 5 | 5 | 97.6% |
| | | EBT | 464 | 464 | 476 | 475 | 23.8 | 24.4 | -0.6 | -2.6% | С | С | 77 | 83 | -6 | -7.76% | 607 | 562 | 579 | -18 | -3.1% |
| | | NBL | 74 | 79 | 73 | 79 | 66.4 | 67.5 | -1.1 | -1.6% | E | Е | 35 | 36 | -1 | -3.05% | 70 | 178 | 185 | -7 | -3.9% |
| | | NBR | 63 | 61 | 65 | 63 | 12.0 | 13.1 | -1.2 | -8.8% | В | В | 0 | 0 | 0 | -21.74% | 120 | 17 | 18 | -1 | -5.0% |
| | Main Street at | NBT | 177 | 171 | 183 | 177 | 43.8 | 48.2 | -4.5 | -9.3% | D | D | 48 | 56 | -8 | -13.60% | 433 | 191 | 206 | -15 | -7.3% |
| 6 | Buchanan | SBL | 160 | 164 | 165 | 170 | 81.5 | 80.7 | 0.8 | 1.0% | F | F | 128 | 134 | -6 | -4.52% | 130 | 472 | 471 | 1 | 0.2% |
| | Boulevard ¹ | SBR | 171 | 169 | 171 | 170 | 23.4 | 24.4 | -1.0 | -4.2% | С | С | 4 | 5 | -1 | -25.50% | 130 | 190 | 176 | 14 | 8.0% |
| | | SBT | 325 | 325 | 326 | 327 | 56.2 | 56.1 | 0.1 | 0.2% | Е | Е | 158 | 154 | 4 | 2.49% | 400 | 471 | 470 | 2 | 0.4% |
| | | WBL | 50 | 50 | 52 | 51 | 60.5 | 62.5 | -1.9 | -3.1% | Е | Е | 17 | 18 | -1 | -3.56% | 382 | 168 | 163 | 5 | 2.9% |
| | | WBR | 43 | 43 | 45 | 44 | 27.9 | 26.8 | 1.1 | 3.9% | С | С | 59 | 58 | 1 | 2.31% | 530 | 397 | 371 | 26 | 7.0% |
| | | WBT | 292 | 293 | 293 | 293 | 27.7 | 27.6 | 0.2 | 0.5% | С | С | 59 | 58 | 1 | 2.31% | 530 | 397 | 371 | 26 | 7.0% |
| | | All | 2040 | 2032 | 2070 | 2063 | 39.0 | 39.8 | -0.7 | -1.8% | D | D | 52 | 54 | -2 | -2.97% | | 568 | 579 | -11 | -1.9% |



| | | | Volume | e (VPH) | Volume | · (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Length | ı (ft) | | Max | (Queue | Length (ft) | |
|------|-----------------------------------------------|----------|--------|---------|--------|---------|-------|-------|-------------|------------|---------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | D!I.d | No- | Difference | Difference | المانية | No- | Build | No- | D:fforonce | Difference | Storage | חייום | No- | Difference | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Bulla | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 50 | 48 | 54 | 52 | 19.3 | 24.8 | -5.5 | -22.1% | С | С | 15 | 25 | -10 | -38.97% | 465 | 234 | 263 | -29 | -10.9% |
| | | EBR | 71 | 70 | 75 | 74 | 11.9 | 15.1 | -3.2 | -21.2% | В | С | 2 | 6 | -4 | -72.99% | 465 | 83 | 134 | -51 | -38.3% |
| | | EBT | | | 0 | 0 | | 0.0 | | | | Α | | 6 | | | 465 | | 134 | | |
| | | NBL | 13 | 13 | 13 | 13 | 3.5 | 7.9 | -4.3 | -55.1% | Α | Α | 1 | 7 | -6 | -83.01% | 558 | 103 | 143 | -40 | -27.9% |
| | | NBR | | | 0 | 0 | | 0.0 | | | | Α | | 7 | | | 558 | | 143 | | |
| | Maxwell Street | NBT | 263 | 263 | 267 | 267 | 6.8 | 7.5 | -0.7 | -9.1% | Α | Α | 15 | 7 | 9 | 124.38% | 558 | 234 | 143 | 91 | 64.1% |
| 7 | at Buchanan Boulevard ² | SBL | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 432 | | 11 | | |
| | (Unsignalized) | SBR | 16 | 16 | 17 | 17 | 0.6 | 0.6 | 0.0 | 8.7% | Α | Α | 0 | 0 | 0 | 475.00% | 432 | 39 | 11 | 28 | 242.6% |
| | , | SBT | 446 | 445 | 448 | 447 | 1.2 | 0.6 | 0.6 | 117.0% | Α | Α | 0 | 0 | 0 | 475.00% | 432 | 39 | 11 | 28 | 242.6% |
| | | WBL | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 295 | | 0 | | |
| | | WBR | | | 0 | 0 | | 0.0 | | | | Α | | 25 | | | 295 | | 263 | | |
| | | WBT | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 295 | | 0 | | |
| | | All | 859 | 855 | 873 | 870 | 4.9 | 5.6 | -0.6 | -11.4% | Α | Α | 6 | 7 | -1 | -18.55% | | 234 | 263 | -29 | -10.9% |
| | | EBL | 154 | 154 | 175 | 170 | 38.8 | 40.1 | -1.3 | -3.3% | D | D | 33 | 43 | -9 | -22.07% | 198 | 301 | 307 | -6 | -2.1% |
| 1 | | EBT | 403 | 405 | 369 | 374 | 37.7 | 36.7 | 1.0 | 2.6% | D | D | 105 | 92 | 13 | 13.97% | 323 | 329 | 329 | 0 | 0.1% |
| | | NBL | 258 | 260 | 250 | 251 | 9.6 | 11.4 | -1.8 | -15.7% | Α | В | 13 | 16 | -3 | -17.74% | 204 | 308 | 386 | -78 | -20.2% |
| | Duke Street at | NBR | 49 | 47 | 41 | 40 | 10.0 | 11.1 | -1.0 | -9.4% | В | В | 30 | 39 | -9 | -22.58% | 300 | 388 | 389 | -1 | -0.4% |
| 8 | Main Street ¹ | NBT | 929 | 923 | 966 | 956 | 10.2 | 12.1 | -1.9 | -15.6% | В | В | 37 | 47 | -10 | -21.87% | 300 | 411 | 413 | -1 | -0.3% |
| | | WBR | 21 | 21 | 22 | 22 | 17.6 | 21.0 | -3.5 | -16.5% | В | С | 11 | 11 | -1 | -6.15% | 221 | 151 | 156 | -6 | -3.7% |
| | | WBT | 98 | 96 | 95 | 93 | 31.7 | 33.6 | -1.9 | -5.6% | С | С | 19 | 20 | -1 | -5.43% | 221 | 169 | 175 | -6 | -3.3% |
| | | All | 1912 | 1906 | 1917 | 1906 | 19.4 | 20.4 | -1.0 | -5.1% | В | С | 35 | 38 | -3 | -7.57% | | 413 | 415 | -1 | -0.3% |
| | | EBL | 11 | 11 | 17 | 16 | 13.6 | 10.5 | 3.1 | 29.4% | В | В | 0 | 0 | 0 | -50.00% | 390 | 15 | 22 | -7 | -33.0% |
| i | | EBT | 3 | 3 | 3 | 3 | 11.6 | 10.4 | 1.2 | 11.0% | В | В | 0 | 0 | 0 | -50.00% | 390 | 15 | 22 | -7 | -33.0% |
| | | NBL | 63 | 62 | 60 | 59 | 0.7 | 0.6 | 0.1 | 8.8% | Α | Α | 0 | 0 | 0 | 0.00% | 140 | 0 | 0 | 0 | 0.0% |
| | Duke Street at | NBR | 1 | 1 | 1 | 1 | 0.2 | 0.5 | -0.4 | -69.9% | Α | Α | 1 | 2 | -1 | -62.40% | 140 | 94 | 141 | -47 | -33.6% |
| 9 | Peabody Street ¹ (Unsignalized) | NBT | 1212 | 1207 | 1226 | 1218 | 2.3 | 3.1 | -0.9 | -27.2% | Α | Α | 1 | 2 | -1 | -62.40% | 140 | 94 | 141 | -47 | -33.6% |
| | (Onsignalizeu) | WBR | 12 | 12 | 13 | 13 | 10.9 | 10.5 | 0.3 | 3.3% | В | В | 0 | 0 | 0 | -30.43% | 543 | 30 | 41 | -11 | -26.4% |
| | | WBT | 33 | 32 | 32 | 31 | 13.1 | 14.7 | -1.6 | -10.7% | В | В | 0 | 0 | 0 | -30.43% | 543 | 30 | 41 | -11 | -26.4% |
| | | All | 1336 | 1328 | 1352 | 1341 | 2.7 | 3.5 | -0.8 | -23.0% | Α | Α | 0 | 1 | 0 | -60.49% | | 94 | 141 | -47 | -33.6% |



| Nede | Interception | Marrana | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Length | ı (ft) | | Max | (Queue | Length (ft) | |
|------|------------------------------------------------|----------|--------------|---------|---------------|----------------|-------|--------------|-------------|-----------------|-------|--------------|-------|--------------|--------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Bui Model | Demand | No-B Model | uild Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL1 | 0 | 0 | 0 | 0 | 0.7 | 0.7 | -0.1 | -7.9% | Α | Α | 5 | 0 | 5 | 0.00% | 370 | 309 | 0 | 309 | 0.0% |
| | | EBL2 | 4 | 5 | 4 | 5 | 11.4 | 8.9 | 2.5 | 27.5% | В | Α | 11 | 0 | 11 | 0.00% | 370 | 360 | 0 | 360 | 0.0% |
| 10 | Memorial Street at Duke Street ¹ | NBL | 14 | 15 | 20 | 20 | 5.3 | 3.6 | 1.7 | 47.2% | Α | Α | 8 | 4 | 4 | 109.72% | 213 | 247 | 209 | 38 | 18.0% |
| 10 | (Unsignalized) | NBT1 | 64 | 1265 | 60 | 1273 | 6.9 | 4.8 | 2.1 | 44.5% | Α | Α | 5 | 4 | 1 | 23.15% | 213 | 309 | 209 | 99 | 47.4% |
| | (* * 6 * * * * * * * * * * * * * * * * * | NBT2 | 1209 | 1203 | 1223 | 1275 | 4.7 | 2.8 | 1.9 | 66.2% | Α | Α | 11 | 4 | 7 | 180.25% | 213 | 360 | 209 | 150 | 71.7% |
| | | All | 1291 | 1285 | 1307 | 1298 | 4.8 | 2.9 | 1.9 | 64.1% | Α | Α | 8 | 2 | 6 | 239.79% | | 360 | 209 | 151 | 71.8% |
| | | EBL | 201 | 196 | 199 | 193 | 24.5 | 20.3 | 4.2 | 20.6% | С | С | 18 | 19 | -1 | -3.55% | 220 | 325 | 307 | 19 | 6.1% |
| | | EBT | 670 | 669 | 688 | 690 | 30.5 | 15.1 | 15.4 | 102.0% | С | В | 125 | 71 | 54 | 76.60% | 336 | 383 | 381 | 2 | 0.5% |
| | | NBL | 120 | 115 | 122 | 117 | 26.3 | 26.4 | -0.1 | -0.5% | С | С | 78 | 74 | 4 | 5.91% | 455 | 296 | 293 | 3 | 1.2% |
| 11 | Chapel Hill Street | NBR | 126 | 126 | 130 | 132 | 35.6 | 12.4 | 23.2 | 188.1% | D | В | 64 | 61 | 3 | 4.65% | 455 | 277 | 275 | 2 | 0.8% |
| 11 | at Duke Street ¹ | NBT | 1031 | 1026 | 1045 | 1039 | 28.2 | 27.8 | 0.3 | 1.2% | С | С | 78 | 74 | 4 | 5.91% | 455 | 296 | 293 | 3 | 1.2% |
| | | WBR | 55 | 58 | 58 | 61 | 25.5 | 13.6 | 12.0 | 88.3% | С | В | 71 | 30 | 40 | 133.29% | 275 | 378 | 291 | 87 | 30.0% |
| | | WBT | 359 | 361 | 384 | 383 | 27.2 | 16.5 | 10.6 | 64.4% | С | В | 87 | 45 | 41 | 91.17% | 275 | 408 | 321 | 87 | 27.2% |
| | | All | 2562 | 2551 | 2626 | 2615 | 28.6 | 21.1 | 7.5 | 35.4% | С | С | 74 | 53 | 21 | 39.16% | | 410 | 386 | 24 | 6.2% |
| | | EBR | 138 | 137 | 136 | 137 | 13.4 | 1.6 | 11.9 | 763.5% | В | Α | 89 | 0 | 89 | 52725.93% | 275 | 340 | 41 | 299 | 734.5% |
| | | EBT | 658 | 658 | 683 | 685 | 19.0 | 1.7 | 17.4 | 1048.7% | С | Α | 89 | 0 | 89 | 52725.93% | 275 | 340 | 41 | 299 | 734.5% |
| | Chapel Hill Street | NBL | 14 | 13 | 15 | 15 | 30.5 | 15.5 | 15.0 | 96.8% | D | С | 4 | 0 | 4 | 2157.14% | 460 | 99 | 31 | 68 | 218.7% |
| 12 | at Willard Street ¹ | NBR | 85 | 84 | 28 | 29 | 33.3 | 11.4 | 21.9 | 192.7% | D | В | 4 | 0 | 4 | 2157.14% | 460 | 99 | 31 | 68 | 218.7% |
| | (Unsignalized) | WBL | 99 | 95 | 51 | 47 | 14.6 | 7.9 | 6.8 | 86.2% | В | Α | 1 | 0 | 1 | 7866.67% | 142 | 125 | 17 | 108 | 643.2% |
| | | WBT | 400 | 406 | 427 | 429 | 5.3 | 1.0 | 4.3 | 414.6% | Α | Α | 1 | 0 | 1 | 5750.00% | 205 | 89 | 7 | 81 | 1100.8% |
| | | All | 1394 | 1393 | 1339 | 1342 | 15.2 | 2.0 | 13.2 | 650.2% | С | Α | 31 | 0 | 31 | 29464.71% | | 340 | 66 | 274 | 416.6% |
| | | EBR | 269 | 270 | 256 | 260 | 7.0 | 3.6 | 3.4 | 95.8% | Α | Α | 88 | 2 | 86 | 3542.78% | 206 | 284 | 153 | 131 | 85.5% |
| | | EBT | 474 | 472 | 454 | 454 | 8.6 | 3.8 | 4.9 | 128.3% | Α | Α | 97 | 9 | 88 | 929.12% | 206 | 301 | 200 | 101 | 50.6% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | Pettigrew Street | NBL | | | 87 | 86 | | 17.1 | | | | В | | 9 | | | 377 | | 168 | | |
| 13 | at Chapel Hill | NBR | | | 69 | 69 | | 8.9 | | | | Α | | 3 | | | 377 | | 139 | | |
| | Street ¹ | WBL | 39 | 37 | 42 | 42 | 31.0 | 13.7 | 17.3 | 126.8% | С | В | 60 | 17 | 43 | 257.02% | 222 | 291 | 206 | 85 | 41.3% |
| | | WBT | 499 | 501 | 391 | 390 | 22.3 | 8.5 | 13.8 | 162.9% | С | Α | 60 | 17 | 43 | 257.02% | 275 | 291 | 206 | 85 | 41.3% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 6.7 | N/A | N/A | N/A | Α | N/A | 10 | N/A | N/A | N/A | | 247 | N/A | N/A | N/A |
| | | All | 1293 | 1280 | 1299 | 1301 | 14.2 | 6.7 | 7.6 | 114.2% | В | Α | 53 | 10 | 43 | 445.23% | | 301 | 255 | 46 | 18.3% |



| | | | Volume | e (VPH) | Volume | e (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Length | ı (ft) | | Max | (Queue | Length (ft) | |
|------|-----------------------------------|----------|--------|---------|--------|---------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 0 | 0 | 14 | 13 | 0.0 | 32.4 | -32.4 | -100.0% | Α | С | 35 | 1 | 34 | 2519.16% | 150 | 246 | 39 | 207 | 529.9% |
| | | EBR | 117 | 116 | 35 | 36 | 21.5 | 11.1 | 10.4 | 94.2% | С | В | 23 | 10 | 12 | 122.36% | 785 | 218 | 137 | 80 | 58.3% |
| | | EBT | 83 | 83 | 123 | 121 | 36.4 | 20.8 | 15.6 | 74.8% | D | С | 35 | 20 | 16 | 79.65% | 785 | 246 | 159 | 86 | 54.2% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 3.0 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 125 | N/A | N/A | N/A |
| | | NBL | | | 21 | 21 | | 16.8 | | | | В | | 2 | | | 100 | | 65 | | |
| | | NBR | 90 | 89 | 7 | 7 | 4.2 | 9.2 | -5.0 | -54.4% | Α | Α | 2 | 7 | -5 | -71.69% | 148 | 68 | 153 | -84 | -55.3% |
| | Blackwell Street | NBT | 82 | 83 | 140 | 139 | 15.7 | 15.3 | 0.4 | 2.4% | В | В | 7 | 12 | -5 | -41.72% | 148 | 92 | 167 | -75 | -44.8% |
| 14 | at Pettigrew | SBL | 6 | 6 | 50 | 51 | 3.0 | 3.0 | 0.0 | -0.8% | Α | Α | 1 | 1 | 1 | 102.02% | 98 | 67 | 50 | 18 | 35.2% |
| | Street ² | SBR | | | 34 | 33 | | 1.0 | | | | Α | | 1 | | | 98 | | 50 | | |
| | | SBT | 94 | 91 | 171 | 164 | 2.5 | 1.4 | 1.1 | 74.9% | Α | Α | 1 | 1 | 1 | 102.02% | 98 | 67 | 50 | 18 | 35.2% |
| | | WBL | | | 7 | 9 | | 16.6 | | | | В | | 0 | | | 143 | | 25 | | |
| | | WBR | | | 49 | 51 | | 15.7 | | | | В | | 13 | | | 375 | | 278 | | |
| | | WBT | | | 211 | 205 | | 14.3 | | | | В | | 18 | | | 375 | | 291 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.1 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 64 | N/A | N/A | N/A |
| | | All | 500 | 468 | 861 | 850 | 15.2 | 11.9 | 3.3 | 27.6% | В | В | 12 | 7 | 5 | 66.81% | | 246 | 291 | -45 | -15.5% |
| | | EBL | 19 | 20 | 15 | 16 | 13.2 | 14.6 | -1.5 | -10.2% | В | В | 22 | 24 | -2 | -7.57% | 1081 | 148 | 155 | -8 | -5.0% |
| | | EBR | 3 | 2 | 6 | 7 | 4.8 | 5.0 | -0.2 | -3.0% | Α | Α | 30 | 32 | -2 | -4.94% | 263 | 193 | 202 | -8 | -4.1% |
| | | EBT | 348 | 351 | 384 | 385 | 14.9 | 16.2 | -1.3 | -7.9% | В | В | 22 | 24 | -2 | -7.57% | 1081 | 148 | 155 | -8 | -5.0% |
| 1 - | Blackwell Street | NBR | 2 | 2 | 7 | 7 | 0.3 | 4.0 | -3.7 | -93.6% | Α | Α | 0 | 13 | -13 | -99.26% | 98 | 9 | 135 | -126 | -93.4% |
| 15 | at Ramseur Street ¹ | NBT | 80 | 81 | 196 | 196 | 2.8 | 8.7 | -5.9 | -67.8% | Α | Α | 1 | 29 | -28 | -96.13% | 98 | 31 | 202 | -171 | -84.5% |
| | 30,000 | SBL | 34 | 34 | 26 | 27 | 13.0 | 16.5 | -3.5 | -21.1% | В | В | 9 | 28 | -20 | -69.61% | 200 | 155 | 284 | -129 | -45.4% |
| | | SBT | 98 | 95 | 248 | 241 | 12.2 | 15.0 | -2.8 | -18.4% | В | В | 9 | 28 | -20 | -69.61% | 200 | 155 | 284 | -129 | -45.4% |
| | | All | 583 | 585 | 883 | 879 | 12.5 | 14.0 | -1.4 | -10.3% | В | В | 13 | 25 | -12 | -48.06% | | 204 | 284 | -80 | -28.2% |



| | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Length | n (ft) | | Max | k Queue | Length (ft) | |
|------|------------------------------|----------|--------|---------|--------|--------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 44 | 42 | 55 | 52 | 30.7 | 28.2 | 2.5 | 8.7% | С | С | 49 | 44 | 5 | 10.71% | 158 | 322 | 301 | 21 | 6.8% |
| | | EBR | 15 | 16 | 50 | 50 | 19.7 | 21.7 | -2.0 | -9.3% | В | С | 39 | 34 | 5 | 13.92% | 158 | 306 | 285 | 21 | 7.2% |
| | | EBT | 244 | 236 | 180 | 176 | 26.7 | 26.7 | 0.1 | 0.3% | С | С | 49 | 44 | 5 | 10.71% | 158 | 322 | 301 | 21 | 6.8% |
| | | NBL | 6 | 6 | 20 | 20 | 9.5 | 7.2 | 2.3 | 32.0% | Α | Α | 4 | 6 | -2 | -28.73% | 202 | 93 | 92 | 1 | 1.0% |
| | | NBR | 5 | 7 | 8 | 9 | 6.1 | 3.9 | 2.2 | 57.2% | Α | Α | 2 | 3 | -1 | -37.39% | 202 | 84 | 83 | 1 | 1.1% |
| | Main Street at | NBT | 87 | 88 | 183 | 183 | 8.7 | 5.7 | 3.0 | 52.2% | Α | Α | 4 | 6 | -2 | -28.73% | 202 | 93 | 92 | 1 | 1.0% |
| 16 | Corcoran Street ² | SBL | 46 | 46 | 24 | 24 | 16.5 | 12.6 | 3.9 | 31.2% | В | В | 10 | 15 | -4 | -28.98% | 172 | 151 | 196 | -45 | -23.0% |
| | | SBR | 19 | 18 | 23 | 22 | 8.0 | 7.1 | 1.0 | 14.0% | Α | Α | 5 | 9 | -4 | -40.39% | 172 | 131 | 176 | -45 | -25.7% |
| | | SBT | 94 | 91 | 193 | 187 | 12.8 | 12.5 | 0.3 | 2.1% | В | В | 10 | 15 | -4 | -28.98% | 172 | 151 | 196 | -45 | -23.0% |
| | | WBL | 22 | 22 | 31 | 31 | 9.9 | 11.2 | -1.3 | -11.7% | Α | В | 11 | 10 | 1 | 6.59% | 310 | 188 | 106 | 82 | 77.9% |
| | | WBR | 76 | 76 | 40 | 42 | 6.1 | 6.2 | -0.1 | -1.8% | Α | Α | 6 | 4 | 1 | 30.40% | 310 | 166 | 84 | 82 | 97.6% |
| | | WBT | 246 | 240 | 179 | 174 | 7.5 | 8.7 | -1.2 | -13.6% | Α | Α | 11 | 10 | 1 | 6.59% | 310 | 188 | 106 | 82 | 77.9% |
| | | All | 904 | 888 | 986 | 970 | 15.2 | 13.9 | 1.3 | 9.0% | В | В | 17 | 17 | 0 | 0.07% | | 328 | 301 | 27 | 9.0% |
| | | EBR | 9 | 9 | 7 | 7 | 50.2 | 36.9 | 13.3 | 35.9% | D | D | 93 | 43 | 50 | 117.34% | 311 | 365 | 231 | 134 | 58.3% |
| | | EBT | 286 | 280 | 204 | 202 | 55.1 | 42.8 | 12.2 | 28.5% | E | D | 108 | 56 | 52 | 92.80% | 311 | 383 | 249 | 134 | 54.0% |
| | | SBL | 170 | 172 | 171 | 173 | 35.7 | 16.6 | 19.2 | 115.6% | D | В | 199 | 76 | 123 | 160.72% | 166 | 532 | 465 | 67 | 14.5% |
| 17 | Mangum Street | SBR | 18 | 17 | 7 | 7 | 13.0 | 5.3 | 7.7 | 144.0% | В | Α | 185 | 65 | 120 | 186.22% | 166 | 514 | 444 | 70 | 15.7% |
| 1, | at Main Street ¹ | SBT | 1081 | 1082 | 1096 | 1099 | 35.5 | 17.7 | 17.8 | 100.1% | D | В | 199 | 76 | 123 | 160.72% | 166 | 532 | 465 | 67 | 14.5% |
| | | WBL | 48 | 45 | 88 | 84 | 47.5 | 53.4 | -5.9 | -11.1% | D | D | 12 | 28 | -16 | -57.81% | 185 | 91 | 192 | -101 | -52.5% |
| | | WBT | 326 | 321 | 243 | 240 | 23.0 | 23.3 | -0.3 | -1.3% | С | С | 46 | 33 | 13 | 38.08% | 342 | 335 | 266 | 68 | 25.6% |
| | | All | 1938 | 1926 | 1817 | 1812 | 36.5 | 23.0 | 13.5 | 58.6% | D | С | 120 | 54 | 66 | 122.77% | | 532 | 465 | 67 | 14.5% |
| | | EBR | 107 | 108 | 116 | 117 | 52.6 | 45.6 | 7.0 | 15.3% | D | D | 41 | 40 | 0 | 0.81% | 318 | 179 | 143 | 36 | 24.8% |
| | Mangum Street | EBT | 276 | 279 | 298 | 302 | 16.0 | 20.8 | -4.8 | -23.1% | В | С | 41 | 40 | 0 | 0.81% | 318 | 179 | 143 | 36 | 24.8% |
| 18 | at Ramseur | SBL | 87 | 89 | 89 | 91 | 29.1 | 17.8 | 11.3 | 63.4% | С | В | 139 | 78 | 61 | 77.73% | 225 | 325 | 317 | 8 | 2.7% |
| | Street ¹ | SBT | 1051 | 1047 | 1101 | 1099 | 27.3 | 16.8 | 10.6 | 63.1% | С | В | 139 | 78 | 61 | 77.73% | 225 | 325 | 317 | 8 | 2.7% |
| | | All | 1521 | 1523 | 1605 | 1609 | 27.2 | 19.7 | 7.5 | 38.2% | С | В | 90 | 59 | 31 | 51.55% | | 325 | 317 | 8 | 2.7% |



| | | | Volume | e (VPH) | Volume | e (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Length | ı (ft) | | Max | (Queue | Length (ft) | |
|------|--------------------------------|----------|--------|---------|--------|---------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBR | 52 | 52 | 53 | 52 | 7.3 | 26.1 | -18.8 | -71.9% | Α | С | 20 | 23 | -3 | -14.08% | 375 | 189 | 188 | 2 | 0.8% |
| | | EBT | 126 | 126 | 127 | 127 | 36.6 | 40.8 | -4.2 | -10.2% | D | D | 31 | 43 | -12 | -28.11% | 375 | 210 | 224 | -14 | -6.3% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 8.6 | N/A | N/A | N/A | Α | N/A | 2 | N/A | N/A | N/A | | 200 | N/A | N/A | N/A |
| | NAS a success Character | SBL | 49 | 49 | 55 | 54 | 1.6 | 0.7 | 0.9 | 132.7% | А | Α | 1 | 0 | 1 | 752.17% | 82 | 102 | 52 | 51 | 98.4% |
| 19 | Mangum Street at Pettigrew | SBR | | | 67 | 67 | | 0.5 | | | | Α | | 0 | | | 82 | | 42 | | |
| | Street ¹ | SBT | 1105 | 1106 | 1095 | 1095 | 0.7 | 0.2 | 0.4 | 176.9% | Α | Α | 1 | 0 | 1 | 752.17% | 82 | 102 | 52 | 51 | 98.4% |
| | | WBL | 52 | 52 | 78 | 77 | 7.3 | 58.6 | -51.2 | -87.5% | Α | Е | 20 | 27 | -7 | -27.23% | 353 | 189 | 168 | 21 | 12.4% |
| | | WBT | | | 200 | 198 | | 37.5 | | | | D | | 44 | | | 400 | | 252 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.4 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 86 | N/A | N/A | N/A |
| | | All | 1361 | 1333 | 1675 | 1670 | 4.4 | 11.4 | -6.9 | -61.0% | Α | В | 8 | 20 | -11 | -57.60% | | 219 | 275 | -56 | -20.4% |
| | | EBL | 30 | 27 | 16 | 15 | 13.5 | 12.4 | 1.1 | 8.9% | В | В | 3 | 2 | 1 | 86.18% | 153 | 74 | 67 | 7 | 9.9% |
| | | EBR | 18 | 20 | 24 | 25 | 5.4 | 5.9 | -0.5 | -8.8% | Α | Α | 0 | 1 | -1 | -83.13% | 917 | 32 | 76 | -44 | -58.1% |
| | | EBT | 49 | 50 | 76 | 75 | 7.7 | 9.3 | -1.6 | -17.1% | Α | Α | 2 | 3 | -2 | -49.02% | 917 | 73 | 105 | -32 | -30.1% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.7 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 87 | N/A | N/A | N/A |
| | | NBL | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 155 | | 0 | | |
| | | NBR | 8 | 8 | 34 | 34 | 11.5 | 8.2 | 3.3 | 40.5% | В | Α | 4 | 5 | -1 | -19.42% | 822 | 86 | 114 | -28 | -24.6% |
| | Pettigrew Street | NBT | 66 | 68 | 100 | 100 | 26.5 | 17.6 | 8.9 | 50.9% | С | В | 10 | 11 | -1 | -7.36% | 822 | 100 | 128 | -28 | -21.7% |
| 20 | at Dillard Street ² | SBL | 38 | 37 | 46 | 45 | 28.5 | 21.3 | 7.2 | 34.0% | С | С | 31 | 27 | 4 | 14.39% | 264 | 216 | 214 | 1 | 0.7% |
| | | SBR | | | 101 | 98 | | 9.9 | | | | Α | | 18 | | | 264 | | 187 | | |
| | | SBT | 110 | 109 | 110 | 110 | 26.9 | 18.5 | 8.4 | 45.2% | С | В | 31 | 27 | 4 | 14.39% | 264 | 216 | 214 | 1 | 0.7% |
| | | WBL | 36 | 37 | 25 | 25 | 8.3 | 6.1 | 2.3 | 37.6% | Α | Α | 2 | 2 | 0 | 19.59% | 695 | 93 | 111 | -17 | -15.8% |
| | | WBR | 45 | 43 | 17 | 18 | 8.4 | 3.6 | 4.8 | 133.4% | Α | Α | 2 | 1 | 1 | 192.56% | 695 | 93 | 96 | -3 | -3.2% |
| | | WBT | | | 88 | 87 | | 6.0 | | | | Α | | 2 | | | 695 | | 111 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 419 | 399 | 638 | 632 | 18.1 | 12.3 | 5.8 | 47.5% | В | В | 10 | 8 | 2 | 18.71% | | 220 | 214 | 5 | 2.4% |



| No. do | | | Volume | (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Length | ı (ft) | | Ma | x Queue | Length (ft) | |
|--------|----------------------------------|----------|--------|--------|--------|--------|-------|--------------|-------------|-----------------|-------|--------------|-------|--------------|--------------|-----------------|------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Bui | | No-B | | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space | Build | No- Build | Difference | Difference % |
| | | | Model | Demand | Model | Demand | | | | | | Bullu | | | | | Available | | | | |
| | | EBL | 10 | 9 | 8 | 7 | 57.4 | 61.4 | -4.1 | -6.6% | E | E | 3 | 2 | 0 | 6.77% | 210 | 43 | 44 | -1 | -2.0% |
| | | EBR | 6 | 6 | 26 | 26 | 4.6 | 5.6 | -1.0 | -17.4% | A | A | 0 | 0 | 0 | 0.00% | 273 | 0 | 0 | 0 | 0.0% |
| | | EBT | 53 | 53 | 59 | 57 | 36.9 | 53.9 | -17.1 | -31.6% | D | D | 11 | 18 | -7 | -41.23% | 696 | 105 | 133 | -29 | -21.4% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | 3 | 3 | 35 | 35 | 8.5 | 5.9 | 2.6 | 44.0% | Α | Α | 11 | 4 | 6 | 139.49% | 70 | 143 | 145 | -2 | -1.6% |
| | | NBR | 46 | 45 | 58 | 61 | 0.4 | 0.3 | 0.1 | 43.9% | Α | Α | 46 | 46 | 0 | 0.20% | 70 | 140 | 140 | 1 | 0.6% |
| | Fayetteville | NBT | 365 | 371 | 382 | 388 | 2.7 | 1.3 | 1.4 | 112.7% | Α | Α | 11 | 4 | 6 | 139.49% | 70 | 143 | 145 | -2 | -1.6% |
| 21 | Street at | SBL | 58 | 58 | 42 | 41 | 40.3 | 21.1 | 19.2 | 90.8% | D | С | 15 | 5 | 9 | 178.62% | 250 | 226 | 124 | 102 | 82.9% |
| | Pettigrew Street ¹ | SBR | 1 | 1 | 7 | 7 | 22.3 | 13.4 | 9.0 | 67.1% | С | В | 86 | 32 | 54 | 165.75% | 400 | 358 | 207 | 152 | 73.5% |
| | | SBT | 434 | 432 | 449 | 445 | 42.5 | 22.4 | 20.1 | 90.0% | D | С | 86 | 52 | 35 | 67.07% | 400 | 358 | 250 | 108 | 43.3% |
| | | WBL | 93 | 96 | 87 | 90 | 49.0 | 59.8 | -10.8 | -18.0% | D | E | 21 | 28 | -7 | -24.97% | 100 | 193 | 200 | -7 | -3.3% |
| | | WBR | 103 | 108 | 45 | 50 | 33.2 | 31.3 | 1.9 | 6.2% | С | С | 49 | 31 | 18 | 60.02% | 1570 | 345 | 254 | 91 | 35.7% |
| | | WBT | 94 | 90 | 127 | 127 | 52.2 | 47.2 | 5.0 | 10.5% | D | D | 49 | 44 | 5 | 10.52% | 1570 | 345 | 277 | 68 | 24.5% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 1277 | 1272 | 1323 | 1334 | 29.2 | 21.3 | 7.9 | 36.9% | С | С | 28 | 22 | 5 | 23.66% | | 388 | 292 | 96 | 32.7% |
| | | NBL | 228 | 227 | 186 | 185 | 26.4 | 14.2 | 12.2 | 86.2% | С | В | 35 | 13 | 22 | 166.84% | 277 | 266 | 150 | 116 | 77.0% |
| | | NBT | 322 | 328 | 359 | 367 | 20.7 | 11.7 | 9.0 | 76.4% | С | В | 24 | 14 | 10 | 66.88% | 286 | 213 | 137 | 76 | 55.0% |
| | Favottovilla | SBR | 43 | 44 | 39 | 40 | 1.0 | 2.1 | -1.0 | -50.9% | Α | Α | 6 | 9 | -3 | -35.83% | 70 | 137 | 156 | -18 | -11.8% |
| 22 | Fayetteville Street at Jackie | SBT | 490 | 490 | 524 | 521 | 4.6 | 6.8 | -2.2 | -31.7% | Α | Α | 11 | 16 | -5 | -30.05% | 70 | 156 | 172 | -16 | -9.4% |
| | Robinson Drive ¹ | WBL | 172 | 169 | 149 | 144 | 40.1 | 40.5 | -0.4 | -0.9% | D | D | 45 | 39 | 5 | 14.01% | 345 | 264 | 222 | 42 | 19.0% |
| | | WBR | 91 | 91 | 115 | 117 | 9.3 | 6.7 | 2.6 | 38.2% | Α | Α | 35 | 33 | 2 | 5.60% | 345 | 251 | 217 | 34 | 15.6% |
| | | WBT | 13 | 13 | 13 | 13 | 38.8 | 36.8 | 2.0 | 5.5% | D | D | 45 | 39 | 5 | 14.01% | 603 | 264 | 222 | 42 | 19.0% |
| | | All | 1361 | 1362 | 1385 | 1387 | 17.1 | 12.9 | 4.2 | 33.0% | В | В | 29 | 24 | 5 | 21.78% | | 285 | 224 | 61 | 27.3% |
| | | EBL | 43 | 44 | 31 | 33 | 49.5 | 45.3 | 4.2 | 9.3% | D | D | 13 | 8 | 5 | 54.25% | 1260 | 102 | 87 | 15 | 17.1% |
| | | EBR | 143 | 139 | 133 | 130 | 6.9 | 6.6 | 0.3 | 4.2% | Α | Α | 2 | 1 | 1 | 122.63% | 1195 | 69 | 53 | 15 | 28.6% |
| | Morehead | EBT | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 13 | 8 | 5 | 54.25% | 1260 | 102 | 87 | 15 | 17.1% |
| 23 | Avenue at | NBR | 20 | 20 | 18 | 18 | 2.1 | 1.8 | 0.3 | 16.7% | Α | Α | 1 | 1 | 0 | 22.22% | 389 | 64 | 63 | 1 | 2.4% |
| 23 | Fayetteville | NBT | 507 | 511 | 514 | 519 | 2.9 | 2.6 | 0.3 | 11.2% | Α | Α | 3 | 3 | 0 | 5.50% | 389 | 82 | 81 | 1 | 1.8% |
| | Street ¹ | SBL | 99 | 93 | 74 | 71 | 4.8 | 3.2 | 1.6 | 50.7% | Α | Α | 1 | 0 | 1 | 240.98% | 255 | 90 | 53 | 37 | 68.6% |
| | | SBT | 564 | 566 | 598 | 594 | 2.3 | 1.5 | 0.8 | 52.9% | Α | Α | 3 | 2 | 1 | 89.92% | 275 | 159 | 141 | 17 | 12.2% |
| | | All | 1376 | 1373 | 1368 | 1365 | 4.7 | 3.5 | 1.2 | 32.7% | Α | Α | 5 | 3 | 2 | 55.30% | | 168 | 141 | 27 | 19.0% |



| No. do | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Lengtl | ı (ft) | | Max | k Queue | Length (ft) | |
|--------|-------------------------------|----------|--------|---------|--------|--------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bui | ild | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 0 | 5 | -5 | -100.00% | 155 | 0 | 107 | -107 | -100.0% |
| | | EBR | 7 | 7 | 13 | 13 | 7.4 | 3.2 | 4.2 | 134.0% | Α | Α | 5 | 0 | 5 | 86100.00% | 1570 | 122 | 4 | 118 | 2959.5% |
| | | EBT | 151 | 149 | 145 | 146 | 7.4 | 6.2 | 1.3 | 20.3% | Α | Α | 5 | 5 | 1 | 17.92% | 1570 | 122 | 107 | 15 | 13.9% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 21 | 7 | 13 | 178.37% | 625 | 213 | 112 | 101 | 90.0% |
| | | NBR | 104 | 102 | 73 | 73 | 14.9 | 9.8 | 5.1 | 52.3% | В | Α | 14 | 4 | 11 | 300.69% | 625 | 198 | 96 | 102 | 106.0% |
| | Pettigrew Street | NBT | 96 | 93 | 51 | 51 | 27.1 | 19.6 | 7.5 | 38.0% | С | В | 21 | 7 | 13 | 178.37% | 625 | 213 | 112 | 101 | 90.0% |
| 24 | at Grant Street ² | SBL | 93 | 90 | 89 | 86 | 34.0 | 25.2 | 8.8 | 35.0% | С | С | 25 | 16 | 9 | 52.81% | 266 | 221 | 199 | 22 | 11.0% |
| | | SBR | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 25 | 7 | 18 | 272.70% | 266 | 221 | 181 | 39 | 21.8% |
| | | SBT | 51 | 50 | 69 | 68 | 31.7 | 23.0 | 8.7 | 37.7% | С | С | 25 | 16 | 9 | 52.81% | 266 | 221 | 199 | 22 | 11.0% |
| | | WBL | 67 | 69 | 127 | 127 | 8.9 | 7.8 | 1.1 | 14.0% | Α | Α | 2 | 4 | -2 | -47.59% | 70 | 67 | 86 | -19 | -22.2% |
| | | WBR | 122 | 123 | 121 | 121 | 10.9 | 5.4 | 5.6 | 103.3% | В | Α | 20 | 6 | 14 | 252.87% | 193 | 298 | 163 | 135 | 82.8% |
| | | WBT | 287 | 294 | 259 | 267 | 10.3 | 7.0 | 3.2 | 46.2% | В | Α | 20 | 8 | 12 | 141.08% | 193 | 300 | 174 | 126 | 72.6% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 989 | 977 | 948 | 952 | 15.2 | 10.5 | 4.7 | 44.3% | В | В | 13 | 7 | 6 | 85.69% | | 308 | 215 | 93 | 43.2% |
| | | EBR | 74 | 73 | 72 | 72 | 2.1 | 2.7 | -0.6 | -21.4% | Α | Α | 0 | 0 | 0 | 0.00% | 206 | 0 | 0 | 0 | 0.0% |
| | | EBT | 290 | 282 | 290 | 287 | 2.4 | 2.9 | -0.5 | -17.3% | Α | Α | 0 | 0 | 0 | 0.00% | 206 | 0 | 0 | 0 | 0.0% |
| | Gann Street at | NBL | 101 | 105 | 99 | 102 | 9.8 | 9.4 | 0.4 | 3.7% | Α | Α | 0 | 0 | 0 | 71.43% | 248 | 54 | 45 | 9 | 18.9% |
| 25 | Pettigrew Street ² | NBR | 11 | 11 | 12 | 12 | 8.0 | 7.1 | 0.9 | 12.4% | Α | Α | 0 | 0 | 0 | 71.43% | 248 | 54 | 45 | 9 | 18.9% |
| | (Unsignalized) | WBL | 21 | 21 | 23 | 23 | 8.1 | 8.4 | -0.3 | -3.5% | Α | Α | 0 | 0 | 0 | 0.00% | 367 | 9 | 8 | 1 | 7.3% |
| | | WBT | 421 | 426 | 432 | 437 | 0.4 | 0.4 | 0.0 | 7.6% | Α | Α | 0 | 0 | 0 | 0.00% | 367 | 0 | 0 | 0 | 0.0% |
| | | All | 918 | 918 | 929 | 933 | 2.5 | 2.6 | -0.1 | -4.6% | Α | Α | 0 | 0 | 0 | 25.00% | | 54 | 45 | 9 | 18.9% |
| | | EBL | 61 | 63 | 69 | 69 | 59.4 | 57.6 | 1.8 | 3.2% | E | E | 25 | 26 | -1 | -5.30% | 196 | 212 | 217 | -5 | -2.4% |
| | | EBR | 183 | 182 | 182 | 182 | 12.9 | 13.1 | -0.2 | -1.2% | В | В | 16 | 18 | -1 | -6.92% | 196 | 201 | 206 | -5 | -2.6% |
| | | NBL | 13 | 13 | 14 | 14 | 18.6 | 18.4 | 0.2 | 1.2% | В | В | 31 | 33 | -2 | -7.04% | 300 | 254 | 261 | -7 | -2.8% |
| | | NBT | 873 | 870 | 878 | 875 | 11.2 | 12.0 | -0.7 | -5.9% | В | В | 31 | 33 | -2 | -7.04% | 528 | 254 | 261 | -7 | -2.8% |
| 26 | Alston Avenue at | SBR | 48 | 46 | 48 | 46 | 12.2 | 12.2 | 0.0 | -0.3% | В | В | 70 | 74 | -4 | -5.83% | 190 | 554 | 579 | -25 | -4.3% |
| 20 | Gann Street ¹ | SBT | 1441 | 1438 | 1443 | 1440 | 13.4 | 14.0 | -0.6 | -4.1% | В | В | 72 | 76 | -4 | -5.74% | 1037 | 557 | 582 | -25 | -4.3% |
| | | WBL | 425 | 457 | 431 | 457 | 61.0 | 59.5 | 1.4 | 2.4% | E | E | 372 | 370 | 2 | 0.50% | 188 | 686 | 685 | 1 | 0.1% |
| | | WBR | 296 | 321 | 294 | 315 | 43.3 | 41.9 | 1.4 | 3.4% | D | D | 147 | 128 | 20 | 15.48% | 1000 | 653 | 652 | 1 | 0.1% |
| | | WBT | 47 | 52 | 48 | 52 | 62.2 | 58.9 | 3.3 | 5.6% | E | E | 163 | 142 | 21 | 14.67% | 1000 | 677 | 676 | 1 | 0.1% |
| | | All | 3386 | 3442 | 3407 | 3450 | 22.9 | 23.1 | -0.2 | -0.8% | С | С | 103 | 100 | 3 | 2.95% | | 690 | 698 | -8 | -1.1% |



| Nada | | | Volume | (VPH) | Volume | · (VPH) | | Dela | y (Seconds) | | LC | os | | Avg | Queue Length | ı (ft) | | Max | k Queue | Length (ft) | |
|------|-------------------------------|----------|--------|--------|--------|---------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bui | ld | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 86 | 86 | 90 | 90 | 49.7 | 57.0 | -7.2 | -12.7% | D | Е | 31 | 38 | -7 | -19.53% | 220 | 197 | 172 | 25 | 14.3% |
| | | EBT | 89 | 89 | 91 | 91 | 37.8 | 43.3 | -5.5 | -12.6% | D | D | 31 | 38 | -7 | -19.53% | 288 | 197 | 172 | 25 | 14.3% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | | | 189 | 188 | | 9.1 | | | | Α | | 50 | | | 541 | | 439 | | |
| 27 | Roxboro Street at | NBR | 8 | 8 | 25 | 24 | 5.3 | 2.6 | 2.7 | 102.9% | А | Α | 83 | 38 | 46 | 121.37% | 541 | 547 | 408 | 139 | 34.0% |
| 27 | Pettigrew Street ¹ | NBT | 1950 | 1973 | 1501 | 1524 | 12.2 | 9.0 | 3.2 | 35.4% | В | Α | 94 | 50 | 44 | 88.63% | 541 | 569 | 439 | 130 | 29.7% |
| | | WBR | | | 100 | 98 | | 67.6 | | | | Е | | 80 | | | 916 | | 349 | | |
| | | WBT | | | 88 | 87 | | 81.0 | | | | F | | 94 | | | 916 | | 368 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 44 | N/A | N/A | N/A |
| | | All | 2157 | 2156 | 2085 | 2102 | 14.6 | 18.4 | -3.8 | -20.5% | В | В | 48 | 55 | -8 | -13.97% | | 569 | 484 | 84 | 17.4% |
| | | EBT LRT | 6 | 6 | | | 0.0 | | | | Α | | 0 | | | | | 0 | | | |
| | LRT at Buchanan | NBT | 277 | 263 | | | 3.3 | | | | Α | | 4 | | | | | 155 | | | |
| 28 | Boulevard ² | SBT | 516 | 445 | | | 7.0 | | | | Α | | 23 | | | | | 437 | | | |
| | 300.000.0 | WBT LRT | 6 | 6 | | | 5.1 | | | | Α | | 9 | | | | | 234 | | | |
| | | All | 805 | 708 | | | 5.7 | | | | Α | | 9 | | | | | 437 | | | |
| | Downtown Durham Corridor | EB LRT | 6 | 6 | | | 23.1 | | | | | | | | | | | | | | |
| | Downtown Durham Corridor | WB LRT | 6 | 6 | | | 23.4 | | | | | | | | | | | | | | |
| | | All | 40355 | 40770 | 40971 | 41136 | 21.0 | 17.2 | | | С | В | 37 | 30 | 7 | 22.37% | | 851 | 747 | 104 | 13.9% |

^{1 -} NCDOT Traffic Impact Criteria is applied

2 - City of Durham Traffic Impact Criteria is applied

Indicates LRT Movement
Indicates Traffic Impact
Indicates Traffic Impact below
Mid-D

Build Max Queue length exceeds No-Build and Storage Space by more than 10 feet



Table 10: D-O LRT: Downtown Durham Segment – VISSIM Intersection Analysis Output Summary - 2040 Build Option 1 vs. 2040 No-Build PM Peak Hour 5:00 - 6:00 PM

| | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | os | | Avg (| Queue Length | (ft) | | Max | (Queue | Length (ft) | |
|------|-------------------------------------------|----------|--------|---------|--------|--------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 53 | 61 | 52 | 63 | 44.7 | 41.1 | 3.6 | 8.7% | D | D | 8 | 8 | 0 | -0.25% | 625 | 74 | 77 | -3 | -3.9% |
| | | EBR | 45 | 52 | 48 | 58 | 60.2 | 50.5 | 9.6 | 19.1% | Е | D | 304 | 284 | 20 | 7.16% | 900 | 457 | 453 | 4 | 0.9% |
| | | EBT | 518 | 592 | 498 | 599 | 66.2 | 53.8 | 12.4 | 23.0% | Е | D | 318 | 298 | 21 | 6.91% | 900 | 474 | 470 | 4 | 0.9% |
| | | NBL | 25 | 47 | 18 | 47 | 32.6 | 32.4 | 0.2 | 0.5% | С | С | 192 | 116 | 76 | 65.51% | 106 | 255 | 185 | 71 | 38.2% |
| | | NBR | 206 | 327 | 140 | 302 | 37.6 | 48.9 | -11.4 | -23.2% | D | D | 170 | 100 | 70 | 69.59% | 106 | 231 | 165 | 66 | 40.0% |
| | NAsta Charatan | NBT | 158 | 250 | 127 | 300 | 41.3 | 50.8 | -9.5 | -18.7% | D | D | 192 | 116 | 76 | 65.51% | 106 | 255 | 185 | 71 | 38.2% |
| 1 | Main Street at 9th Street ¹ | SBL | 244 | 270 | 219 | 240 | 184.3 | 65.2 | 119.2 | 182.8% | F | Е | 378 | 181 | 197 | 108.63% | 330 | 609 | 503 | 107 | 21.2% |
| | Juisueet | SBR | 71 | 74 | 65 | 76 | 60.3 | 32.7 | 27.5 | 84.1% | Е | С | 350 | 157 | 193 | 123.37% | 330 | 580 | 472 | 108 | 22.9% |
| | | SBT | 141 | 147 | 180 | 198 | 66.9 | 39.5 | 27.4 | 69.3% | Е | D | 378 | 181 | 197 | 108.63% | 330 | 609 | 503 | 107 | 21.2% |
| | | WBL | 214 | 263 | 168 | 216 | 46.2 | 70.0 | -23.8 | -34.0% | D | Е | 106 | 158 | -52 | -33.03% | 190 | 388 | 392 | -4 | -1.0% |
| | | WBR | 230 | 286 | 187 | 245 | 18.9 | 14.2 | 4.6 | 32.6% | В | В | 171 | 149 | 22 | 14.73% | 300 | 374 | 373 | 1 | 0.3% |
| | | WBT | 357 | 441 | 347 | 452 | 22.5 | 17.7 | 4.9 | 27.5% | С | В | 186 | 163 | 23 | 14.16% | 300 | 396 | 395 | 1 | 0.3% |
| | | All | 2263 | 2810 | 2048 | 2796 | 59.4 | 43.4 | 16.0 | 36.7% | E | D | 229 | 159 | 70 | 44.11% | | 609 | 529 | 80 | 15.2% |
| | | EBL | 145 | 174 | 135 | 176 | 15.9 | 17.9 | -2.0 | -11.4% | С | С | 105 | 103 | 2 | 2.10% | 60 | 327 | 321 | 6 | 1.9% |
| | | EBT | 825 | 1015 | 726 | 965 | 18.5 | 16.9 | 1.6 | 9.2% | С | С | 105 | 103 | 2 | 2.10% | 290 | 327 | 321 | 6 | 1.9% |
| | Main Street at | SBL | 30 | 32 | 27 | 33 | 180.9 | 225.0 | -44.2 | -19.6% | F | F | 81 | 117 | -36 | -31.16% | 370 | 204 | 203 | 1 | 0.6% |
| 2 | Iredell Street ¹ | SBR | 79 | 80 | 67 | 77 | 141.2 | 175.0 | -33.8 | -19.3% | F | F | 81 | 117 | -36 | -31.16% | 370 | 204 | 203 | 1 | 0.6% |
| | (Unsignalized) | WBR | 17 | 22 | 20 | 25 | 7.6 | 11.6 | -4.0 | -34.2% | Α | В | 65 | 101 | -36 | -35.53% | 290 | 416 | 418 | -2 | -0.6% |
| | | WBT | 724 | 910 | 635 | 836 | 13.8 | 15.7 | -1.9 | -12.1% | В | С | 65 | 101 | -36 | -35.53% | 290 | 416 | 418 | -2 | -0.6% |
| | | All | 1821 | 2233 | 1610 | 2112 | 24.4 | 26.8 | -2.3 | -8.7% | С | D | 84 | 107 | -23 | -21.85% | | 416 | 418 | -2 | -0.6% |



| | | | Volume | (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | OS | | Avg | Queue Length | ı (ft) | | Ma | x Queue | Length (ft) | |
|------|----------------------------|----------|--------|--------|--------|--------|-------|--------------|-------------|-----------------|-------|--------------|-------|-------------|--------------|-----------------|------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Bui | - | No-B | | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No Build | Difference | Difference % | Storage Space | Build | No- Build | Difference | Difference % |
| | | | Model | Demand | Model | Demand | | Bullu | | /0 | | Бини | | Dullu | | /6 | Available | | Bullu | | /6 |
| | | EBL | 96 | 118 | 87 | 113 | 127.1 | 37.9 | 89.2 | 235.4% | F | D | 300 | 271 | 29 | 10.86% | 198 | 459 | 454 | 5 | 1.1% |
| | | EBR | 269 | 323 | 196 | 255 | 8.8 | 7.9 | 0.9 | 11.9% | Α | Α | 1 | 3 | -2 | -65.96% | 317 | 95 | 114 | -19 | -16.5% |
| | | EBT | 496 | 606 | 477 | 630 | 39.8 | 34.4 | 5.5 | 16.0% | D | С | 311 | 318 | -7 | -2.19% | 317 | 474 | 469 | 5 | 1.0% |
| | | NBL | 280 | 312 | 175 | 283 | 30.3 | 51.0 | -20.7 | -40.6% | С | D | 120 | 209 | -89 | -42.74% | 121 | 221 | 267 | -46 | -17.2% |
| | | NBR | 164 | 182 | 131 | 185 | 1.7 | 1.5 | 0.2 | 12.0% | Α | Α | 2 | 101 | -99 | -98.26% | 116 | 113 | 251 | -138 | -55.0% |
| | Main Street at | NBT | 331 | 352 | 318 | 448 | 15.7 | 16.1 | -0.5 | -2.8% | В | В | 120 | 209 | -89 | -42.74% | 121 | 221 | 267 | -46 | -17.2% |
| 3 | Broad Street ¹ | SBL | 108 | 126 | 80 | 116 | 106.9 | 107.6 | -0.7 | -0.7% | F | F | 104 | 86 | 18 | 20.65% | 130 | 562 | 561 | 1 | 0.2% |
| | Broad Street | SBR | 90 | 105 | 42 | 65 | 69.5 | 78.8 | -9.3 | -11.8% | E | E | 310 | 339 | -29 | -8.63% | 450 | 531 | 528 | 3 | 0.6% |
| | | SBT | 483 | 573 | 437 | 625 | 80.7 | 93.0 | -12.2 | -13.2% | F | F | 349 | 375 | -25 | -6.78% | 450 | 573 | 569 | 3 | 0.6% |
| | | WBL | 137 | 187 | 146 | 167 | 251.7 | 49.3 | 202.4 | 410.7% | F | D | 433 | 49 | 384 | 784.76% | 412 | 676 | 348 | 329 | 94.5% |
| | | WBR | 95 | 129 | 77 | 87 | 52.8 | 48.9 | 3.9 | 7.9% | D | D | 178 | 263 | -85 | -32.45% | 560 | 588 | 591 | -2 | -0.4% |
| | | WBT | 372 | 515 | 443 | 513 | 58.9 | 53.7 | 5.1 | 9.6% | Е | D | 222 | 326 | -104 | -31.89% | 560 | 671 | 673 | -2 | -0.3% |
| | | All | 2919 | 3528 | 2609 | 3487 | 57.0 | 47.3 | 9.7 | 20.5% | E | D | 204 | 212 | -8 | -3.87% | | 677 | 674 | 3 | 0.5% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 5.6 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBR | 7 | 10 | 35 | 82 | 74.3 | 128.0 | -53.7 | -41.9% | F | F | 212 | 278 | -66 | -23.62% | 720 | 305 | 362 | -57 | -15.7% |
| | | NBT | 376 | 609 | 257 | 596 | 107.5 | 141.6 | -34.1 | -24.1% | F | F | 212 | 278 | -66 | -23.62% | 720 | 305 | 362 | -57 | -15.7% |
| | Pettigrew Street | SBL | 18 | 22 | 33 | 42 | 5.8 | 12.4 | -6.6 | -53.5% | Α | В | 3 | 22 | -20 | -88.44% | 105 | 138 | 180 | -42 | -23.5% |
| 4 | at 9th Street ¹ | SBT | 382 | 440 | 362 | 430 | 0.6 | 1.9 | -1.3 | -69.8% | Α | Α | 3 | 22 | -20 | -88.44% | 105 | 138 | 180 | -42 | -23.5% |
| | (Unsignalized) | WBL | 76 | 87 | 18 | 26 | 387.5 | 19.7 | 367.8 | 1871.9% | F | С | 182 | 1 | 180 | 12335.04% | 185 | 323 | 63 | 260 | 413.0% |
| | | WBR | 12 | 15 | 38 | 53 | 339.7 | 46.6 | 293.1 | 628.3% | F | E | 182 | 1 | 180 | 12335.04% | 185 | 323 | 63 | 260 | 413.0% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 883 | 1183 | 743 | 1229 | 79.0 | 59.4 | 19.6 | 33.1% | F | F | 99 | 100 | -1 | -1.31% | | 328 | 362 | -34 | -9.3% |



| | | | Volume | e (VPH) | Volume | (VPH) | | Delay | y (Seconds) | | LC | OS | | Avg | Queue Length | ı (ft) | | Max | Queue | Length (ft) | |
|------|------------------------------------|----------|-----------|-----------|-----------|-----------|--------------|--------------|-------------|---------------|--------|----------|------------|-----------|--------------|-------------------|------------------|------------|------------|-------------|----------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | Build | No- | Difference | Difference | Build | No- | Build | No | Difference | Difference | Storage Space | Build | No- | Difference | Difference |
| | | | Model | Demand | Model | Demand | 24.16 | Build | | % | | Build | 2 4.11 4.1 | Build | | % | Available | 30.110. | Build | | % |
| | | EBL | | | 29 | 53 | | 373.3 | | | | F | | 638 | | | 506 | | 840 | | |
| | | EBR | | | 89 | 166 | | 316.2 | | | | F | | 638 | | | 506 | | 840 | | |
| | | EBT | | | 2 | 3 | | 345.7 | | | | F | | 638 | | | 506 | | 840 | | |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | | | 33 | 48 | | 118.5 | | | | F | | 187 | | | 443 | | 395 | | |
| | | NBR | | | 7 | 9 | | 67.0 | | | | F | | 658 | | | 443 | | 784 | | |
| | Pettigrew Street | NBT | 775 | 846 | 574 | 820 | 94.7 | 122.4 | -27.7 | -22.6% | F | F | 527 | 715 | -188 | -26.25% | 443 | 827 | 841 | -14 | -1.7% |
| 5 | at Swift Avenue ¹ | SBL | | | 11 | 16 | | 133.0 | | | | F | | 30 | | | 137 | | 222 | | |
| | (Unsignalized) | SBR | | | 32 | 45 | | 1.3 | | | | Α | | 30 | | | 137 | | 222 | | |
| | | SBT | 888 | 1083 | 734 | 986 | 0.9 | 1.0 | -0.1 | -12.6% | Α | Α | 3 | 30 | -27 | -90.11% | 137 | 164 | 222 | -58 | -26.3% |
| | | WBL | | | 9 | 17 | | 854.1 | | | | F | | 369 | | | 515 | | 502 | | |
| | | WBR | | | 22 | 43 | | 941.6 | | | | F | | 369 | | | 515 | | 502 | | |
| | | WBT | | | 3 | 6 | | 928.8 | | | | F | | 369 | | | 515 | | 502 | | , |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.7 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 87 | N/A | N/A | N/A |
| | | All | 1676 | 1929 | 1544 | 2212 | 44.1 | 92.5 | -48.4 | -52.3% | E | F | 133 | 389 | -257 | -65.94% | | 827 | 847 | -20 | -2.4% |
| | | EBL | 182 | 184 | 183 | 187 | 119.2 | 118.9 | 0.3 | 0.3% | F | F | 339 | 343 | -4 | -1.22% | 215 | 611 | 610 | 1 | 0.2% |
| | | EBR | 64 | 65 | 68 | 69 | 11.5 | 12.4 | -0.9 | -7.1% | В | В | 0 | 0 | 0 | 0.00% | 267 | 0 | 0 | 0 | 0.0% |
| | | EBT | 540 | 549 | 541 | 554 | 24.1 | 24.5 | -0.4 | -1.7% | C | C | 15 | 16 | -1 | -4.79% | 607 | 474 | 462 | 13 | 2.7% |
| | | NBL | 76 | 94 | 72 | 97 | 119.7 | 117.9 | 1.8 | 1.5% | F | F | 90 | 83 | 7 | 8.51% | 70 | 191 | 211 | -20 | -9.5% |
| | | NBR | 55 | 66 | 52 | 67 | 18.9 | 18.6 | 0.3 | 1.8% | В | В | 0 | 0 | 0 | 3.57% | 120 | 10 | 8 | 2 | 25.2% |
| | Main Street at | NBT | 274 | 339 | 256 | 350 | 55.6 | 60.1 | -4.5 | -7.5% | E | E | 106 | 109 | -3 | -2.61% | 433 | 199 | 222 | -23 | -10.6% |
| 6 | Buchanan Boulevard ¹ | SBL | 101 | 109 | 98 | 107 | 151.0 | 154.1 | -3.1 | -2.0% | F | F | 167 | 165 | 2 | 1.12% | 130 | 471 | 475 | -4 | -0.8% |
| | Bodicvara | SBR | 175 | 180 | 170 | 179 | 41.5 | 43.1 | -1.5 | -3.6% | D | D | 8 | 10 | -2 | -20.79% | 130 | 290 | 255 | 34 | 13.5% |
| | | SBT | 283 | 310 | 280 | 312 | 92.9 94.8 | 95.5 | -2.5 1.3 | -2.7% | F F | F | 269 | 277 | -8 | -2.87% -13.02% | 400 | 471 | 474 | -3 | -0.5% |
| | | WBL | 32 182 | 34 183 | 35 181 | 36 181 | | 93.5 26.1 | | 1.4% -0.1% | - | F | 38 | 44 229 | -6 4 | 1.81% | 382 | 484 620 | 516 621 | -32 | -6.2% -0.1% |
| | | | 698 | 685 | 701 | 689 | 26.1 27.7 | 27.2 | 0.0 | 1.7% | С | <u> </u> | 233 233 | 229 | 4 | 1.81% | 530 530 | 620 | 621 | -1 | -0.1% |
| | | WBT | | | | | | | | | С | | | | | | 530 | | | -1 | |
| | | All | 2664 | 2798 | 2636 | 2828 | 51.4 | 52.0 | -0.5 | -1.0% | D | D | 125 | 125 | -1 | -0.42% | | 622 | 622 | 0 | 0.0% |



| | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | LC | OS | | Avg | Queue Length | n (ft) | | Max | x Queue | Length (ft) | |
|------|---------------------------------------|----------|--------|---------|--------|--------|--------|--------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 7 | 37 | 12 | 40 | 1374.8 | 1273.0 | 101.8 | 8.0% | F | F | 441 | 510 | -69 | -13.57% | 465 | 554 | 615 | -61 | -9.8% |
| | | EBR | 8 | 48 | 13 | 49 | 1181.6 | 984.3 | 197.3 | 20.0% | F | F | 163 | 192 | -29 | -15.09% | 465 | 190 | 218 | -28 | -12.9% |
| | | EBT | | | 0 | 0 | | 0.0 | | | | Α | | 192 | | | 465 | | 218 | | |
| | | NBL | 47 | 55 | 44 | 57 | 83.8 | 96.3 | -12.5 | -13.0% | F | F | 301 | 383 | -82 | -21.35% | 558 | 451 | 516 | -65 | -12.6% |
| | | NBR | | | 0 | 0 | | 0.0 | | | | Α | | 383 | | | 558 | | 516 | | |
| | Maxwell Street | NBT | 397 | 462 | 367 | 474 | 110.7 | 107.1 | 3.6 | 3.3% | F | F | 441 | 383 | 58 | 15.10% | 558 | 554 | 516 | 38 | 7.5% |
| 7 | at Buchanan Boulevard ² | SBL | | | 0 | 0 | | 0.0 | | | | Α | | 1 | | | 432 | | 153 | | |
| | (Unsignalized) | SBR | 45 | 48 | 46 | 50 | 3.9 | 2.3 | 1.7 | 74.8% | Α | Α | 1 | 1 | 0 | 12.61% | 432 | 127 | 153 | -26 | -17.2% |
| | _ | SBT | 334 | 361 | 336 | 367 | 1.9 | 1.3 | 0.6 | 44.8% | Α | Α | 1 | 1 | 0 | 12.61% | 432 | 127 | 153 | -26 | -17.2% |
| | | WBL | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 295 | | 0 | | |
| | | WBR | | | 0 | 0 | | 0.0 | | | | Α | | 510 | | | 295 | | 615 | | |
| | | WBT | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 295 | | 0 | | |
| | | All | 840 | 1011 | 818 | 1037 | 79.6 | 85.8 | -6.2 | -7.2% | F | F | 225 | 213 | 12 | 5.48% | | 554 | 615 | -61 | -9.8% |
| | | EBL | 174 | 178 | 168 | 172 | 48.9 | 49.1 | -0.3 | -0.5% | D | D | 57 | 53 | 4 | 7.98% | 198 | 310 | 311 | 0 | -0.1% |
| | | EBT | 443 | 449 | 440 | 446 | 37.3 | 37.8 | -0.4 | -1.2% | D | D | 117 | 118 | -1 | -0.74% | 323 | 331 | 334 | -3 | -0.8% |
| | | NBL | 246 | 246 | 274 | 274 | 13.9 | 13.9 | 0.0 | 0.4% | В | В | 21 | 25 | -4 | -14.80% | 204 | 412 | 408 | 4 | 1.0% |
| 8 | Duke Street at | NBR | 27 | 27 | 29 | 28 | 13.2 | 12.8 | 0.5 | 3.6% | В | В | 73 | 64 | 9 | 14.65% | 300 | 404 | 400 | 5 | 1.2% |
| | Main Street ¹ | NBT | 1175 | 1167 | 1143 | 1133 | 14.7 | 14.1 | 0.6 | 4.3% | В | В | 83 | 73 | 10 | 13.30% | 300 | 428 | 423 | 5 | 1.1% |
| | | WBR | 26 | 27 | 23 | 24 | 28.0 | 28.9 | -1.0 | -3.3% | С | С | 54 | 53 | 1 | 1.78% | 221 | 253 | 255 | -2 | -0.9% |
| | | WBT | 285 | 276 | 278 | 270 | 34.8 | 35.2 | -0.4 | -1.2% | С | D | 65 | 64 | 1 | 1.34% | 221 | 271 | 273 | -2 | -0.8% |
| | | All | 2376 | 2370 | 2355 | 2347 | 23.9 | 23.6 | 0.3 | 1.2% | С | С | 67 | 64 | 3 | 4.60% | | 432 | 425 | 7 | 1.6% |
| | | EBL | 30 | 28 | 31 | 28 | 14.9 | 16.0 | -1.1 | -6.9% | В | С | 1 | 1 | 0 | -32.84% | 390 | 53 | 56 | -4 | -6.2% |
| | | EBT | 12 | 11 | 16 | 15 | 19.0 | 20.6 | -1.6 | -7.9% | С | С | 1 | 1 | 0 | -32.84% | 390 | 53 | 56 | -4 | -6.2% |
| | Duke Street at | NBL | 102 | 102 | 105 | 104 | 0.8 | 0.8 | 0.1 | 8.9% | Α | Α | 0 | 0 | 0 | 0.00% | 140 | 0 | 0 | 0 | 0.0% |
| 9 | Peabody Street ¹ | NBR | 3 | 3 | 4 | 4 | 0.6 | 3.1 | -2.4 | -79.4% | Α | Α | 12 | 17 | -5 | -31.24% | 140 | 156 | 272 | -116 | -42.7% |
| | (Unsignalized) | NBT | 1409 | 1405 | 1407 | 1399 | 5.9 | 6.2 | -0.4 | -5.6% | Α | Α | 12 | 17 | -5 | -31.24% | 140 | 156 | 272 | -116 | -42.7% |
| | , | WBR | 7 | 7 | 8 | 8 | 16.3 | 13.2 | 3.1 | 23.1% | С | В | 0 | 0 | 0 | -65.22% | 543 | 27 | 38 | -11 | -29.8% |
| | | WBT | 29 | 27 | 31 | 30 | 16.5 | 17.1 | -0.6 | -3.3% | С | С | 0 | 0 | 0 | -65.22% | 543 | 27 | 38 | -11 | -29.8% |
| | | All | 1591 | 1583 | 1601 | 1588 | 6.0 | 6.4 | -0.4 | -5.9% | Α | Α | 4 | 5 | -2 | -31.27% | | 156 | 272 | -116 | -42.7% |



| | | | Volume | (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | OS | | Avg | Queue Lengtl | n (ft) | | Ma | x Queue | Length (ft) | |
|------|------------------------------------------------|----------|--------|--------|--------|--------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL1 | 1 | 0 | 1 | 0 | 5.5 | 3.5 | 2.0 | 56.8% | Α | Α | 9 | 0 | 9 | 144500.00% | 370 | 343 | 3 | 340 | 10924.9% |
| | Managarial Charact | EBL2 | 9 | 10 | 13 | 15 | 14.0 | 15.5 | -1.5 | -9.8% | В | С | 29 | 0 | 29 | 468400.00% | 370 | 401 | 3 | 398 | 12797.6% |
| 10 | Memorial Street at Duke Street ¹ | NBL | 9 | 10 | 10 | 10 | 8.8 | 6.8 | 2.0 | 28.9% | Α | Α | 35 | 22 | 14 | 63.61% | 213 | 297 | 287 | 9 | 3.2% |
| | (Unsignalized) | NBT1 | 102 | 1500 | 104 | 1492 | 10.3 | 8.4 | 1.9 | 22.2% | В | Α | 9 | 22 | -13 | -58.07% | 213 | 343 | 287 | 56 | 19.4% |
| | , | NBT2 | 1399 | 1500 | 1394 | 1432 | 8.9 | 6.9 | 1.9 | 27.7% | Α | Α | 29 | 22 | 8 | 35.84% | 213 | 401 | 287 | 114 | 39.6% |
| | | All | 1519 | 1520 | 1522 | 1517 | 9.0 | 7.1 | 1.9 | 26.6% | Α | Α | 22 | 13 | 9 | 72.96% | | 402 | 287 | 114 | 39.8% |
| | | EBL | 152 | 149 | 163 | 161 | 48.5 | 61.5 | -13.1 | -21.3% | D | E | 43 | 67 | -24 | -35.37% | 220 | 338 | 350 | -12 | -3.4% |
| | | EBT | 366 | 365 | 389 | 388 | 16.5 | 17.0 | -0.6 | -3.3% | В | В | 33 | 35 | -2 | -6.42% | 336 | 345 | 365 | -20 | -5.6% |
| | | NBL | 221 | 221 | 189 | 189 | 40.2 | 38.0 | 2.3 | 6.0% | D | D | 167 | 147 | 20 | 13.85% | 455 | 582 | 520 | 63 | 12.1% |
| 11 | Chapel Hill Street | NBR | 113 | 113 | 111 | 111 | 9.5 | 7.7 | 1.7 | 22.6% | Α | Α | 151 | 131 | 20 | 15.38% | 455 | 563 | 500 | 63 | 12.6% |
| | at Duke Street ¹ | NBT | 1339 | 1343 | 1320 | 1318 | 43.2 | 40.8 | 2.4 | 5.8% | D | D | 167 | 147 | 20 | 13.85% | 455 | 582 | 520 | 63 | 12.1% |
| | | WBR | 18 | 18 | 23 | 23 | 21.9 | 15.7 | 6.2 | 39.7% | С | В | 183 | 121 | 62 | 51.32% | 275 | 399 | 397 | 2 | 0.6% |
| | | WBT | 712 | 717 | 747 | 749 | 23.3 | 17.2 | 6.0 | 35.0% | С | В | 203 | 140 | 63 | 45.06% | 275 | 429 | 427 | 2 | 0.5% |
| | | All | 2922 | 2926 | 2943 | 2939 | 33.6 | 31.3 | 2.3 | 7.5% | С | С | 135 | 112 | 23 | 20.35% | | 582 | 520 | 63 | 12.1% |
| | | EBR | 59 | 57 | 55 | 52 | 5.8 | 1.3 | 4.5 | 345.4% | Α | Α | 13 | 0 | 13 | 2931.88% | 275 | 303 | 72 | 231 | 321.5% |
| | | EBT | 420 | 421 | 446 | 447 | 11.3 | 1.6 | 9.7 | 617.5% | В | Α | 13 | 0 | 13 | 2931.88% | 275 | 303 | 72 | 231 | 321.5% |
| | Chapel Hill Street | NBL | 41 | 43 | 40 | 42 | 142.2 | 47.4 | 94.9 | 200.3% | F | E | 108 | 18 | 90 | 508.26% | 460 | 299 | 203 | 96 | 47.6% |
| 12 | at Willard Street ¹ | NBR | 119 | 118 | 97 | 93 | 105.7 | 26.3 | 79.4 | 301.7% | F | D | 108 | 18 | 90 | 508.26% | 460 | 299 | 203 | 96 | 47.6% |
| | (Unsignalized) | WBL | 81 | 79 | 59 | 57 | 4.6 | 4.0 | 0.5 | 13.6% | Α | Α | 21 | 6 | 15 | 271.82% | 142 | 240 | 271 | -31 | -11.4% |
| | | WBT | 689 | 692 | 729 | 730 | 18.3 | 9.5 | 8.8 | 92.7% | С | Α | 48 | 20 | 28 | 139.05% | 205 | 238 | 278 | -40 | -14.4% |
| | | All | 1409 | 1410 | 1426 | 1421 | 25.7 | 8.7 | 17.0 | 195.7% | D | Α | 52 | 10 | 41 | 401.58% | | 310 | 284 | 26 | 9.3% |
| | | EBR | 137 | 141 | 164 | 167 | 6.3 | 3.3 | 3.1 | 93.7% | Α | Α | 50 | 3 | 47 | 1693.97% | 206 | 278 | 193 | 85 | 44.1% |
| | | EBT | 402 | 398 | 379 | 373 | 7.7 | 4.1 | 3.6 | 87.5% | Α | Α | 56 | 9 | 47 | 517.08% | 206 | 295 | 240 | 55 | 22.9% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | Pettigrew Street | NBL | | | 248 | 246 | | 47.3 | | | | D | | 78 | | | 377 | | 384 | | |
| 13 | at Chapel Hill | NBR | | | 40 | 41 | | 36.5 | | | | D | | 58 | | | 377 | | 355 | | |
| | Street ¹ | WBL | 24 | 25 | 38 | 37 | 35.2 | 15.1 | 20.2 | 134.1% | D | В | 118 | 33 | 85 | 254.52% | 222 | 299 | 244 | 55 | 22.4% |
| | | WBT | 770 | 771 | 542 | 541 | 38.3 | 13.9 | 24.4 | 175.0% | D | В | 118 | 33 | 85 | 254.52% | 275 | 299 | 244 | 55 | 22.4% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.3 | N/A | N/A | N/A | Α | N/A | 9 | N/A | N/A | N/A | | 247 | N/A | N/A | N/A |
| | | All | 1345 | 1335 | 1410 | 1405 | 25.6 | 16.6 | 9.0 | 54.1% | С | В | 59 | 36 | 23 | 64.35% | | 300 | 387 | -87 | -22.5% |



| | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | OS | | Avg | Queue Length | ı (ft) | | Max | (Queue | Length (ft) | |
|------|--------------------------------|----------|-------------|---------------|---------------|----------------|-------|--------------|-------------|-----------------|-------|--------------|-------|-------------|--------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Bu Model | ild Demand | No-B Model | uild Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 16 | 15 | 25 | 26 | 26.8 | 26.4 | 0.4 | 1.4% | С | С | 27 | 3 | 24 | 863.27% | 150 | 263 | 59 | 204 | 343.1% |
| | | EBR | 104 | 107 | 53 | 53 | 16.0 | 11.9 | 4.1 | 34.8% | В | В | 16 | 10 | 7 | 66.69% | 785 | 235 | 198 | 36 | 18.4% |
| | | EBT | 106 | 108 | 142 | 143 | 25.9 | 18.1 | 7.8 | 42.8% | С | В | 27 | 17 | 10 | 58.62% | 785 | 263 | 223 | 40 | 18.0% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 1.4 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 62 | N/A | N/A | N/A |
| | | NBL | | | 42 | 43 | | 20.1 | | | | С | | 4 | | | 100 | | 142 | | |
| | | NBR | 68 | 67 | 49 | 47 | 8.5 | 12.1 | -3.6 | -29.6% | Α | В | 7 | 16 | -8 | -53.86% | 148 | 124 | 176 | -52 | -29.7% |
| | Blackwell Street | NBT | 209 | 204 | 206 | 200 | 16.3 | 16.2 | 0.0 | 0.3% | В | В | 16 | 22 | -6 | -25.76% | 148 | 147 | 190 | -43 | -22.4% |
| 14 | at Pettigrew | SBL | 29 | 29 | 72 | 74 | 13.7 | 12.8 | 0.9 | 6.8% | В | В | 29 | 10 | 19 | 181.65% | 98 | 164 | 96 | 68 | 70.2% |
| | Street ² | SBR | | | 43 | 44 | | 2.4 | | | | Α | | 10 | | | 98 | | 96 | | |
| | | SBT | 217 | 219 | 185 | 187 | 7.2 | 7.1 | 0.1 | 2.0% | Α | Α | 29 | 10 | 19 | 181.65% | 98 | 164 | 96 | 68 | 70.2% |
| | | WBL | | | 35 | 35 | | 5.8 | | | | Α | | 1 | | | 143 | | 30 | | |
| | | WBR | | | 48 | 49 | | 10.9 | | | | В | | 2 | | | 375 | | 103 | | |
| | | WBT | | | 130 | 126 | | 6.3 | | | | Α | | 5 | | | 375 | | 117 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.2 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 73 | N/A | N/A | N/A |
| | | All | 777 | 749 | 1029 | 1027 | 14.0 | 12.2 | 1.8 | 14.9% | В | В | 17 | 9 | 8 | 87.29% | | 263 | 230 | 33 | 14.2% |
| | | EBL | 38 | 40 | 107 | 111 | 15.3 | 18.6 | -3.3 | -17.7% | В | В | 29 | 31 | -3 | -8.76% | 1081 | 173 | 192 | -19 | -10.1% |
| | | EBR | 185 | 186 | 185 | 190 | 19.0 | 14.3 | 4.8 | 33.3% | В | В | 29 | 59 | -31 | -51.66% | 263 | 175 | 260 | -85 | -32.8% |
| | Black all Grand | EBT | 348 | 348 | 376 | 371 | 15.2 | 17.0 | -1.7 | -10.3% | В | В | 29 | 31 | -3 | -8.76% | 1081 | 173 | 192 | -19 | -10.1% |
| 15 | Blackwell Street at Ramseur | NBR | 91 | 88 | 59 | 57 | 1.6 | 2.7 | -1.1 | -41.6% | Α | Α | 0 | 11 | -10 | -98.94% | 98 | 18 | 129 | -111 | -86.1% |
| 13 | Street ¹ | NBT | 134 | 131 | 220 | 218 | 4.2 | 6.8 | -2.6 | -37.7% | Α | Α | 3 | 24 | -21 | -88.41% | 98 | 49 | 195 | -146 | -74.7% |
| | | SBL | 41 | 42 | 80 | 81 | 11.7 | 14.7 | -3.0 | -20.2% | В | В | 5 | 13 | -8 | -60.98% | 200 | 96 | 171 | -75 | -43.8% |
| | | SBT | 62 | 62 | 114 | 115 | 10.5 | 13.3 | -2.8 | -20.9% | В | В | 5 | 13 | -8 | -60.98% | 200 | 96 | 171 | -75 | -43.8% |
| | | All | 897 | 897 | 1141 | 1143 | 12.5 | 13.5 | -1.0 | -7.1% | В | В | 14 | 26 | -12 | -45.90% | | 175 | 263 | -89 | -33.6% |



| | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | LC | OS | | Avg | Queue Length | n (ft) | | Max | Queue | Length (ft) | |
|------|---------------------------------------------|----------|-------------|---------------|---------------|----------------|-------|--------------|-------------|-----------------|-------|--------------|-------|-------------|--------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Bu Model | ild Demand | No-B Model | uild Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 48 | 46 | 43 | 41 | 31.7 | 33.3 | -1.6 | -4.7% | С | С | 59 | 57 | 2 | 3.90% | 158 | 321 | 353 | -32 | -9.0% |
| | | EBR | 10 | 10 | 23 | 24 | 22.8 | 24.7 | -1.9 | -7.5% | С | С | 48 | 46 | 2 | 4.68% | 158 | 305 | 337 | -32 | -9.4% |
| | | EBT | 261 | 253 | 231 | 223 | 30.3 | 31.6 | -1.3 | -4.2% | С | С | 59 | 57 | 2 | 3.90% | 158 | 321 | 353 | -32 | -9.0% |
| | | NBL | 13 | 14 | 38 | 38 | 9.9 | 9.8 | 0.1 | 1.2% | Α | Α | 7 | 16 | -9 | -57.59% | 202 | 121 | 182 | -60 | -33.1% |
| | | NBR | 6 | 7 | 15 | 16 | 8.1 | 7.4 | 0.7 | 9.2% | Α | Α | 4 | 12 | -8 | -70.02% | 202 | 112 | 172 | -60 | -34.8% |
| | NAsia Chasat at | NBT | 152 | 150 | 274 | 275 | 7.3 | 8.8 | -1.5 | -17.0% | Α | Α | 7 | 16 | -9 | -57.59% | 202 | 121 | 182 | -60 | -33.1% |
| 16 | Main Street at Corcoran Street ² | SBL | 75 | 72 | 56 | 57 | 15.3 | 14.9 | 0.5 | 3.1% | В | В | 11 | 13 | -2 | -16.06% | 172 | 164 | 188 | -25 | -13.0% |
| | Corcoran Street | SBR | 34 | 33 | 37 | 35 | 7.7 | 8.0 | -0.4 | -4.4% | Α | Α | 6 | 8 | -2 | -21.22% | 172 | 143 | 168 | -25 | -14.6% |
| | | SBT | 86 | 82 | 158 | 154 | 11.1 | 11.0 | 0.2 | 1.7% | В | В | 11 | 13 | -2 | -16.06% | 172 | 164 | 188 | -25 | -13.0% |
| | | WBL | 7 | 12 | 13 | 18 | 25.0 | 32.8 | -7.8 | -23.8% | С | С | 24 | 30 | -5 | -17.64% | 310 | 269 | 279 | -10 | -3.7% |
| | | WBR | 73 | 122 | 46 | 66 | 16.6 | 21.2 | -4.7 | -22.0% | В | С | 18 | 21 | -4 | -16.98% | 310 | 248 | 258 | -10 | -4.0% |
| | | WBT | 116 | 190 | 118 | 165 | 24.4 | 30.8 | -6.5 | -21.0% | С | С | 24 | 30 | -5 | -17.64% | 310 | 269 | 279 | -10 | -3.7% |
| | | All | 881 | 991 | 1053 | 1112 | 20.0 | 19.1 | 0.8 | 4.4% | В | В | 23 | 27 | -3 | -12.61% | | 340 | 381 | -41 | -10.7% |
| | | EBR | 32 | 29 | 25 | 24 | 35.8 | 36.9 | -1.1 | -2.9% | D | D | 61 | 48 | 13 | 27.68% | 311 | 379 | 357 | 22 | 6.3% |
| | | EBT | 309 | 303 | 278 | 272 | 32.9 | 31.8 | 1.1 | 3.5% | С | С | 74 | 61 | 13 | 22.03% | 311 | 398 | 375 | 22 | 6.0% |
| | | SBL | 80 | 84 | 92 | 92 | 74.0 | 34.5 | 39.5 | 114.7% | Е | С | 364 | 135 | 229 | 170.19% | 166 | 539 | 510 | 29 | 5.6% |
| 17 | Mangum Street | SBR | 15 | 15 | 14 | 14 | 22.5 | 8.7 | 13.8 | 158.5% | С | Α | 346 | 120 | 226 | 188.62% | 166 | 520 | 491 | 29 | 5.9% |
| '' | at Main Street ¹ | SBT | 935 | 974 | 982 | 985 | 68.7 | 33.4 | 35.2 | 105.4% | E | С | 364 | 135 | 229 | 170.19% | 166 | 539 | 510 | 29 | 5.6% |
| | | WBL | 179 | 298 | 200 | 281 | 182.5 | 179.1 | 3.5 | 1.9% | F | F | 277 | 282 | -5 | -1.62% | 185 | 373 | 375 | -2 | -0.5% |
| | | WBT | 180 | 309 | 162 | 235 | 88.8 | 79.9 | 8.9 | 11.1% | F | E | 112 | 57 | 55 | 96.17% | 342 | 367 | 361 | 5 | 1.5% |
| | | All | 1731 | 2012 | 1752 | 1903 | 75.3 | 53.6 | 21.7 | 40.4% | E | D | 228 | 120 | 109 | 90.99% | | 539 | 512 | 27 | 5.2% |
| | | EBR | 152 | 147 | 176 | 176 | 53.5 | 46.6 | 6.9 | 14.9% | D | D | 55 | 54 | 1 | 2.77% | 318 | 224 | 224 | 1 | 0.3% |
| | Mangum Street | EBT | 326 | 331 | 335 | 333 | 9.8 | 9.4 | 0.4 | 4.4% | Α | Α | 55 | 54 | 1 | 2.77% | 318 | 224 | 224 | 1 | 0.3% |
| 18 | at Ramseur | SBL | 63 | 73 | 56 | 61 | 39.3 | 29.3 | 10.0 | 34.2% | D | С | 219 | 213 | 6 | 2.79% | 225 | 328 | 335 | -7 | -2.0% |
| | Street ¹ | SBT | 1084 | 1228 | 1151 | 1229 | 37.6 | 28.2 | 9.4 | 33.4% | D | С | 219 | 213 | 6 | 2.79% | 225 | 328 | 335 | -7 | -2.0% |
| | | All | 1624 | 1779 | 1718 | 1799 | 33.6 | 26.5 | 7.1 | 27.0% | С | С | 137 | 133 | 4 | 2.78% | | 328 | 335 | -7 | -2.0% |



| | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | OS | | Avg | Queue Length | ı (ft) | | Max | k Queue | Length (ft) | |
|------|-------------------------------------------------|----------|--------|---------|--------|--------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | uild | | No- | | Difference | | No- | | No | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBR | 100 | 101 | 119 | 122 | 4.9 | 15.8 | -10.9 | -68.8% | Α | В | 5 | 15 | -10 | -66.11% | 375 | 137 | 254 | -116 | -45.9% |
| | | EBT | 104 | 103 | 143 | 142 | 19.9 | 23.5 | -3.6 | -15.3% | В | С | 12 | 29 | -18 | -60.46% | 375 | 158 | 290 | -132 | -45.5% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 6.7 | N/A | N/A | N/A | Α | N/A | 2 | N/A | N/A | N/A | | 200 | N/A | N/A | N/A |
| | NA a a success Change at | SBL | 42 | 47 | 56 | 58 | 1.8 | 0.6 | 1.2 | 192.0% | Α | Α | 2 | 0 | 2 | 4037.50% | 82 | 126 | 44 | 82 | 188.7% |
| 19 | Mangum Street at Pettigrew | SBR | | | 28 | 29 | | 0.3 | | | | Α | | 0 | | | 82 | | 34 | | |
| | Street ¹ | SBT | 1189 | 1328 | 1243 | 1318 | 0.9 | 0.3 | 0.6 | 202.2% | Α | Α | 2 | 0 | 2 | 4037.50% | 82 | 126 | 44 | 82 | 188.7% |
| | | WBL | 100 | 101 | 122 | 123 | 4.9 | 68.3 | -63.4 | -92.8% | Α | E | 5 | 55 | -50 | -91.00% | 353 | 137 | 302 | -164 | -54.5% |
| | | WBT | | | 185 | 181 | | 33.7 | | | | С | | 36 | | | 400 | | 241 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.5 | N/A | N/A | N/A | Α | N/A | 4 | N/A | N/A | N/A | | 103 | N/A | N/A | N/A |
| | | All | 1463 | 1579 | 1897 | 1973 | 2.7 | 10.7 | -8.0 | -74.5% | Α | В | 4 | 19 | -15 | -78.88% | | 207 | 382 | -174 | -45.7% |
| | | EBL | 154 | 155 | 25 | 26 | 17.5 | 11.6 | 5.9 | 50.9% | В | В | 15 | 2 | 13 | 774.01% | 153 | 215 | 57 | 159 | 279.9% |
| | | EBR | 9 | 9 | 27 | 27 | 7.6 | 9.7 | -2.1 | -21.6% | Α | Α | 1 | 4 | -3 | -80.52% | 917 | 89 | 150 | -61 | -40.5% |
| | | EBT | 99 | 103 | 195 | 197 | 11.5 | 12.2 | -0.7 | -5.9% | В | В | 5 | 12 | -7 | -56.55% | 917 | 126 | 179 | -52 | -29.3% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 1.4 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 125 | N/A | N/A | N/A |
| | | NBL | | | 53 | 51 | | 25.0 | | | | С | | 6 | | | 155 | | 89 | | |
| | | NBR | 4 | 4 | 72 | 69 | 17.7 | 14.1 | 3.6 | 25.8% | В | В | 18 | 21 | -3 | -12.19% | 822 | 191 | 231 | -40 | -17.2% |
| | Dottigrow Stroot | NBT | 193 | 188 | 251 | 251 | 22.5 | 16.6 | 5.9 | 35.4% | С | В | 25 | 28 | -3 | -9.56% | 822 | 203 | 245 | -42 | -17.2% |
| 20 | Pettigrew Street at Dillard Street ² | SBL | 137 | 133 | 97 | 96 | 37.1 | 24.6 | 12.5 | 50.8% | D | С | 65 | 46 | 19 | 40.97% | 264 | 288 | 252 | 36 | 14.2% |
| | at Billara Street | SBR | | | 16 | 16 | | 13.4 | | | | В | | 33 | | | 264 | | 225 | | |
| | | SBT | 221 | 217 | 244 | 238 | 23.1 | 16.9 | 6.2 | 36.8% | С | В | 65 | 46 | 19 | 40.97% | 264 | 288 | 252 | 36 | 14.2% |
| | | WBL | 9 | 9 | 67 | 69 | 21.7 | 17.8 | 3.9 | 22.2% | С | В | 9 | 10 | -2 | -17.56% | 695 | 129 | 183 | -53 | -29.1% |
| | | WBR | 87 | 89 | 32 | 32 | 22.6 | 11.7 | 11.0 | 94.1% | С | В | 9 | 6 | 2 | 36.09% | 695 | 129 | 168 | -39 | -23.0% |
| | | WBT | | | 78 | 78 | | 16.3 | | | | В | | 10 | | | 695 | | 183 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.2 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 933 | 907 | 1158 | 1150 | 22.4 | 16.5 | 5.9 | 35.9% | С | В | 23 | 19 | 4 | 23.11% | | 305 | 277 | 28 | 10.1% |



| | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | OS | | Avg | Queue Length | ı (ft) | | Ma | x Queue | Length (ft) | |
|------|----------------------------------|----------|-------------|---------------|---------------|----------------|-------|--------------|-------------|-----------------|-------|--------------|-------|-------------|--------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Bu Model | ild Demand | No-B Model | uild Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 5 | 5 | 10 | 10 | 50.9 | 38.7 | 12.2 | 31.6% | D | D | 1 | 2 | 0 | -24.64% | 210 | 28 | 38 | -9 | -24.2% |
| | | EBR | 67 | 66 | 126 | 124 | 10.5 | 29.3 | -18.8 | -64.2% | В | С | 0 | 17 | -17 | -99.28% | 273 | 17 | 156 | -139 | -89.1% |
| | | EBT | 124 | 125 | 180 | 180 | 42.0 | 45.2 | -3.2 | -7.1% | D | D | 30 | 48 | -18 | -37.75% | 696 | 230 | 281 | -51 | -18.3% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | 6 | 6 | 20 | 19 | 8.1 | 5.2 | 2.9 | 56.0% | Α | Α | 7 | 2 | 5 | 253.00% | 70 | 132 | 64 | 67 | 105.1% |
| | | NBR | 146 | 146 | 128 | 133 | 0.4 | 0.5 | -0.2 | -31.3% | Α | Α | 9 | 2 | 7 | 346.06% | 70 | 131 | 64 | 67 | 103.8% |
| | Fayetteville | NBT | 364 | 372 | 429 | 436 | 2.4 | 1.1 | 1.3 | 120.9% | Α | Α | 7 | 2 | 5 | 253.00% | 70 | 132 | 64 | 67 | 105.1% |
| 21 | Street at | SBL | 76 | 75 | 43 | 42 | 58.4 | 25.8 | 32.7 | 126.8% | Е | С | 28 | 6 | 23 | 408.04% | 250 | 409 | 148 | 261 | 177.0% |
| | Pettigrew Street ¹ | SBR | 2 | 2 | 4 | 4 | 58.8 | 24.9 | 33.9 | 136.4% | Е | С | 193 | 91 | 101 | 110.87% | 400 | 412 | 405 | 7 | 1.8% |
| | | SBT | 692 | 692 | 670 | 667 | 64.4 | 27.0 | 37.3 | 138.2% | Е | С | 193 | 91 | 101 | 110.87% | 400 | 412 | 405 | 7 | 1.8% |
| | | WBL | 119 | 125 | 123 | 131 | 75.4 | 143.1 | -67.7 | -47.3% | E | F | 51 | 133 | -82 | -61.71% | 100 | 282 | 474 | -192 | -40.5% |
| | | WBR | 62 | 60 | 39 | 40 | 24.1 | 65.4 | -41.3 | -63.2% | С | E | 20 | 62 | -41 | -67.07% | 1570 | 203 | 378 | -175 | -46.3% |
| | | WBT | 47 | 46 | 84 | 83 | 51.2 | 64.0 | -12.8 | -20.0% | D | E | 20 | 62 | -41 | -67.07% | 1570 | 203 | 378 | -175 | -46.3% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 1721 | 1720 | 1855 | 1869 | 40.3 | 31.1 | 9.2 | 29.5% | D | С | 40 | 43 | -3 | -7.29% | | 413 | 500 | -87 | -17.4% |
| | | NBL | 383 | 385 | 309 | 308 | 40.0 | 17.8 | 22.3 | 125.4% | D | В | 108 | 29 | 79 | 276.49% | 277 | 373 | 275 | 98 | 35.6% |
| | | NBT | 511 | 519 | 560 | 567 | 23.6 | 10.8 | 12.8 | 118.2% | С | В | 65 | 20 | 45 | 223.97% | 286 | 378 | 240 | 138 | 57.6% |
| | F | SBR | 4 | 5 | 30 | 31 | 1.5 | 6.9 | -5.4 | -78.1% | Α | Α | 21 | 40 | -19 | -47.16% | 70 | 175 | 195 | -20 | -10.4% |
| 22 | Fayetteville Street at Jackie | SBT | 874 | 878 | 889 | 891 | 6.1 | 7.2 | -1.1 | -15.4% | Α | Α | 28 | 40 | -12 | -30.67% | 70 | 194 | 195 | -1 | -0.3% |
| | Robinson Drive ¹ | WBL | 158 | 155 | 157 | 151 | 45.3 | 43.9 | 1.4 | 3.3% | D | D | 45 | 44 | 1 | 1.20% | 345 | 244 | 239 | 5 | 2.1% |
| | | WBR | 5 | 5 | 17 | 21 | 7.7 | 41.5 | -33.8 | -81.5% | Α | D | 35 | 44 | -9 | -21.22% | 345 | 232 | 239 | -8 | -3.3% |
| | | WBT | 5 | 5 | 8 | 8 | 39.0 | 42.9 | -4.0 | -9.2% | D | D | 45 | 44 | 1 | 1.20% | 603 | 244 | 239 | 5 | 2.1% |
| | | All | 1939 | 1952 | 1970 | 1977 | 20.7 | 13.2 | 7.4 | 56.3% | С | В | 49 | 37 | 12 | 32.48% | | 378 | 288 | 90 | 31.2% |
| | | EBL | 120 | 123 | 129 | 130 | 53.9 | 54.5 | -0.6 | -1.1% | D | D | 39 | 43 | -4 | -9.58% | 1260 | 205 | 214 | -9 | -4.2% |
| | | EBR | 0 | 0 | 18 | 17 | 0.0 | 6.7 | -6.7 | -100.0% | Α | Α | 18 | 21 | -3 | -14.70% | 1195 | 172 | 181 | -9 | -5.0% |
| | Morehead | EBT | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 39 | 43 | -4 | -9.58% | 1260 | 205 | 214 | -9 | -4.2% |
| 23 | Avenue at | NBR | 0 | 0 | 3 | 3 | 0.0 | 2.6 | -2.6 | -100.0% | Α | Α | 5 | 3 | 2 | 56.06% | 389 | 119 | 101 | 18 | 18.0% |
| 23 | Fayetteville | NBT | 774 | 781 | 739 | 745 | 6.4 | 3.2 | 3.2 | 100.0% | Α | Α | 8 | 6 | 2 | 36.31% | 389 | 137 | 119 | 18 | 15.3% |
| | Street ¹ | SBL | 130 | 131 | 147 | 146 | 11.6 | 6.2 | 5.4 | 87.3% | В | Α | 5 | 2 | 3 | 150.00% | 255 | 144 | 86 | 59 | 68.4% |
| | | SBT | 901 | 902 | 899 | 896 | 5.6 | 2.4 | 3.2 | 132.1% | Α | Α | 17 | 5 | 11 | 224.82% | 275 | 360 | 109 | 251 | 230.1% |
| | | All | 1926 | 1937 | 1935 | 1937 | 9.3 | 6.5 | 2.8 | 43.2% | Α | Α | 19 | 18 | 1 | 5.79% | | 360 | 214 | 146 | 68.2% |



| | | | Volume | e (VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | os | | Avg | Queue Length | ı (ft) | | Max | Queue | Length (ft) | |
|------|-----------------------------------------------|----------|-------------|---------------|----------------|----------------|-------|--------------|-------------|-----------------|-------|--------------|-------|-------------|--------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Bu Model | ild Demand | No-Bo Model | uild Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 37 | 39 | 25 | 27 | 17.1 | 17.5 | -0.4 | -2.3% | В | В | 3 | 32 | -30 | -91.38% | 155 | 57 | 291 | -234 | -80.5% |
| | | EBR | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 17 | 0 | 17 | 0.00% | 1570 | 226 | 0 | 226 | 0.0% |
| | | EBT | 308 | 307 | 324 | 328 | 10.9 | 15.9 | -5.0 | -31.6% | В | В | 17 | 32 | -15 | -46.75% | 1570 | 226 | 291 | -65 | -22.3% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | 59 | 58 | 53 | 54 | 28.8 | 25.5 | 3.4 | 13.3% | C | С | 31 | 44 | -13 | -29.71% | 625 | 256 | 306 | -49 | -16.1% |
| | | NBR | 97 | 97 | 188 | 185 | 18.9 | 21.4 | -2.5 | -11.5% | В | С | 23 | 35 | -11 | -32.52% | 625 | 242 | 290 | -48 | -16.6% |
| | Dattiana Charat | NBT | 87 | 83 | 123 | 119 | 27.9 | 25.0 | 2.9 | 11.4% | С | С | 31 | 44 | -13 | -29.71% | 625 | 256 | 306 | -49 | -16.1% |
| 24 | Pettigrew Street at Grant Street ² | SBL | 123 | 118 | 137 | 134 | 35.5 | 25.9 | 9.7 | 37.3% | D | С | 47 | 23 | 23 | 99.33% | 266 | 316 | 255 | 61 | 23.8% |
| | at Grant Street | SBR | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 47 | 14 | 33 | 237.03% | 266 | 316 | 241 | 75 | 31.2% |
| | | SBT | 109 | 107 | 61 | 59 | 33.5 | 21.4 | 12.2 | 56.9% | С | С | 47 | 23 | 23 | 99.33% | 266 | 316 | 255 | 61 | 23.8% |
| | | WBL | 214 | 215 | 137 | 140 | 17.0 | 16.2 | 0.8 | 4.6% | В | В | 16 | 9 | 7 | 83.94% | 70 | 207 | 118 | 89 | 75.8% |
| | | WBR | 92 | 92 | 92 | 92 | 10.6 | 8.3 | 2.3 | 28.1% | В | Α | 12 | 7 | 5 | 73.31% | 193 | 193 | 140 | 52 | 37.4% |
| | | WBT | 169 | 173 | 193 | 200 | 11.2 | 11.0 | 0.2 | 1.7% | В | В | 13 | 11 | 2 | 18.71% | 193 | 195 | 151 | 44 | 28.9% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 1306 | 1289 | 1334 | 1338 | 18.8 | 18.0 | 0.7 | 4.0% | В | В | 22 | 23 | -1 | -5.32% | | 343 | 332 | 10 | 3.1% |
| | | EBR | 156 | 157 | 121 | 121 | 3.8 | 2.9 | 0.9 | 29.6% | Α | Α | 0 | 0 | 0 | 0.00% | 206 | 7 | 0 | 7 | 0.0% |
| | | EBT | 414 | 410 | 501 | 496 | 4.3 | 2.8 | 1.5 | 53.8% | Α | Α | 0 | 0 | 0 | 0.00% | 206 | 7 | 0 | 7 | 0.0% |
| | Gann Street at | NBL | 126 | 128 | 169 | 172 | 15.5 | 15.7 | -0.1 | -0.9% | С | С | 3 | 3 | 0 | 1.34% | 248 | 134 | 122 | 12 | 9.9% |
| 25 | Pettigrew Street ² | NBR | 88 | 87 | 44 | 43 | 13.3 | 13.1 | 0.2 | 1.7% | В | В | 3 | 3 | 0 | 1.34% | 248 | 134 | 122 | 12 | 9.9% |
| | (Unsignalized) | WBL | 27 | 26 | 64 | 63 | 8.7 | 10.1 | -1.4 | -14.1% | Α | В | 0 | 0 | 0 | -100.00% | 367 | 13 | 39 | -27 | -67.4% |
| | | WBT | 414 | 420 | 350 | 357 | 0.6 | 0.5 | 0.1 | 25.3% | Α | Α | 0 | 0 | 0 | 0.00% | 367 | 0 | 0 | 0 | 0.0% |
| | | All | 1225 | 1228 | 1249 | 1252 | 4.9 | 4.7 | 0.3 | 5.5% | Α | Α | 1 | 1 | 0 | 0.57% | | 134 | 122 | 12 | 9.9% |
| | | EBL | 33 | 34 | 30 | 31 | 52.2 | 56.0 | -3.9 | -6.9% | D | Е | 10 | 10 | 0 | -1.08% | 196 | 153 | 156 | -3 | -2.2% |
| | | EBR | 177 | 175 | 188 | 186 | 7.1 | 7.2 | -0.2 | -2.1% | Α | Α | 4 | 6 | -1 | -22.01% | 196 | 142 | 151 | -10 | -6.4% |
| | | NBL | 129 | 128 | 136 | 137 | 19.1 | 18.6 | 0.5 | 2.7% | В | В | 45 | 47 | -2 | -4.80% | 300 | 414 | 395 | 19 | 4.9% |
| | | NBT | 1473 | 1484 | 1490 | 1500 | 9.0 | 9.7 | -0.8 | -7.9% | Α | Α | 45 | 47 | -2 | -4.80% | 528 | 414 | 395 | 19 | 4.9% |
| 26 | Alston Avenue at | SBR | 21 | 20 | 23 | 22 | 14.3 | 10.2 | 4.1 | 40.1% | В | В | 72 | 51 | 21 | 40.57% | 190 | 550 | 208 | 342 | 164.6% |
| | Gann Street ¹ | SBT | 1358 | 1346 | 1360 | 1355 | 15.1 | 13.4 | 1.7 | 12.8% | В | В | 74 | 59 | 15 | 26.36% | 1037 | 554 | 223 | 330 | 148.0% |
| | | WBL | 154 | 153 | 151 | 150 | 39.6 | 55.3 | -15.7 | -28.4% | D | E | 36 | 52 | -16 | -30.88% | 188 | 227 | 300 | -73 | -24.2% |
| | | WBR | 153 | 150 | 150 | 147 | 11.2 | 11.9 | -0.7 | -5.6% | В | В | 1 | 1 | 0 | 2.76% | 1000 | 83 | 80 | 3 | 4.2% |
| | | WBT | 1 | 1 | 1 | 1 | 34.1 | 24.4 | 9.7 | 39.6% | С | С | 4 | 4 | 0 | 6.54% | 1000 | 108 | 103 | 4 | 4.3% |
| | | All | 3499 | 3491 | 3529 | 3529 | 13.6 | 13.8 | -0.3 | -1.9% | В | В | 32 | 31 | 2 | 5.26% | | 554 | 409 | 145 | 35.4% |



| | | | Volume | e (VPH) | Volume | e (VPH) | | Dela | y (Seconds) | | LC |)S | | Avg (| Queue Length | (ft) | | Max | x Queue | Length (ft) | |
|------|-------------------------------------------|----------|--------|---------|--------|---------|-------|-------|-------------|------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Bu | ild | No-B | Build | | No- | | Difference | | No- | | No | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 34 | 36 | 77 | 77 | 23.4 | 26.4 | -2.9 | -11.2% | С | С | 10 | 15 | -5 | -36.48% | 220 | 152 | 139 | 13 | 9.4% |
| | | EBT | 112 | 114 | 122 | 123 | 15.1 | 14.7 | 0.4 | 2.8% | В | В | 10 | 15 | -5 | -36.48% | 288 | 152 | 139 | 13 | 9.4% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | | | 206 | 205 | | 20.9 | | | | С | | 110 | | | 541 | | 474 | | |
| 27 | Roxboro Street at | NBR | 152 | 153 | 127 | 127 | 24.7 | 7.9 | 16.9 | 214.5% | С | Α | 258 | 99 | 160 | 161.77% | 541 | 569 | 458 | 111 | 24.3% |
| 27 | Pettigrew Street ¹ | NBT | 1563 | 1577 | 1228 | 1244 | 35.6 | 20.5 | 15.1 | 73.7% | D | С | 273 | 110 | 163 | 148.68% | 541 | 587 | 474 | 113 | 23.8% |
| | | WBR | | | 46 | 46 | | 19.5 | | | | В | | 13 | | | 916 | | 163 | | |
| | | WBT | | | 101 | 99 | | 28.5 | | | | С | | 20 | | | 916 | | 178 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 45 | N/A | N/A | N/A |
| | | All | 1887 | 1880 | 1907 | 1921 | 33.0 | 20.0 | 13.0 | 65.0% | С | В | 118 | 54 | 63 | 116.26% | | 587 | 474 | 113 | 23.8% |
| | | EBT LRT | 6 | 6 | | | 0.0 | | | | Α | | 0 | | | | | 0 | | | |
| | LDT at Duckanan | NBT | 453 | 462 | | | 54.8 | | | | F | | 137 | | | | | 213 | | | |
| 28 | LRT at Buchanan Boulevard ² | SBT | 343 | 361 | | | 3.9 | | | | Α | | 30 | | | | | 354 | | | |
| | Dodievara | WBT LRT | 6 | 6 | | | 5.1 | | | | Α | | 9 | | | | | 235 | | | |
| | | All | 808 | 823 | | | 32.4 | | | | D | | 44 | | | | | 356 | | | |
| | Downtown Durham Corridor | EB LRT | 6 | 6 | | | 20.2 | | | | | | | | | | | | | | |
| | Downtown Durham Corridor | WB LRT | 6 | 6 | | | 22.0 | | | | | | | | | | | | | | |
| | | All | 46845 | 49870 | 46792 | 50848 | 31.7 | 27.7 | | | С | С | 79 | 88 | -9 | -9.72% | | 827 | 851 | -24 | -2.8% |

1 - NCDOT Traffic Impact Criteria is applied

2 - City of Durham Traffic Impact Criteria is applied

Indicates LRT Movement
Indicates Traffic Impact
Indicates Traffic Impact below Mid-D

Build Max Queue length exceeds No-Build and Storage Space by more than 10 feet



Table 11: D-O LRT: Downtown Durham Segment – VISSIM Intersection Analysis Output Summary - 2040 Build Option2 vs. 2040 No-Build AM Peak Hour 8:00 - 9:00 AM

| | Intersection | | Volume (VPH) Build | | Volume (VPH) | | Delay (Seconds) | | | | | os | | Avg C | ueue Length | (ft) | Max Queue Length (ft) | | | | |
|------|----------------------------------------|----------|---------------------|--------|--------------|--------|-----------------|-------|------------|------------|-------|-------|-------|-------|-------------|------------|-----------------------|-------|-------|------------|------------|
| Node | | Movement | | | No-Build | | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 84 | 84 | 81 | 84 | 25.5 | 28.7 | -3.2 | -11.2% | С | С | 10 | 12 | -2 | -13.8% | 625 | 109 | 111 | -2 | -1.8% |
| | | EBR | 63 | 64 | 61 | 62 | 22.1 | 26.8 | -4.6 | -17.2% | С | С | 63 | 77 | -14 | -18.7% | 900 | 437 | 428 | 9 | 2.1% |
| | | EBT | 366 | 364 | 343 | 348 | 27.3 | 30.8 | -3.6 | -11.5% | С | С | 73 | 88 | -15 | -17.4% | 900 | 454 | 445 | 9 | 2.0% |
| | | NBL | 72 | 76 | 72 | 78 | 31.2 | 29.3 | 1.9 | 6.4% | С | С | 85 | 83 | 2 | 2.5% | 106 | 227 | 223 | 4 | 1.9% |
| | | NBR | 121 | 119 | 111 | 111 | 17.1 | 18.6 | -1.5 | -8.1% | В | В | 68 | 66 | 2 | 2.8% | 106 | 204 | 199 | 4 | 2.1% |
| | | NBT | 189 | 187 | 173 | 176 | 25.5 | 27.4 | -2.0 | -7.2% | С | С | 85 | 83 | 2 | 2.5% | 106 | 227 | 223 | 4 | 1.9% |
| 1 | Main Street at 9th Street ¹ | SBL | 126 | 124 | 127 | 127 | 28.5 | 27.8 | 0.7 | 2.4% | С | С | 116 | 125 | -9 | -7.6% | 330 | 464 | 485 | -21 | -4.3% |
| | | SBR | 84 | 83 | 95 | 96 | 33.6 | 33.8 | -0.1 | -0.4% | С | С | 94 | 104 | -10 | -9.3% | 330 | 435 | 456 | -21 | -4.6% |
| | | SBT | 369 | 373 | 375 | 384 | 38.8 | 37.2 | 1.6 | 4.4% | D | D | 116 | 125 | -9 | -7.6% | 330 | 464 | 485 | -21 | -4.3% |
| | | WBL | 135 | 133 | 125 | 128 | 13.0 | 18.8 | -5.8 | -30.7% | В | В | 6 | 10 | -4 | -40.0% | 190 | 130 | 139 | -9 | -6.5% |
| | | WBR | 116 | 116 | 111 | 114 | 7.3 | 13.2 | -5.8 | -44.3% | Α | В | 11 | 27 | -16 | -58.6% | 300 | 298 | 328 | -30 | -9.3% |
| | | WBT | 256 | 257 | 265 | 274 | 10.4 | 16.7 | -6.3 | -37.7% | В | В | 17 | 35 | -18 | -51.6% | 300 | 320 | 350 | -30 | -8.7% |
| | | All | 1980 | 1980 | 1940 | 1982 | 24.6 | 27.0 | -2.4 | -9.0% | С | С | 62 | 70 | -8 | -11.0% | | 474 | 487 | -12 | -2.5% |
| | | EBL | 118 | 117 | 118 | 119 | 3.0 | 3.3 | -0.3 | -9.9% | Α | Α | 0 | 8 | -7 | -93.9% | 60 | 70 | 91 | -20 | -22.6% |
| | | EBT | 494 | 490 | 462 | 467 | 2.2 | 3.2 | -0.9 | -29.6% | Α | Α | 0 | 8 | -7 | -93.9% | 290 | 70 | 91 | -20 | -22.6% |
| | Main Street at Iredell | SBL | 44 | 42 | 38 | 37 | 16.7 | 17.0 | -0.3 | -1.7% | С | С | 0 | 3 | -3 | -96.0% | 370 | 26 | 40 | -13 | -33.2% |
| 2 | Street ¹ | SBR | 22 | 21 | 21 | 20 | 10.7 | 11.5 | -0.8 | -6.7% | В | В | 0 | 3 | -3 | -96.0% | 370 | 26 | 40 | -13 | -33.2% |
| | (Unsignalized) | WBR | 138 | 141 | 138 | 145 | 2.8 | 2.6 | 0.2 | 8.6% | Α | Α | 1 | 1 | 0 | 50.0% | 290 | 130 | 97 | 32 | 33.3% |
| | | WBT | 485 | 485 | 481 | 496 | 3.9 | 3.7 | 0.3 | 6.8% | Α | Α | 1 | 1 | 0 | 50.0% | 290 | 130 | 97 | 32 | 33.3% |
| | | All | 1302 | 1296 | 1258 | 1284 | 3.6 | 3.9 | -0.2 | -6.1% | Α | Α | 0 | 4 | -3 | -87.8% | | 159 | 140 | 19 | 13.5% |



| | | | Volume (VPH) | | Volume (VPH) | | | De | lay (Seconds) |) | LC | os | | Avg Q | ueue Length | (ft) | Max Queue Length (ft) | | | | | |
|------|------------------------------------------|----------|---------------|---------------|----------------|--------|-------|--------------|---------------|-----------------|-------|--------------|-------|--------------|-------------|-----------------|-------------------------------|-------|--------------|------------|-----------------|--|
| Node | Intersection | Movement | Buil Model | Demand Demand | No-Bu Model | Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % | |
| | | EBL | 13 | 14 | 13 | 14 | 77.8 | 57.2 | 20.6 | 36.0% | Е | Е | 23 | 43 | -20 | -46.0% | 198 | 338 | 390 | -52 | -13.3% | |
| | | EBR | 151 | 147 | 144 | 143 | 2.5 | 6.9 | -4.5 | -64.3% | Α | Α | 0 | 3 | -3 | -99.2% | 317 | 11 | 54 | -43 | -78.8% | |
| | | EBT | 375 | 371 | 342 | 347 | 30.3 | 37.3 | -7.0 | -18.9% | С | D | 73 | 101 | -28 | -27.7% | 317 | 425 | 444 | -19 | -4.2% | |
| | Main Street at Broad Street ¹ | NBL | 271 | 273 | 241 | 252 | 36.1 | 30.1 | 6.0 | 19.9% | D | С | 127 | 202 | -75 | -37.2% | 121 | 271 | 275 | -4 | -1.5% | |
| | | NBR | 250 | 250 | 237 | 243 | 2.5 | 2.7 | -0.1 | -4.5% | Α | Α | 2 | 0 | 2 | 409.0% | 116 | 158 | 48 | 110 | 232.2% | |
| | | NBT | 302 | 302 | 290 | 299 | 26.5 | 17.3 | 9.2 | 53.0% | С | В | 127 | 202 | -75 | -37.2% | 121 | 271 | 275 | -4 | -1.5% | |
| 3 | | SBL | 65 | 61 | 69 | 66 | 67.5 | 60.5 | 7.0 | 11.6% | Е | Е | 26 | 24 | 2 | 8.4% | 130 | 156 | 180 | -24 | -13.2% | |
| | | SBR | 50 | 51 | 50 | 52 | 28.6 | 28.8 | -0.3 | -0.9% | С | С | 52 | 66 | -14 | -20.9% | 450 | 431 | 466 | -35 | -7.4% | |
| l | | SBT | 399 | 389 | 411 | 412 | 46.5 | 43.7 | 2.8 | 6.3% | D | D | 82 | 96 | -13 | -14.0% | 450 | 473 | 508 | -35 | -6.8% | |
| | | WBL | 162 | 160 | 171 | 175 | 66.3 | 68.3 | -2.0 | -2.9% | Е | E | 68 | 92 | -24 | -26.2% | 412 | 328 | 463 | -136 | -29.3% | |
| | | WBR | 29 | 29 | 33 | 32 | 17.2 | 21.7 | -4.5 | -20.8% | В | С | 15 | 23 | -9 | -37.0% | 560 | 292 | 390 | -98 | -25.1% | |
| l | | WBT | 301 | 302 | 328 | 337 | 24.0 | 26.9 | -2.9 | -10.7% | С | С | 45 | 57 | -12 | -21.8% | 560 | 375 | 473 | -98 | -20.7% | |
| | | All | 2369 | 2349 | 2328 | 2372 | 31.3 | 30.9 | 0.3 | 1.0% | С | С | 53 | 76 | -22 | -29.6% | | 496 | 578 | -82 | -14.2% | |
| l | | EBT LRT | 6 | 6 | N/A | N/A | 1.9 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A | |
| | | NBR | 28 | 30 | 28 | 29 | 10.3 | 9.0 | 1.3 | 14.7% | В | Α | 9 | 11 | -2 | -20.1% | 720 | 209 | 174 | 36 | 20.6% | |
| | | NBT | 237 | 241 | 213 | 220 | 15.4 | 14.5 | 0.9 | 6.2% | С | В | 9 | 11 | -2 | -20.1% | 720 | 209 | 174 | 36 | 20.6% | |
| | Pettigrew Street at 9th | SBL | 23 | 24 | 24 | 25 | 1.9 | 1.6 | 0.3 | 21.6% | Α | Α | 0 | 0 | 0 | 30.4% | 105 | 103 | 53 | 50 | 95.2% | |
| 4 | Street ¹ | SBT | 543 | 546 | 537 | 549 | 0.4 | 0.4 | 0.0 | -3.3% | Α | Α | 0 | 0 | 0 | 30.4% | 105 | 103 | 53 | 50 | 95.2% | |
| | (Unsignalized) | WBL | 73 | 74 | 75 | 79 | 35.5 | 39.4 | -3.9 | -9.9% | Е | E | 29 | 33 | -4 | -12.1% | 185 | 282 | 298 | -16 | -5.4% | |
| | | WBR | 146 | 141 | 143 | 145 | 40.0 | 38.7 | 1.2 | 3.2% | E | Е | 29 | 33 | -4 | -12.1% | 185 | 282 | 298 | -16 | -5.4% | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A | |
| | | All | 1062 | 1056 | 1019 | 1047 | 11.9 | 11.9 | 0.0 | 0.2% | В | В | 10 | 15 | -5 | -35.4% | | 306 | 310 | -3 | -1.1% | |



| | | | Volume (| VPH) | Volume | (VPH) | | De | lay (Seconds | | LC | os | | Avg C | ueue Length | (ft) | | Max Queue Length (ft) | | | | |
|------|---------------------------|----------|----------|--------|----------|--------|-------|-------|--------------|------------|-------|-------|-------|-------|-------------|------------|--------------------|-----------------------|-------|------------|------------|--|
| Node | Intersection | Movement | Build | t l | No-Build | | | No- | -166 | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference | |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % | |
| | | EBL | 6 | 6 | 6 | 6 | 34.1 | 104.7 | -70.7 | -67.5% | D | F | 0 | 5 | -5 | -92.0% | 506 | 21 | 73 | -52 | -71.5% | |
| | | EBR | 33 | 31 | 32 | 31 | 9.0 | 32.2 | -23.1 | -71.9% | Α | D | 0 | 5 | -5 | -92.0% | 506 | 21 | 73 | -52 | -71.5% | |
| | | EBT | 2 | 2 | 1 | 2 | 12.0 | 42.6 | -30.6 | -71.8% | В | Е | 0 | 5 | -5 | -92.0% | 506 | 21 | 73 | -52 | -71.5% | |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A | |
| | | NBL | 192 | 188 | 186 | 191 | 7.9 | 25.1 | -17.1 | -68.4% | Α | D | 1 | 49 | -48 | -97.2% | 443 | 105 | 440 | -335 | -76.1% | |
| | | NBR | 20 | 20 | 19 | 19 | 10.9 | 27.9 | -17.0 | -60.9% | В | D | 58 | 204 | -146 | -71.8% | 443 | 575 | 684 | -109 | -15.9% | |
| | Pettigrew Street at Swift | NBT | 807 | 808 | 752 | 777 | 19.3 | 47.1 | -27.8 | -59.1% | С | Е | 58 | 204 | -146 | -71.8% | 443 | 575 | 684 | -109 | -15.9% | |
| 5 | Avenue ¹ | SBL | 22 | 22 | 21 | 22 | 13.1 | 48.7 | -35.6 | -73.2% | В | Е | 1 | 12 | -12 | -95.8% | 137 | 116 | 188 | -72 | -38.4% | |
| | (Unsignalized) | SBR | 38 | 38 | 40 | 42 | 1.4 | 1.9 | -0.5 | -24.6% | Α | Α | 1 | 12 | -12 | -95.8% | 137 | 116 | 188 | -72 | -38.4% | |
| | | SBT | 652 | 636 | 662 | 666 | 0.4 | 0.7 | -0.3 | -49.1% | Α | Α | 1 | 12 | -12 | -95.8% | 137 | 116 | 188 | -72 | -38.4% | |
| | | WBL | 1 | 1 | 1 | 1 | 6.4 | 38.6 | -32.2 | -83.4% | Α | Е | 0 | 2 | -2 | -100.0% | 515 | 0 | 9 | -9 | -100.0% | |
| | | WBR | 11 | 11 | 10 | 11 | 38.2 | 100.9 | -62.7 | -62.1% | E | F | 0 | 2 | -2 | -100.0% | 515 | 0 | 9 | -9 | -100.0% | |
| | | WBT | 2 | 2 | 2 | 2 | 23.7 | 106.4 | -82.7 | -77.7% | С | F | 0 | 2 | -2 | -100.0% | 515 | 0 | 9 | -9 | -100.0% | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A | |
| | | All | 1798 | 1765 | 1733 | 1770 | 10.6 | 26.2 | -15.6 | -59.7% | В | D | 9 | 43 | -34 | -80.1% | | 575 | 684 | -109 | -15.9% | |
| | | EBL | 134 | 127 | 134 | 128 | 51.8 | 52.8 | -1.0 | -1.8% | D | D | 40 | 42 | -3 | -6.3% | 215 | 329 | 421 | -92 | -21.8% | |
| | | EBR | 86 | 86 | 87 | 86 | 7.3 | 7.5 | -0.2 | -2.9% | Α | Α | 0 | 0 | 0 | 50.0% | 267 | 9 | 5 | 5 | 97.6% | |
| | | EBT | 464 | 464 | 476 | 475 | 23.8 | 24.4 | -0.6 | -2.5% | С | С | 77 | 83 | -6 | -7.6% | 607 | 562 | 579 | -17 | -3.0% | |
| | | NBL | 74 | 79 | 73 | 79 | 66.3 | 67.5 | -1.2 | -1.8% | E | E | 35 | 36 | -1 | -3.6% | 70 | 180 | 185 | -5 | -2.5% | |
| | | NBR | 63 | 61 | 65 | 63 | 11.9 | 13.1 | -1.3 | -9.5% | В | В | 0 | 0 | 0 | -93.5% | 120 | 7 | 18 | -10 | -58.5% | |
| | Main Street at Buchanan | NBT | 177 | 171 | 183 | 177 | 44.1 | 48.2 | -4.2 | -8.6% | D | D | 49 | 56 | -7 | -12.9% | 433 | 191 | 206 | -15 | -7.1% | |
| 6 | Boulevard ¹ | SBL | 159 | 164 | 165 | 170 | 81.0 | 80.7 | 0.3 | 0.4% | F | F | 125 | 134 | -8 | -6.2% | 130 | 472 | 471 | 1 | 0.2% | |
| | Bodievard | SBR | 171 | 169 | 171 | 170 | 23.2 | 24.4 | -1.2 | -4.9% | С | С | 4 | 5 | -1 | -14.7% | 130 | 190 | 176 | 14 | 7.9% | |
| | | SBT | 325 | 325 | 326 | 327 | 55.8 | 56.1 | -0.3 | -0.6% | E | Е | 156 | 154 | 3 | 1.7% | 400 | 471 | 470 | 2 | 0.4% | |
| | | WBL | 50 | 50 | 52 | 51 | 60.4 | 62.5 | -2.1 | -3.3% | E | E | 17 | 18 | -1 | -3.9% | 382 | 168 | 163 | 5 | 2.9% | |
| | | WBR | 44 | 43 | 45 | 44 | 27.9 | 26.8 | 1.1 | 4.2% | С | С | 59 | 58 | 1 | 2.3% | 530 | 397 | 371 | 26 | 7.0% | |
| | | WBT | 293 | 293 | 293 | 293 | 27.7 | 27.6 | 0.2 | 0.6% | С | С | 59 | 58 | 1 | 2.3% | 530 | 397 | 371 | 26 | 7.0% | |
| | | All | 2040 | 2032 | 2070 | 2063 | 39.0 | 39.8 | -0.8 | -2.0% | D | D | 52 | 54 | -2 | -3.4% | | 568 | 579 | -11 | -1.9% | |



| | | Volume (VPH) | | | Volume (VPH) | | | De | lay (Seconds | LO | os | | Avg C | ueue Length | (ft) | Max Queue Length (ft) | | | | | |
|------|-----------------------------------------|--------------|-------|--------|--------------|--------|-------|-------|--------------|------------|-------|-------|-------|-------------|------------|-----------------------|--------------------|-------|-------|------------|------------|
| Node | Intersection | Movement | Build | i . | No-B | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 50 | 48 | 54 | 52 | 19.1 | 24.8 | -5.7 | -23.1% | С | С | 15 | 25 | -10 | -41.3% | 465 | 235 | 263 | -28 | -10.6% |
| | | EBR | 71 | 70 | 75 | 74 | 11.6 | 15.1 | -3.6 | -23.5% | В | С | 2 | 6 | -4 | -74.5% | 465 | 82 | 134 | -52 | -38.9% |
| | | EBT | | | 0 | 0 | | 0.0 | | | | Α | | 6 | | | 465 | | 134 | | |
| | | NBL | 13 | 13 | 13 | 13 | 3.5 | 7.9 | -4.4 | -55.4% | Α | Α | 1 | 7 | -6 | -84.0% | 558 | 101 | 143 | -42 | -29.4% |
| | | NBR | | | 0 | 0 | | 0.0 | | | | Α | | 7 | | | 558 | | 143 | | |
| | Maxwell Street at | NBT | 263 | 263 | 267 | 267 | 6.7 | 7.5 | -0.9 | -11.6% | Α | Α | 15 | 7 | 8 | 115.7% | 558 | 235 | 143 | 92 | 64.7% |
| 7 | Buchanan Boulevard ² | SBL | | | 0 | 0 | | 0.0 | | | | Α | ļ | 0 | | | 432 | | 11 | | |
| | (Unsignalized) | SBR | 16 | 16 | 17 | 17 | 0.6 | 0.6 | 0.0 | 5.4% | Α | Α | 0 | 0 | 0 | 1200.0% | 432 | 52 | 11 | 41 | 355.0% |
| | | SBT | 446 | 445 | 448 | 447 | 1.2 | 0.6 | 0.6 | 114.8% | Α | Α | 0 | 0 | 0 | 1200.0% | 432 | 52 | 11 | 41 | 355.0% |
| | | WBL | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 295 | | 0 | | |
| | | WBR | | | 0 | 0 | | 0.0 | | | | Α | | 25 | | | 295 | | 263 | | |
| | | WBT | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 295 | | 0 | | |
| | | All | 859 | 855 | 873 | 870 | 4.8 | 5.6 | -0.7 | -13.4% | Α | Α | 5 | 7 | -1 | -20.8% | | 235 | 263 | -28 | -10.6% |
| | | EBL | 154 | 154 | 175 | 170 | 38.8 | 40.1 | -1.3 | -3.3% | D | D | 34 | 43 | -9 | -21.8% | 198 | 300 | 307 | -7 | -2.4% |
| | | EBT | 403 | 405 | 369 | 374 | 37.7 | 36.7 | 1.0 | 2.7% | D | D | 105 | 92 | 13 | 14.0% | 323 | 329 | 329 | -1 | -0.2% |
| | | NBL | 259 | 260 | 250 | 251 | 10.1 | 11.4 | -1.3 | -11.8% | В | В | 15 | 16 | -1 | -6.9% | 204 | 348 | 386 | -38 | -9.8% |
| 8 | Duke Street at Main Street ¹ | NBR | 49 | 47 | 41 | 40 | 10.5 | 11.1 | -0.6 | -5.3% | В | В | 31 | 39 | -7 | -18.6% | 300 | 393 | 389 | 3 | 0.9% |
| | | NBT | 929 | 923 | 966 | 956 | 10.8 | 12.1 | -1.3 | -11.1% | В | В | 39 | 47 | -9 | -18.0% | 300 | 416 | 413 | 3 | 0.7% |
| | | WBR | 21 | 21 | 22 | 22 | 17.5 | 21.0 | -3.5 | -16.8% | В | С | 11 | 11 | -1 | -5.9% | 221 | 151 | 156 | -6 | -3.6% |
| | | WBT | 98 | 96 | 95 | 93 | 31.8 | 33.6 | -1.8 | -5.4% | С | С | 19 | 20 | -1 | -5.2% | 221 | 169 | 175 | -6 | -3.2% |
| | | All | 1912 | 1906 | 1917 | 1906 | 19.7 | 20.4 | -0.7 | -3.5% | В | С | 36 | 38 | -2 | -5.6% | | 417 | 415 | 2 | 0.5% |
| | | EBL | 11 | 11 | 17 | 16 | 13.1 | 10.5 | 2.6 | 24.3% | В | В | 0 | 0 | 0 | -50.0% | 390 | 19 | 22 | -3 | -12.9% |
| | | EBT | 3 | 3 | 3 | 3 | 10.7 | 10.4 | 0.3 | 2.9% | В | В | 0 | 0 | 0 | -50.0% | 390 | 19 | 22 | -3 | -12.9% |
| | Duke Street at Peabody | NBL | 63 | 62 | 60 | 59 | 0.7 | 0.6 | 0.1 | 7.8% | Α | Α | 0 | 0 | 0 | 0.0% | 140 | 0 | 0 | 0 | 0.0% |
| 9 | Street ¹ | NBR | 1 | 1 | 1 | 1 | 0.3 | 0.5 | -0.3 | -49.4% | Α | Α | 0 | 2 | -1 | -75.2% | 140 | 83 | 141 | -58 | -41.2% |
| | (Unsignalized) | NBT | 1213 | 1207 | 1226 | 1218 | 2.2 | 3.1 | -0.9 | -28.6% | Α | Α | 0 | 2 | -1 | -75.2% | 140 | 83 | 141 | -58 | -41.2% |
| | (Charge and Charge) | WBR | 12 | 12 | 13 | 13 | 10.6 | 10.5 | 0.1 | 0.5% | В | В | 0 | 0 | 0 | -26.1% | 543 | 31 | 41 | -10 | -24.2% |
| | | WBT | 33 | 32 | 32 | 31 | 13.2 | 14.7 | -1.5 | -10.2% | В | В | 0 | 0 | 0 | -26.1% | 543 | 31 | 41 | -10 | -24.2% |
| | | All | 1336 | 1328 | 1352 | 1341 | 2.6 | 3.5 | -0.8 | -24.3% | Α | Α | 0 | 1 | 0 | -69.1% | | 86 | 141 | -55 | -38.8% |



| | Intersection | | Volume (VPH) | | Volume (VPH) | | | Delay (Seconds) | | | | | | Avg C | ueue Length | (ft) | Max Queue Length (ft) | | | | | |
|------|------------------------------------------------------------------|----------|----------------|--------|---------------|--------|-------|-----------------|------------|-----------------|-------|--------------|-------|--------------|-------------|-----------------|-------------------------------|-------|--------------|------------|-----------------|--|
| Node | | Movement | Build Model | Demand | No-B Model | Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % | |
| | | EBL1 | 0 | 0 | 0 | 0 | 0.7 | 0.7 | -0.1 | -7.9% | Α | Α | 5 | 0 | 5 | 0.0% | 370 | 267 | 0 | 267 | 0.0% | |
| | | EBL2 | 4 | 5 | 4 | 5 | 9.5 | 8.9 | 0.6 | 6.6% | Α | Α | 12 | 0 | 12 | 0.0% | 370 | 361 | 0 | 361 | 0.0% | |
| 40 | Memorial Street at Duke Street ¹ (Unsignalized) | NBL | 14 | 15 | 20 | 20 | 4.6 | 3.6 | 1.0 | 26.2% | Α | Α | 9 | 4 | 5 | 116.5% | 213 | 267 | 209 | 58 | 27.6% | |
| 10 | | NBT1 | 63 | 1265 | 60 | 1273 | 7.3 | 4.8 | 2.5 | 53.0% | Α | Α | 5 | 4 | 1 | 20.5% | 213 | 267 | 209 | 57 | 27.2% | |
| | (Onsignanzea) | NBT2 | 1210 | 1265 | 1223 | 12/3 | 4.6 | 2.8 | 1.8 | 63.6% | Α | Α | 12 | 4 | 8 | 187.3% | 213 | 361 | 209 | 151 | 72.2% | |
| | | All | 1291 | 1285 | 1307 | 1298 | 4.8 | 2.9 | 1.8 | 62.4% | Α | Α | 8 | 2 | 6 | 245.2% | | 362 | 209 | 152 | 72.7% | |
| | | EBL | 200 | 196 | 199 | 193 | 22.9 | 20.3 | 2.6 | 12.7% | С | С | 18 | 19 | -1 | -3.4% | 220 | 326 | 307 | 19 | 6.3% | |
| | | EBT | 670 | 669 | 688 | 690 | 27.0 | 15.1 | 11.9 | 78.8% | С | В | 109 | 71 | 38 | 54.3% | 336 | 385 | 381 | 5 | 1.2% | |
| | | NBL | 120 | 115 | 122 | 117 | 27.1 | 26.4 | 0.7 | 2.8% | С | С | 79 | 74 | 5 | 6.3% | 455 | 301 | 293 | 8 | 2.8% | |
| 11 | Chapel Hill Street at Duke | NBR | 125 | 126 | 130 | 132 | 32.8 | 12.4 | 20.5 | 165.7% | С | В | 64 | 61 | 3 | 5.3% | 455 | 282 | 275 | 7 | 2.5% | |
| 11 | . Street ¹ | NBT | 1032 | 1026 | 1045 | 1039 | 28.0 | 27.8 | 0.2 | 0.7% | С | С | 79 | 74 | 5 | 6.3% | 455 | 301 | 293 | 8 | 2.8% | |
| | | WBR | 55 | 58 | 58 | 61 | 25.6 | 13.6 | 12.1 | 89.0% | С | В | 71 | 30 | 41 | 135.0% | 275 | 377 | 291 | 86 | 29.4% | |
| | | WBT | 360 | 361 | 384 | 383 | 27.8 | 16.5 | 11.3 | 68.2% | С | В | 87 | 45 | 42 | 92.5% | 275 | 406 | 321 | 85 | 26.7% | |
| | | All | 2562 | 2551 | 2626 | 2615 | 27.5 | 21.1 | 6.4 | 30.0% | С | С | 72 | 53 | 19 | 35.5% | | 410 | 386 | 24 | 6.2% | |
| | | EBR | 138 | 137 | 136 | 137 | 12.4 | 1.6 | 10.8 | 696.4% | В | Α | 79 | 0 | 79 | 46522.2% | 275 | 334 | 41 | 293 | 719.5% | |
| | | EBT | 658 | 658 | 683 | 685 | 17.9 | 1.7 | 16.2 | 980.4% | С | Α | 79 | 0 | 79 | 46522.2% | 275 | 334 | 41 | 293 | 719.5% | |
| | Chapel Hill Street at Willard | NBL | 14 | 13 | 15 | 15 | 31.6 | 15.5 | 16.1 | 104.1% | D | С | 4 | 0 | 4 | 2050.0% | 460 | 87 | 31 | 56 | 179.2% | |
| 12 | Street ¹ | NBR | 85 | 84 | 28 | 29 | 30.3 | 11.4 | 18.9 | 166.5% | D | В | 4 | 0 | 4 | 2050.0% | 460 | 87 | 31 | 56 | 179.2% | |
| | (Unsignalized) | WBL | 99 | 95 | 51 | 47 | 14.3 | 7.9 | 6.4 | 81.8% | В | Α | 1 | 0 | 1 | 6433.3% | 142 | 120 | 17 | 104 | 617.3% | |
| | | WBT | 400 | 406 | 427 | 429 | 5.1 | 1.0 | 4.0 | 393.9% | Α | Α | 0 | 0 | 0 | 2300.0% | 205 | 62 | 7 | 54 | 733.5% | |
| | | All | 1394 | 1393 | 1339 | 1342 | 14.3 | 2.0 | 12.3 | 604.9% | В | Α | 28 | 0 | 28 | 25994.1% | | 334 | 66 | 268 | 407.3% | |
| | | EBR | 268 | 270 | 256 | 260 | 7.0 | 3.6 | 3.4 | 95.1% | Α | Α | 85 | 2 | 83 | 3402.3% | 206 | 281 | 153 | 128 | 83.3% | |
| | | EBT | 475 | 472 | 454 | 454 | 8.4 | 3.8 | 4.6 | 122.3% | Α | Α | 94 | 9 | 84 | 892.4% | 206 | 297 | 200 | 98 | 48.9% | |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A | |
| | Pettigrew Street at Chapel | NBL | | | 87 | 86 | | 17.1 | | | | В | | 9 | | | 377 | | 168 | | | |
| 13 | Hill Street ¹ | NBR | | | 69 | 69 | | 8.9 | | | | Α | | 3 | | | 377 | | 139 | | | |
| | niii street | WBL | 38 | 37 | 42 | 42 | 30.3 | 13.7 | 16.7 | 122.0% | С | В | 56 | 17 | 39 | 233.2% | 222 | 292 | 206 | 86 | 41.7% | |
| | | WBT | 499 | 501 | 391 | 390 | 20.5 | 8.5 | 12.0 | 141.7% | С | Α | 56 | 17 | 39 | 233.2% | 275 | 292 | 206 | 86 | 41.7% | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.6 | N/A | N/A | N/A | Α | N/A | 9 | N/A | N/A | N/A | | 247 | N/A | N/A | N/A | |
| | | All | 1292 | 1280 | 1299 | 1301 | 13.4 | 6.7 | 6.8 | 101.6% | В | Α | 50 | 10 | 40 | 419.0% | | 299 | 255 | 45 | 17.5% | |



| | | | Volume | (VPH) | Volume (| VPH) | | De | lay (Seconds) |) | LC | os | | Avg C | ueue Length | (ft) | | Max | Queue | Length (ft) | |
|------|-------------------------------|----------|--------------|---------------|----------------|--------|-------|--------------|---------------|-----------------|-------|--------------|-------|--------------|-------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Bui Model | Demand Demand | No-Bu Model | Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 0 | 0 | 14 | 13 | 0.0 | 32.4 | -32.4 | -100.0% | Α | С | 36 | 1 | 34 | 2569.6% | 150 | 253 | 39 | 214 | 548.5% |
| | | EBR | 117 | 116 | 35 | 36 | 22.8 | 11.1 | 11.7 | 105.5% | C | В | 23 | 10 | 13 | 127.3% | 785 | 226 | 137 | 88 | 64.3% |
| | | EBT | 83 | 83 | 123 | 121 | 36.0 | 20.8 | 15.2 | 72.8% | D | С | 36 | 20 | 16 | 83.1% | 785 | 253 | 159 | 94 | 58.8% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 1.2 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 125 | N/A | N/A | N/A |
| | | NBL | | | 21 | 21 | | 16.8 | | | | В | | 2 | | | 100 | | 65 | | |
| | | NBR | 91 | 89 | 7 | 7 | 4.3 | 9.2 | -5.0 | -53.9% | Α | Α | 2 | 7 | -5 | -72.9% | 148 | 72 | 153 | -81 | -52.8% |
| | Blackwell Street at | NBT | 82 | 83 | 140 | 139 | 15.1 | 15.3 | -0.2 | -1.1% | В | В | 7 | 12 | -5 | -43.6% | 148 | 96 | 167 | -71 | -42.5% |
| 14 | Pettigrew Street ² | SBL | 6 | 6 | 50 | 51 | 3.6 | 3.0 | 0.7 | 22.3% | Α | Α | 1 | 1 | 0 | 72.7% | 98 | 57 | 50 | 7 | 14.4% |
| | r ettigi ett street | SBR | | | 34 | 33 | | 1.0 | | | | Α | | 1 | | | 98 | | 50 | | |
| | | SBT | 95 | 91 | 171 | 164 | 2.2 | 1.4 | 0.8 | 53.2% | Α | Α | 1 | 1 | 0 | 72.7% | 98 | 57 | 50 | 7 | 14.4% |
| | | WBL | | | 7 | 9 | | 16.6 | | | | В | | 0 | | | 143 | | 25 | | |
| | | WBR | | | 49 | 51 | | 15.7 | | | | В | | 13 | | | 375 | | 278 | | |
| | | WBT | | | 211 | 205 | | 14.3 | | | | В | | 18 | | | 375 | | 291 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.1 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 64 | N/A | N/A | N/A |
| | | All | 500 | 468 | 861 | 850 | 15.3 | 11.9 | 3.4 | 28.3% | В | В | 12 | 7 | 5 | 67.9% | | 253 | 291 | -38 | -13.1% |
| | | EBL | 19 | 20 | 15 | 16 | 12.6 | 14.6 | -2.0 | -13.7% | В | В | 22 | 24 | -2 | -8.2% | 1081 | 147 | 155 | -9 | -5.5% |
| | | EBR | 3 | 2 | 6 | 7 | 4.8 | 5.0 | -0.2 | -3.5% | Α | Α | 30 | 32 | -2 | -6.1% | 263 | 192 | 202 | -10 | -4.9% |
| | | EBT | 348 | 351 | 384 | 385 | 14.8 | 16.2 | -1.4 | -8.6% | В | В | 22 | 24 | -2 | -8.2% | 1081 | 147 | 155 | -9 | -5.5% |
| 15 | Blackwell Street at Ramseur | NBR | 2 | 2 | 7 | 7 | 0.2 | 4.0 | -3.8 | -94.1% | Α | Α | 0 | 13 | -13 | -99.0% | 98 | 10 | 135 | -126 | -92.7% |
| | Street ¹ | NBT | 80 | 81 | 196 | 196 | 2.8 | 8.7 | -5.9 | -68.3% | Α | Α | 1 | 29 | -28 | -96.1% | 98 | 34 | 202 | -168 | -83.3% |
| | | SBL | 34 | 34 | 26 | 27 | 13.4 | 16.5 | -3.2 | -19.1% | В | В | 9 | 28 | -20 | -69.6% | 200 | 154 | 284 | -130 | -45.8% |
| | | SBT | 98 | 95 | 248 | 241 | 11.9 | 15.0 | -3.1 | -20.8% | В | В | 9 | 28 | -20 | -69.6% | 200 | 154 | 284 | -130 | -45.8% |
| | | All | 583 | 585 | 883 | 879 | 12.4 | 14.0 | -1.6 | -11.2% | В | В | 13 | 25 | -12 | -48.4% | | 203 | 284 | -81 | -28.6% |



| | | | Volume (| (VPH) | Volume | (VPH) | | De | lay (Seconds |) | L | OS | | Avg C | ueue Length | (ft) | | Max | Queue | Length (ft) | |
|------|------------------------------------------------|----------|----------------|--------|----------------|--------|-------|--------------|--------------|-----------------|-------|--------------|-------|--------------|-------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Build Model | Demand | No-Bi Model | Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 44 | 42 | 55 | 52 | 30.8 | 28.2 | 2.6 | 9.2% | С | С | 50 | 44 | 5 | 12.2% | 158 | 325 | 301 | 24 | 7.9% |
| | | EBR | 15 | 16 | 50 | 50 | 20.2 | 21.7 | -1.5 | -7.1% | С | С | 40 | 34 | 5 | 15.6% | 158 | 309 | 285 | 24 | 8.3% |
| | | EBT | 245 | 236 | 180 | 176 | 27.2 | 26.7 | 0.6 | 2.1% | С | С | 50 | 44 | 5 | 12.2% | 158 | 325 | 301 | 24 | 7.9% |
| | | NBL | 6 | 6 | 20 | 20 | 7.3 | 7.2 | 0.1 | 1.7% | Α | Α | 5 | 6 | -2 | -26.2% | 202 | 88 | 92 | -4 | -4.5% |
| | | NBR | 5 | 7 | 8 | 9 | 5.0 | 3.9 | 1.1 | 27.8% | Α | Α | 2 | 3 | -1 | -38.2% | 202 | 79 | 83 | -4 | -4.9% |
| | Main Chuant at Causana | NBT | 88 | 88 | 183 | 183 | 9.4 | 5.7 | 3.6 | 63.4% | Α | Α | 5 | 6 | -2 | -26.2% | 202 | 88 | 92 | -4 | -4.5% |
| 16 | Main Street at Corcoran Street ² | SBL | 46 | 46 | 24 | 24 | 16.9 | 12.6 | 4.3 | 34.0% | В | В | 10 | 15 | -4 | -29.7% | 172 | 149 | 196 | -47 | -24.1% |
| | Street | SBR | 19 | 18 | 23 | 22 | 7.9 | 7.1 | 0.8 | 11.3% | Α | Α | 5 | 9 | -4 | -41.6% | 172 | 128 | 176 | -47 | -26.9% |
| | | SBT | 94 | 91 | 193 | 187 | 12.7 | 12.5 | 0.2 | 1.7% | В | В | 10 | 15 | -4 | -29.7% | 172 | 149 | 196 | -47 | -24.1% |
| | | WBL | 22 | 22 | 31 | 31 | 11.1 | 11.2 | -0.1 | -1.3% | В | В | 11 | 10 | 1 | 11.5% | 310 | 207 | 106 | 102 | 96.6% |
| | | WBR | 76 | 76 | 40 | 42 | 6.3 | 6.2 | 0.1 | 0.8% | Α | Α | 6 | 4 | 2 | 39.1% | 310 | 186 | 84 | 102 | 121.0% |
| | | WBT | 246 | 240 | 179 | 174 | 7.7 | 8.7 | -1.0 | -11.6% | Α | Α | 11 | 10 | 1 | 11.5% | 310 | 207 | 106 | 102 | 96.6% |
| | | All | 905 | 888 | 986 | 970 | 15.4 | 13.9 | 1.5 | 11.1% | В | В | 17 | 17 | 0 | 1.6% | | 341 | 301 | 40 | 13.2% |
| | | EBR | 9 | 9 | 7 | 7 | 49.0 | 36.9 | 12.1 | 32.7% | D | D | 94 | 43 | 51 | 119.6% | 311 | 376 | 231 | 145 | 62.8% |
| | | EBT | 286 | 280 | 204 | 202 | 55.4 | 42.8 | 12.6 | 29.4% | Е | D | 109 | 56 | 53 | 94.5% | 311 | 394 | 249 | 145 | 58.2% |
| | | SBL | 170 | 172 | 171 | 173 | 35.0 | 16.6 | 18.4 | 111.0% | С | В | 188 | 76 | 111 | 146.0% | 166 | 533 | 465 | 69 | 14.8% |
| 17 | Mangum Street at Main | SBR | 18 | 17 | 7 | 7 | 12.5 | 5.3 | 7.1 | 133.8% | В | Α | 174 | 65 | 109 | 169.3% | 166 | 515 | 444 | 71 | 16.0% |
| 1, | Street ¹ | SBT | 1083 | 1082 | 1096 | 1099 | 34.1 | 17.7 | 16.3 | 92.1% | С | В | 188 | 76 | 111 | 146.0% | 166 | 533 | 465 | 69 | 14.8% |
| | | WBL | 48 | 45 | 88 | 84 | 47.1 | 53.4 | -6.3 | -11.8% | D | D | 12 | 28 | -17 | -58.5% | 185 | 92 | 192 | -100 | -52.0% |
| | | WBT | 326 | 321 | 243 | 240 | 23.1 | 23.3 | -0.2 | -1.0% | С | С | 46 | 33 | 13 | 38.3% | 342 | 334 | 266 | 68 | 25.6% |
| | | All | 1939 | 1926 | 1817 | 1812 | 35.7 | 23.0 | 12.7 | 55.0% | D | С | 116 | 54 | 62 | 114.4% | | 533 | 465 | 68 | 14.7% |
| | | EBR | 107 | 108 | 116 | 117 | 49.9 | 45.6 | 4.3 | 9.3% | D | D | 39 | 40 | -1 | -3.7% | 318 | 170 | 143 | 26 | 18.3% |
| | Mangum Street at Ramseur | EBT | 276 | 279 | 298 | 302 | 15.7 | 20.8 | -5.1 | -24.4% | В | С | 39 | 40 | -1 | -3.7% | 318 | 170 | 143 | 26 | 18.3% |
| 18 | Street at Ramseur | SBL | 86 | 89 | 89 | 91 | 29.5 | 17.8 | 11.7 | 65.4% | С | В | 134 | 78 | 56 | 71.4% | 225 | 322 | 317 | 5 | 1.5% |
| | 3 | SBT | 1052 | 1047 | 1101 | 1099 | 27.1 | 16.8 | 10.3 | 61.6% | С | В | 134 | 78 | 56 | 71.4% | 225 | 322 | 317 | 5 | 1.5% |
| | | All | 1521 | 1523 | 1605 | 1609 | 26.8 | 19.7 | 7.1 | 36.2% | С | В | 87 | 59 | 27 | 45.8% | | 322 | 317 | 5 | 1.5% |



| | | | Volume | (VPH) | Volume | (VPH) | | De | lay (Seconds | | LC | OS | | Avg C | ueue Length | (ft) | | Max | (Queue | Length (ft) | |
|------|-----------------------------|----------|--------|--------|--------|--------|-------|-------|--------------|------------|-------|-------|-------|-------|-------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Buil | d | No-Bı | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBR | 53 | 52 | 53 | 52 | 7.6 | 26.1 | -18.5 | -70.9% | Α | С | 20 | 23 | -2 | -10.7% | 375 | 193 | 188 | 5 | 2.9% |
| | | EBT | 126 | 126 | 127 | 127 | 37.6 | 40.8 | -3.2 | -7.8% | D | D | 32 | 43 | -11 | -26.1% | 375 | 214 | 224 | -10 | -4.6% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 12.7 | N/A | N/A | N/A | В | N/A | 4 | N/A | N/A | N/A | | 200 | N/A | N/A | N/A |
| | | SBL | 49 | 49 | 55 | 54 | 1.6 | 0.7 | 0.9 | 121.2% | Α | Α | 1 | 0 | 1 | 734.8% | 82 | 104 | 52 | 52 | 100.6% |
| 19 | Mangum Street at Pettigrew | SBR | | | 67 | 67 | | 0.5 | | | | Α | | 0 | | | 82 | | 42 | | |
| | Street ¹ | SBT | 1105 | 1106 | 1095 | 1095 | 0.7 | 0.2 | 0.4 | 182.1% | Α | Α | 1 | 0 | 1 | 734.8% | 82 | 104 | 52 | 52 | 100.6% |
| | | WBL | 53 | 52 | 78 | 77 | 7.6 | 58.6 | -51.0 | -87.1% | Α | E | 20 | 27 | -7 | -24.4% | 353 | 193 | 168 | 25 | 14.7% |
| | | WBT | | | 200 | 198 | | 37.5 | | | | D | | 44 | | | 400 | | 252 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.4 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 84 | N/A | N/A | N/A |
| | | All | 1362 | 1333 | 1675 | 1670 | 4.6 | 11.4 | -6.8 | -59.8% | Α | В | 9 | 20 | -11 | -55.5% | | 223 | 275 | -52 | -18.9% |
| | | EBL | 30 | 27 | 16 | 15 | 12.5 | 12.4 | 0.1 | 0.9% | В | В | 2 | 2 | 1 | 60.6% | 153 | 77 | 67 | 10 | 14.1% |
| | | EBR | 18 | 20 | 24 | 25 | 5.5 | 5.9 | -0.4 | -7.3% | Α | Α | 0 | 1 | -1 | -76.9% | 917 | 43 | 76 | -33 | -43.6% |
| | | EBT | 49 | 50 | 76 | 75 | 8.1 | 9.3 | -1.2 | -13.4% | Α | Α | 2 | 3 | -2 | -47.1% | 917 | 82 | 105 | -23 | -21.5% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.5 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 75 | N/A | N/A | N/A |
| | | NBL | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 155 | | 0 | | |
| | | NBR | 8 | 8 | 34 | 34 | 11.5 | 8.2 | 3.4 | 41.1% | В | Α | 5 | 5 | -1 | -10.5% | 822 | 90 | 114 | -24 | -21.0% |
| | Pettigrew Street at Dillard | NBT | 66 | 68 | 100 | 100 | 28.2 | 17.6 | 10.6 | 60.6% | С | В | 10 | 11 | 0 | -1.2% | 822 | 104 | 128 | -24 | -18.4% |
| 20 | Street ² | SBL | 39 | 37 | 46 | 45 | 28.2 | 21.3 | 6.9 | 32.6% | С | С | 31 | 27 | 4 | 15.7% | 264 | 222 | 214 | 8 | 3.6% |
| | | SBR | | | 101 | 98 | | 9.9 | | | | Α | | 18 | | | 264 | | 187 | | |
| | | SBT | 110 | 109 | 110 | 110 | 27.5 | 18.5 | 9.0 | 48.7% | С | В | 31 | 27 | 4 | 15.7% | 264 | 222 | 214 | 8 | 3.6% |
| | | WBL | 36 | 37 | 25 | 25 | 7.5 | 6.1 | 1.5 | 24.6% | Α | Α | 2 | 2 | 0 | 0.3% | 695 | 96 | 111 | -15 | -13.4% |
| | | WBR | 45 | 43 | 17 | 18 | 7.8 | 3.6 | 4.2 | 115.1% | Α | Α | 2 | 1 | 1 | 145.5% | 695 | 96 | 96 | 0 | -0.5% |
| | | WBT | | | 88 | 87 | | 6.0 | | | | Α | | 2 | | | 695 | | 111 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 420 | 399 | 638 | 632 | 18.3 | 12.3 | 6.0 | 49.1% | В | В | 10 | 8 | 2 | 20.2% | | 224 | 214 | 10 | 4.4% |



| | | | Volume (| VPH) | Volume | (VPH) | | De | lay (Seconds | | LC | OS | | Avg Q | ueue Length | (ft) | | Max | « Queue | Length (ft) | |
|------|----------------------------------|----------|----------------|--------|---------------|----------------|-------|--------------|--------------|-----------------|-------|--------------|-------|--------------|-------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Build Model | Demand | No-B Model | uild Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 10 | 9 | 8 | 7 | 57.2 | 61.4 | -4.3 | -6.9% | E | E | 3 | 2 | 0 | 8.9% | 210 | 43 | 44 | -1 | -2.3% |
| | | EBR | 6 | 6 | 26 | 26 | 5.0 | 5.6 | -4.5 | -10.7% | A | A | 0 | 0 | 0 | 0.0% | 273 | 0 | 0 | 0 | 0.0% |
| | | EBT | 53 | 53 | 59 | 57 | 37.7 | 53.9 | -16.2 | -30.0% | D | D | 11 | 18 | -7 | -39.9% | 696 | 104 | 133 | -29 | -21.6% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | A | N/A | 0 | N/A | N/A | N/A | 030 | 0 | N/A | N/A | N/A |
| | | NBL | 3 | 3 | 35 | 35 | 8.6 | 5.9 | 2.7 | 45.7% | A | A | 10 | 4 | 6 | 134.1% | 70 | 143 | 145 | -2 | -1.5% |
| | | NBR | 47 | 45 | 58 | 61 | 0.4 | 0.3 | 0.1 | 43.9% | Α | Α | 45 | 46 | -2 | -3.9% | 70 | 141 | 140 | 1 | 0.7% |
| | | NBT | 364 | 371 | 382 | 388 | 2.7 | 1.3 | 1.4 | 108.8% | Α | Α | 10 | 4 | 6 | 134.1% | 70 | 143 | 145 | -2 | -1.5% |
| 21 | Fayetteville Street at | SBL | 59 | 58 | 42 | 41 | 40.9 | 21.1 | 19.8 | 93.5% | D | С | 16 | 5 | 11 | 212.4% | 250 | 225 | 124 | 101 | 81.9% |
| | Pettigrew Street ¹ | SBR | 1 | 1 | 7 | 7 | 16.1 | 13.4 | 2.8 | 20.9% | В | В | 84 | 32 | 52 | 159.8% | 400 | 343 | 207 | 136 | 65.9% |
| | | SBT | 435 | 432 | 449 | 445 | 41.8 | 22.4 | 19.5 | 87.1% | D | С | 84 | 52 | 33 | 63.3% | 400 | 343 | 250 | 92 | 37.0% |
| | | WBL | 93 | 96 | 87 | 90 | 48.7 | 59.8 | -11.0 | -18.4% | D | Е | 22 | 28 | -6 | -22.7% | 100 | 214 | 200 | 14 | 6.8% |
| | | WBR | 102 | 108 | 45 | 50 | 32.6 | 31.3 | 1.3 | 4.0% | С | С | 48 | 31 | 18 | 57.4% | 1570 | 350 | 254 | 96 | 37.6% |
| | | WBT | 94 | 90 | 127 | 127 | 51.2 | 47.2 | 4.0 | 8.4% | D | D | 48 | 44 | 4 | 8.7% | 1570 | 350 | 277 | 73 | 26.2% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 1277 | 1272 | 1323 | 1334 | 28.9 | 21.3 | 7.6 | 35.7% | С | С | 27 | 22 | 5 | 22.1% | | 380 | 292 | 88 | 30.1% |
| | | NBL | 228 | 227 | 186 | 185 | 27.5 | 14.2 | 13.3 | 93.7% | С | В | 37 | 13 | 24 | 179.9% | 277 | 261 | 150 | 111 | 73.8% |
| | | NBT | 322 | 328 | 359 | 367 | 21.4 | 11.7 | 9.7 | 82.5% | С | В | 25 | 14 | 11 | 76.9% | 286 | 235 | 137 | 97 | 70.6% |
| | | SBR | 43 | 44 | 39 | 40 | 0.9 | 2.1 | -1.1 | -54.0% | Α | Α | 6 | 9 | -4 | -39.4% | 70 | 134 | 156 | -22 | -14.1% |
| 22 | Fayetteville Street at Jackie | SBT | 491 | 490 | 524 | 521 | 4.4 | 6.8 | -2.4 | -35.9% | Α | Α | 10 | 16 | -6 | -36.1% | 70 | 149 | 172 | -23 | -13.4% |
| | Robinson Drive ¹ | WBL | 172 | 169 | 149 | 144 | 39.7 | 40.5 | -0.8 | -1.9% | D | D | 44 | 39 | 5 | 12.5% | 345 | 261 | 222 | 39 | 17.7% |
| | | WBR | 91 | 91 | 115 | 117 | 9.0 | 6.7 | 2.3 | 34.7% | Α | Α | 35 | 33 | 1 | 4.1% | 345 | 249 | 217 | 31 | 14.3% |
| | | WBT | 13 | 13 | 13 | 13 | 38.3 | 36.8 | 1.6 | 4.2% | D | D | 44 | 39 | 5 | 12.5% | 603 | 261 | 222 | 39 | 17.7% |
| | | All | 1362 | 1362 | 1385 | 1387 | 17.3 | 12.9 | 4.4 | 34.2% | В | В | 29 | 24 | 5 | 21.7% | | 281 | 224 | 58 | 25.7% |
| | | EBL | 43 | 44 | 31 | 33 | 48.9 | 45.3 | 3.6 | 8.0% | D | D | 13 | 8 | 4 | 53.4% | 1260 | 102 | 87 | 15 | 17.3% |
| | | EBR | 143 | 139 | 133 | 130 | 6.8 | 6.6 | 0.2 | 2.6% | Α | Α | 2 | 1 | 1 | 134.3% | 1195 | 69 | 53 | 16 | 29.1% |
| | | EBT | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 13 | 8 | 4 | 53.4% | 1260 | 102 | 87 | 15 | 17.3% |
| 23 | Morehead Avenue at | NBR | 20 | 20 | 18 | 18 | 2.0 | 1.8 | 0.2 | 13.5% | Α | Α | 1 | 1 | 0 | 19.7% | 389 | 60 | 63 | -3 | -4.5% |
| | Fayetteville Street ¹ | NBT | 507 | 511 | 514 | 519 | 2.9 | 2.6 | 0.3 | 13.4% | Α | Α | 3 | 3 | 0 | 6.4% | 389 | 78 | 81 | -3 | -3.5% |
| | | SBL | 99 | 93 | 74 | 71 | 4.5 | 3.2 | 1.3 | 41.0% | Α | Α | 1 | 0 | 1 | 196.7% | 255 | 77 | 53 | 24 | 45.0% |
| | | SBT | 564 | 566 | 598 | 594 | 2.3 | 1.5 | 0.8 | 52.9% | Α | Α | 3 | 2 | 1 | 90.3% | 275 | 163 | 141 | 22 | 15.5% |
| | | All | 1376 | 1373 | 1368 | 1365 | 4.6 | 3.5 | 1.1 | 31.6% | Α | Α | 5 | 3 | 2 | 54.4% | | 171 | 141 | 30 | 20.9% |



| | | | Volume (| (VPH) | Volume | (VPH) | | De | lay (Seconds) | | LO | os | | Avg C | ueue Length | (ft) | | Max | (Queue | Length (ft) | |
|------|---------------------------|----------|----------|--------|--------|--------|-------|-------|---------------|------------|-------|-------|-------|-------|-------------|------------|--------------------|-------|---------|-------------|------------|
| Node | Intersection | Movement | Build | d | No-Bu | uild | | No- | | Difference | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 0 | 5 | -5 | -100.0% | 155 | 0 | 107 | -107 | -100.0% |
| | | EBR | 7 | 7 | 13 | 13 | 7.0 | 3.2 | 3.8 | 120.4% | Α | Α | 5 | 0 | 5 | 86900.0% | 1570 | 120 | 4 | 116 | 2916.7% |
| | | EBT | 152 | 149 | 145 | 146 | 7.6 | 6.2 | 1.4 | 23.2% | Α | Α | 5 | 5 | 1 | 19.0% | 1570 | 120 | 107 | 13 | 12.3% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 20 | 7 | 13 | 170.4% | 625 | 205 | 112 | 94 | 83.7% |
| | | NBR | 104 | 102 | 73 | 73 | 14.5 | 9.8 | 4.7 | 48.5% | В | Α | 14 | 4 | 10 | 287.0% | 625 | 191 | 96 | 95 | 98.7% |
| | Pettigrew Street at Grant | NBT | 96 | 93 | 51 | 51 | 26.5 | 19.6 | 6.9 | 35.1% | С | В | 20 | 7 | 13 | 170.4% | 625 | 205 | 112 | 94 | 83.7% |
| 24 | Street ² | SBL | 93 | 90 | 89 | 86 | 33.2 | 25.2 | 8.0 | 32.0% | С | С | 24 | 16 | 8 | 48.9% | 266 | 218 | 199 | 19 | 9.6% |
| | | SBR | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 24 | 7 | 18 | 263.2% | 266 | 218 | 181 | 37 | 20.3% |
| | | SBT | 51 | 50 | 69 | 68 | 31.0 | 23.0 | 8.0 | 34.9% | С | С | 24 | 16 | 8 | 48.9% | 266 | 218 | 199 | 19 | 9.6% |
| | | WBL | 67 | 69 | 127 | 127 | 8.9 | 7.8 | 1.2 | 15.1% | Α | Α | 2 | 4 | -2 | -47.8% | 70 | 70 | 86 | -16 | -18.9% |
| | | WBR | 122 | 123 | 121 | 121 | 11.1 | 5.4 | 5.8 | 107.0% | В | Α | 21 | 6 | 15 | 271.1% | 193 | 303 | 163 | 140 | 85.8% |
| | | WBT | 287 | 294 | 259 | 267 | 10.7 | 7.0 | 3.7 | 52.1% | В | Α | 21 | 8 | 13 | 153.3% | 193 | 305 | 174 | 131 | 75.4% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 989 | 977 | 948 | 952 | 15.2 | 10.5 | 4.7 | 44.2% | В | В | 13 | 7 | 6 | 84.3% | | 315 | 215 | 99 | 46.2% |
| | | EBR | 74 | 73 | 72 | 72 | 2.2 | 2.7 | -0.5 | -17.8% | Α | Α | 0 | 0 | 0 | 0.0% | 206 | 0 | 0 | 0 | 0.0% |
| | | EBT | 291 | 282 | 290 | 287 | 2.4 | 2.9 | -0.5 | -17.7% | Α | Α | 0 | 0 | 0 | 0.0% | 206 | 0 | 0 | 0 | 0.0% |
| | Gann Street at Pettigrew | NBL | 101 | 105 | 99 | 102 | 9.6 | 9.4 | 0.2 | 1.8% | Α | Α | 0 | 0 | 0 | 35.7% | 248 | 47 | 45 | 2 | 4.4% |
| 25 | Street ² | NBR | 11 | 11 | 12 | 12 | 8.3 | 7.1 | 1.3 | 17.8% | Α | Α | 0 | 0 | 0 | 35.7% | 248 | 47 | 45 | 2 | 4.4% |
| | (Unsignalized) | WBL | 21 | 21 | 23 | 23 | 8.0 | 8.4 | -0.4 | -4.8% | Α | Α | 0 | 0 | 0 | 0.0% | 367 | 7 | 8 | -1 | -11.3% |
| | | WBT | 421 | 426 | 432 | 437 | 0.5 | 0.4 | 0.0 | 9.1% | Α | Α | 0 | 0 | 0 | 0.0% | 367 | 0 | 0 | 0 | 0.0% |
| | | All | 919 | 918 | 929 | 933 | 2.5 | 2.6 | -0.2 | -5.8% | Α | Α | 0 | 0 | 0 | -8.3% | | 47 | 45 | 2 | 4.4% |
| | | EBL | 61 | 63 | 69 | 69 | 60.5 | 57.6 | 2.9 | 5.1% | Е | E | 25 | 26 | -1 | -4.2% | 196 | 215 | 217 | -2 | -1.0% |
| | | EBR | 183 | 182 | 182 | 182 | 13.1 | 13.1 | 0.0 | 0.2% | В | В | 16 | 18 | -1 | -6.9% | 196 | 204 | 206 | -2 | -1.1% |
| | | NBL | 13 | 13 | 14 | 14 | 18.6 | 18.4 | 0.2 | 1.1% | В | В | 31 | 33 | -2 | -7.2% | 300 | 260 | 261 | -1 | -0.4% |
| | | NBT | 873 | 870 | 878 | 875 | 11.2 | 12.0 | -0.7 | -6.1% | В | В | 31 | 33 | -2 | -7.2% | 528 | 260 | 261 | -1 | -0.4% |
| 26 | Alston Avenue at Gann | SBR | 48 | 46 | 48 | 46 | 12.3 | 12.2 | 0.1 | 0.7% | В | В | 69 | 74 | -5 | -6.8% | 190 | 530 | 579 | -49 | -8.4% |
| 20 | Street ¹ | SBT | 1442 | 1438 | 1443 | 1440 | 13.4 | 14.0 | -0.6 | -4.4% | В | В | 71 | 76 | -5 | -6.7% | 1037 | 533 | 582 | -49 | -8.4% |
| | | WBL | 423 | 457 | 431 | 457 | 61.8 | 59.5 | 2.3 | 3.9% | E | E | 372 | 370 | 2 | 0.5% | 188 | 685 | 685 | 0 | 0.0% |
| | | WBR | 294 | 321 | 294 | 315 | 42.8 | 41.9 | 0.9 | 2.2% | D | D | 141 | 128 | 14 | 10.7% | 1000 | 652 | 652 | 0 | 0.1% |
| | | WBT | 47 | 52 | 48 | 52 | 61.3 | 58.9 | 2.4 | 4.1% | Е | E | 156 | 142 | 14 | 10.2% | 1000 | 677 | 676 | 0 | 0.1% |
| | | All | 3384 | 3442 | 3407 | 3450 | 22.9 | 23.1 | -0.2 | -0.7% | С | С | 101 | 100 | 1 | 1.5% | | 690 | 698 | -8 | -1.2% |



| | | | Volume | (VPH) | Volume | (VPH) | | De | lay (Seconds | | LC | OS | | Avg Q | ueue Length | (ft) | | Max | Queue | Length (ft) | |
|------|----------------------------------------|----------|--------|--------|--------|--------|-------|-------|--------------|------------|-------|-------|-------|-------|-------------|------------|------------------|-------|-------|-------------|------------|
| Node | Intersection | Movement | Build | d | No-B | uild | Build | No- | Difference | Difference | Build | No- | Build | No- | Difference | Difference | Storage Space | Build | No- | Difference | Difference |
| | | | Model | Demand | Model | Demand | Bullu | Build | Difference | % | Bullu | Build | Bullu | Build | Difference | % | Available | Dullu | Build | Difference | % |
| | | EBL | 86 | 86 | 90 | 90 | 48.4 | 57.0 | -8.6 | -15.0% | D | E | 30 | 38 | -8 | -22.1% | 220 | 211 | 172 | 39 | 22.7% |
| | | EBT | 89 | 89 | 91 | 91 | 37.4 | 43.3 | -5.9 | -13.6% | D | D | 30 | 38 | -8 | -22.1% | 288 | 211 | 172 | 39 | 22.7% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | | | 189 | 188 | | 9.1 | | | | Α | | 50 | | | 541 | | 439 | | |
| 27 | Roxboro Street at Pettigrew | NBR | 8 | 8 | 25 | 24 | 12.9 | 2.6 | 10.3 | 392.6% | В | Α | 69 | 38 | 31 | 83.0% | 541 | 269 | 408 | -139 | -34.1% |
| 27 | Street ¹ | NBT | 1950 | 1973 | 1501 | 1524 | 14.0 | 9.0 | 5.1 | 56.3% | В | Α | 81 | 50 | 31 | 63.1% | 541 | 291 | 439 | -147 | -33.6% |
| | | WBR | | | 100 | 98 | | 67.6 | | | | Е | | 80 | | | 916 | | 349 | | |
| | | WBT | | | 88 | 87 | | 81.0 | | | | F | | 94 | | | 916 | | 368 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 2157 | 2156 | 2085 | 2102 | 16.3 | 18.4 | -2.1 | -11.6% | В | В | 42 | 55 | -14 | -24.8% | | 293 | 484 | -192 | -39.6% |
| | | EBT LRT | 6 | 6 | | | 0.0 | | | | Α | | 0 | | | | | 0 | | | |
| | | NBT | 277 | 263 | | | 3.0 | | | | Α | | 4 | | | | | 152 | | | |
| 28 | LRT at Buchanan Boulevard ² | SBT | 516 | 445 | | | 6.4 | | | | Α | | 20 | | | | | 410 | | | |
| | | WBT LRT | 6 | 6 | | | 5.1 | | | | Α | | 9 | | | | | 234 | | | |
| | | All | 805 | 708 | | | 5.2 | | | | Α | | 8 | | | | | 410 | | | |
| | Downtown Durham Corridor | EB LRT | 6 | 6 | | | 21.5 | | | | | | | | | | | | | | |
| | Downtown Durham Corridor | WB LRT | 6 | 6 | | | 21.4 | | | | | | | | | | | | | | |
| | | All | 40696 | 40406 | 40971 | 41136 | 18.5 | 17.2 | | | В | В | 31 | 30 | 1 | 3.3% | | 701 | 747 | -46 | -6.2% |

- 1 NCDOT Traffic Impact Criteria is applied
- 2 City of Durham Traffic Impact Criteria is applied

Indicates LRT Movement
Indicates Traffic Impact

Indicates Traffic Impact below Mid-D

Build Max Queue length exceeds No-Build and Storage Space by more than 10 feet



Table 12: D-O LRT: Downtown Durham Segment – VISSIM Intersection Analysis Output Summary - 2040 Build Option 2 vs. 2040 No-Build PM Peak Hour 5:00 - 6:00 PM

| | | | Volume (| VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | OS | | Avg C | Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|----------------------------------------|----------|----------|--------|--------|--------|-------|-------|-------------|------------|--------|-------|-------|-------|--------------|------------|------------------|-------|-------|-------------|------------|
| Node | Intersection | Movement | Build | | No-B | uild | Build | No- | Difference | Difference | امانين | No- | Build | No- | Difference | Difference | Storage Space | Build | No- | Difference | Difference |
| | | | Model | Demand | Model | Demand | Bullu | Build | Difference | % | Bullu | Build | Bullu | Build | Difference | % | Available | Bullu | Build | Difference | % |
| | | EBL | 56 | 61 | 52 | 63 | 41.6 | 41.1 | 0.5 | 1.2% | D | D | 9 | 8 | 2 | 21.6% | 625 | 87 | 77 | 10 | 13.3% |
| | | EBR | 48 | 52 | 48 | 58 | 43.3 | 50.5 | -7.2 | -14.3% | D | D | 231 | 284 | -53 | -18.6% | 900 | 456 | 453 | 3 | 0.6% |
| | | EBT | 547 | 592 | 498 | 599 | 45.8 | 53.8 | -8.1 | -15.0% | D | D | 244 | 298 | -53 | -18.0% | 900 | 473 | 470 | 3 | 0.6% |
| | | NBL | 24 | 47 | 18 | 47 | 26.6 | 32.4 | -5.8 | -17.9% | С | С | 116 | 116 | 0 | 0.1% | 106 | 185 | 185 | 0 | 0.2% |
| | | NBR | 179 | 305 | 140 | 302 | 23.0 | 48.9 | -25.9 | -52.9% | С | D | 101 | 100 | 1 | 0.6% | 106 | 166 | 165 | 0 | 0.2% |
| | | NBT | 169 | 288 | 127 | 300 | 33.5 | 50.8 | -17.3 | -34.0% | С | D | 116 | 116 | 0 | 0.1% | 106 | 185 | 185 | 0 | 0.2% |
| 1 | Main Street at 9th Street ¹ | SBL | 226 | 237 | 219 | 240 | 43.4 | 65.2 | -21.8 | -33.4% | D | E | 96 | 181 | -86 | -47.3% | 330 | 376 | 503 | -127 | -25.2% |
| | | SBR | 69 | 74 | 65 | 76 | 20.1 | 32.7 | -12.7 | -38.7% | С | С | 74 | 157 | -83 | -52.7% | 330 | 345 | 472 | -127 | -26.9% |
| | | SBT | 178 | 180 | 180 | 198 | 28.7 | 39.5 | -10.9 | -27.5% | С | D | 96 | 181 | -86 | -47.3% | 330 | 376 | 503 | -127 | -25.2% |
| | | WBL | 179 | 204 | 168 | 216 | 50.0 | 70.0 | -20.0 | -28.5% | D | E | 85 | 158 | -73 | -46.4% | 190 | 390 | 392 | -3 | -0.7% |
| | | WBR | 211 | 248 | 187 | 245 | 12.9 | 14.2 | -1.3 | -9.2% | В | В | 116 | 149 | -32 | -21.9% | 300 | 374 | 373 | 1 | 0.3% |
| | | WBT | 377 | 441 | 347 | 452 | 16.4 | 17.7 | -1.3 | -7.1% | В | В | 128 | 163 | -35 | -21.4% | 300 | 396 | 395 | 1 | 0.3% |
| | | All | 2262 | 2729 | 2048 | 2796 | 32.7 | 43.4 | -10.7 | -24.6% | С | D | 118 | 159 | -42 | -26.1% | | 497 | 529 | -32 | -6.0% |
| | | EBL | 149 | 174 | 135 | 176 | 12.5 | 17.9 | -5.5 | -30.5% | В | С | 54 | 103 | -49 | -47.2% | 60 | 318 | 321 | -3 | -0.9% |
| | | EBT | 806 | 960 | 726 | 965 | 11.8 | 16.9 | -5.2 | -30.5% | В | С | 54 | 103 | -49 | -47.2% | 290 | 318 | 321 | -3 | -0.9% |
| | Main Street at Iredell | SBL | 30 | 32 | 27 | 33 | 109.8 | 225.0 | -115.3 | -51.2% | F | F | 45 | 117 | -72 | -61.5% | 370 | 191 | 203 | -12 | -6.1% |
| 2 | Street ¹ | SBR | 79 | 80 | 67 | 77 | 81.0 | 175.0 | -94.0 | -53.7% | F | F | 45 | 117 | -72 | -61.5% | 370 | 191 | 203 | -12 | -6.1% |
| | (Unsignalized) | WBR | 20 | 22 | 20 | 25 | 8.0 | 11.6 | -3.6 | -30.9% | Α | В | 38 | 101 | -63 | -62.6% | 290 | 417 | 418 | -1 | -0.3% |
| | | WBT | 686 | 813 | 635 | 836 | 12.9 | 15.7 | -2.7 | -17.4% | В | С | 38 | 101 | -63 | -62.6% | 290 | 417 | 418 | -1 | -0.3% |
| | | All | 1769 | 2081 | 1610 | 2112 | 17.1 | 26.8 | -9.6 | -36.0% | С | D | 46 | 107 | -61 | -57.3% | | 417 | 418 | -1 | -0.3% |



| | | | Volume (| VPH) | Volume (| VPH) | | Dela | ay (Seconds) | | LC | OS | | Avg (| Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|------------------------------------------|----------|----------------|--------|-----------------|--------|-------|--------------|--------------|-----------------|-------|--------------|-------|--------------|--------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Build Model | Demand | No-Bui Model | Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 101 | 118 | 87 | 113 | 39.8 | 37.9 | 1.9 | 4.9% | D | D | 171 | 271 | -100 | -36.9% | 198 | 455 | 454 | 1 | 0.2% |
| | | EBR | 228 | 268 | 196 | 255 | 4.2 | 7.9 | -3.7 | -46.7% | Α | Α | 26 | 3 | 23 | 877.1% | 317 | 126 | 114 | 12 | 10.5% |
| | | EBT | 513 | 606 | 477 | 630 | 28.6 | 34.4 | -5.7 | -16.7% | С | С | 231 | 318 | -87 | -27.4% | 317 | 471 | 469 | 2 | 0.4% |
| | | NBL | 185 | 263 | 175 | 283 | 75.6 | 51.0 | 24.6 | 48.1% | Е | D | 196 | 209 | -13 | -6.1% | 121 | 268 | 267 | 1 | 0.3% |
| | | NBR | 134 | 174 | 131 | 185 | 9.8 | 1.5 | 8.3 | 547.7% | А | Α | 178 | 101 | 78 | 77.1% | 116 | 253 | 251 | 2 | 0.8% |
| | | NBT | 332 | 439 | 318 | 448 | 24.4 | 16.1 | 8.3 | 51.6% | С | В | 196 | 209 | -13 | -6.1% | 121 | 268 | 267 | 1 | 0.3% |
| 3 | Main Street at Broad Street ¹ | SBL | 84 | 112 | 80 | 116 | 116.2 | 107.6 | 8.6 | 8.0% | F | F | 71 | 86 | -16 | -18.1% | 130 | 482 | 561 | -79 | -14.1% |
| | | SBR | 42 | 62 | 42 | 65 | 70.8 | 78.8 | -7.9 | -10.1% | Е | E | 334 | 339 | -5 | -1.5% | 450 | 529 | 528 | 1 | 0.2% |
| | | SBT | 442 | 630 | 437 | 625 | 92.0 | 93.0 | -1.0 | -1.1% | F | F | 373 | 375 | -2 | -0.5% | 450 | 570 | 569 | 1 | 0.2% |
| | | WBL | 162 | 171 | 146 | 167 | 47.1 | 49.3 | -2.2 | -4.5% | D | D | 75 | 49 | 26 | 52.7% | 412 | 314 | 348 | -34 | -9.8% |
| | | WBR | 85 | 89 | 77 | 87 | 35.4 | 48.9 | -13.6 | -27.7% | D | D | 152 | 263 | -111 | -42.2% | 560 | 589 | 591 | -2 | -0.3% |
| | | WBT | 483 | 510 | 443 | 513 | 40.9 | 53.7 | -12.9 | -24.0% | D | D | 204 | 326 | -121 | -37.2% | 560 | 672 | 673 | -2 | -0.3% |
| | | All | 2792 | 3442 | 2609 | 3487 | 45.4 | 47.3 | -1.9 | -4.0% | D | D | 184 | 212 | -28 | -13.4% | | 672 | 674 | -2 | -0.3% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 2.8 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBR | 47 | 79 | 35 | 82 | 99.9 | 128.0 | -28.0 | -21.9% | F | F | 260 | 278 | -17 | -6.2% | 720 | 365 | 362 | 2 | 0.6% |
| | | NBT | 331 | 587 | 257 | 596 | 109.0 | 141.6 | -32.6 | -23.0% | F | F | 260 | 278 | -17 | -6.2% | 720 | 365 | 362 | 2 | 0.6% |
| | Pettigrew Street at 9th | SBL | 34 | 38 | 33 | 42 | 2.8 | 12.4 | -9.6 | -77.2% | Α | В | 2 | 22 | -20 | -90.9% | 105 | 81 | 180 | -99 | -54.9% |
| 4 | Street ¹ | SBT | 370 | 398 | 362 | 430 | 0.4 | 1.9 | -1.6 | -81.6% | Α | Α | 2 | 22 | -20 | -90.9% | 105 | 81 | 180 | -99 | -54.9% |
| | (Unsignalized) | WBL | 21 | 27 | 18 | 26 | 22.3 | 19.7 | 2.7 | 13.5% | С | С | 2 | 1 | 1 | 52.1% | 185 | 80 | 63 | 17 | 26.3% |
| | | WBR | 40 | 53 | 38 | 53 | 49.1 | 46.6 | 2.4 | 5.2% | E | E | 2 | 1 | 1 | 52.1% | 185 | 80 | 63 | 17 | 26.3% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 856 | 1182 | 743 | 1229 | 50.5 | 59.4 | -8.8 | -14.9% | F | F | 66 | 100 | -34 | -34.2% | | 365 | 362 | 2 | 0.6% |



| | | | Volume (| VPH) | Volume (| (VPH) | | Dela | y (Seconds) | | LC | OS | | Avg C | Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|---------------------------|----------|----------|--------|----------|--------|-------|-------|-------------|-----------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|-------|-------------|------------|
| Node | Intersection | Movement | Build | I | No-Bu | ild | | No- | | | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | Difference % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 33 | 47 | 29 | 53 | 296.4 | 373.3 | -76.9 | -20.6% | F | F | 452 | 638 | -186 | -29.1% | 506 | 783 | 840 | -57 | -6.8% |
| | | EBR | 112 | 157 | 89 | 166 | 227.3 | 316.2 | -88.9 | -28.1% | F | F | 452 | 638 | -186 | -29.1% | 506 | 783 | 840 | -57 | -6.8% |
| | | EBT | 2 | 2 | 2 | 3 | 175.8 | 345.7 | -169.8 | -49.1% | F | F | 452 | 638 | -186 | -29.1% | 506 | 783 | 840 | -57 | -6.8% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | 36 | 49 | 33 | 48 | 134.6 | 118.5 | 16.2 | 13.6% | F | F | 66 | 187 | -121 | -64.6% | 443 | 392 | 395 | -3 | -0.7% |
| | | NBR | 7 | 8 | 7 | 9 | 56.8 | 67.0 | -10.2 | -15.3% | F | F | 629 | 658 | -29 | -4.3% | 443 | 785 | 784 | 1 | 0.1% |
| | Pettigrew Street at Swift | NBT | 595 | 789 | 574 | 820 | 114.4 | 122.4 | -8.0 | -6.5% | F | F | 686 | 715 | -29 | -4.0% | 443 | 842 | 841 | 1 | 0.1% |
| 5 | Avenue ¹ | SBL | 11 | 14 | 11 | 16 | 40.8 | 133.0 | -92.2 | -69.3% | Е | F | 19 | 30 | -11 | -36.8% | 137 | 163 | 222 | -60 | -26.8% |
| | | SBR | 32 | 43 | 32 | 45 | 1.0 | 1.3 | -0.3 | -23.7% | Α | Α | 19 | 30 | -11 | -36.8% | 137 | 163 | 222 | -60 | -26.8% |
| | | SBT | 792 | 1012 | 734 | 986 | 0.6 | 1.0 | -0.4 | -42.1% | Α | Α | 19 | 30 | -11 | -36.8% | 137 | 163 | 222 | -60 | -26.8% |
| | | WBL | 9 | 16 | 9 | 17 | 532.1 | 854.1 | -322.0 | -37.7% | F | F | 238 | 369 | -132 | -35.7% | 515 | 470 | 502 | -31 | -6.2% |
| | | WBR | 25 | 40 | 22 | 43 | 563.1 | 941.6 | -378.5 | -40.2% | F | F | 238 | 369 | -132 | -35.7% | 515 | 470 | 502 | -31 | -6.2% |
| | | WBT | 4 | 5 | 3 | 6 | 642.6 | 928.8 | -286.2 | -30.8% | F | F | 238 | 369 | -132 | -35.7% | 515 | 470 | 502 | -31 | -6.2% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 1669 | 2182 | 1544 | 2212 | 77.8 | 92.5 | -14.7 | -15.9% | F | F | 250 | 389 | -139 | -35.6% | | 845 | 847 | -3 | -0.3% |
| | | EBL | 182 | 184 | 183 | 187 | 118.6 | 118.9 | -0.3 | -0.2% | F | F | 339 | 343 | -4 | -1.1% | 215 | 610 | 610 | 0 | 0.0% |
| | | EBR | 64 | 65 | 68 | 69 | 11.5 | 12.4 | -0.9 | -6.9% | В | В | 0 | 0 | 0 | 0.0% | 267 | 0 | 0 | 0 | 0.0% |
| | | EBT | 541 | 549 | 541 | 554 | 24.2 | 24.5 | -0.3 | -1.2% | С | С | 16 | 16 | 0 | -2.6% | 607 | 457 | 462 | -5 | -1.0% |
| | | NBL | 77 | 94 | 72 | 97 | 120.8 | 117.9 | 2.9 | 2.5% | F | F | 93 | 83 | 9 | 11.1% | 70 | 195 | 211 | -16 | -7.5% |
| | | NBR | 55 | 66 | 52 | 67 | 16.8 | 18.6 | -1.7 | -9.3% | В | В | 0 | 0 | 0 | -100.0% | 120 | 1 | 8 | -7 | -87.6% |
| | Main Street at Buchanan | NBT | 274 | 339 | 256 | 350 | 56.8 | 60.1 | -3.4 | -5.6% | E | E - | 110 | 109 | 1 | 1.2% | 433 | 206 | 222 | -17 | -7.5% |
| 6 | Boulevard ¹ | SBL | 101 | 109 | 98 | 107 | 153.5 | 154.1 | -0.6 | -0.4% | F | F | 169 | 165 | 3 | 1.9% | 130 | 471 | 475 | -4 | -0.8% |
| | | SBR | 174 | 180 | 170 | 179 | 41.9 | 43.1 | -1.2 | -2.8% | D | D | 9 | 10 | -1 | -10.9% | 130 | 291 | 255 | 36 | 14.1% |
| | | SBT | 280 | 310 | 280 | 312 | 92.5 | 95.5 | -3.0 | -3.1% | F | F | 267 | 277 | -10 | -3.6% | 400 | 472 | 474 | -2 | -0.5% |
| | | WBL | 32 | 34 | 35 | 36 | 93.9 | 93.5 | 0.4 | 0.4% | F | F | 34 | 44 | -10 | -22.9% | 382 | 481 | 516 | -35 | -6.7% |
| | | WBR | 182 | 183 | 181 | 181 | 26.0 | 26.1 | -0.1 | -0.5% | С | С | 231 | 229 | 2 | 1.0% | 530 | 621 | 621 | 0 | 0.0% |
| | | WBT | 699 | 685 | 701 | 689 | 27.4 | 27.2 | 0.2 | 0.6% | C | C | 231 | 229 | 2 | 1.0% | 530 | 621 | 621 | 0 | 0.0% |
| | <u> </u> | All | 2662 | 2798 | 2636 | 2828 | 51.5 | 52.0 | -0.5 | -1.0% | D | D | 125 | 125 | -1 | -0.5% | | 623 | 622 | 1 | 0.1% |



| | | | Volume (| VPH) | Volume | (VPH) | | Dela | ay (Seconds) | | L | OS | | Avg (| Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|-----------------------------------------|----------|----------|--------|--------|--------|--------|--------|--------------|-----------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|-------|-------------|------------|
| Node | Intersection | Movement | Build | d . | No-B | uild | | No- | -166 | | | No- | | No- | -166 | Difference | Storage | | No- | - · · · · | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | Difference % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 8 | 37 | 12 | 40 | 1341.8 | 1273.0 | 68.8 | 5.4% | F | F | 434 | 510 | -76 | -14.8% | 465 | 553 | 615 | -61 | -10.0% |
| | | EBR | 12 | 48 | 13 | 49 | 1083.3 | 984.3 | 99.0 | 10.1% | F | F | 161 | 192 | -31 | -16.1% | 465 | 188 | 218 | -30 | -13.6% |
| | | EBT | | | 0 | 0 | | 0.0 | | | | Α | | 192 | | | 465 | | 218 | | |
| | | NBL | 48 | 55 | 44 | 57 | 84.0 | 96.3 | -12.3 | -12.8% | F | F | 294 | 383 | -89 | -23.3% | 558 | 450 | 516 | -66 | -12.7% |
| | | NBR | | | 0 | 0 | | 0.0 | | | | Α | | 383 | | | 558 | | 516 | | |
| | Maxwell Street at | NBT | 396 | 462 | 367 | 474 | 108.9 | 107.1 | 1.7 | 1.6% | F | F | 434 | 383 | 51 | 13.4% | 558 | 553 | 516 | 38 | 7.3% |
| 7 | Buchanan Boulevard ² | SBL | | | 0 | 0 | | 0.0 | | | | Α | | 1 | | | 432 | | 153 | | |
| | (Unsignalized) | SBR | 45 | 48 | 46 | 50 | 3.6 | 2.3 | 1.4 | 60.9% | Α | Α | 1 | 1 | 0 | 27.7% | 432 | 134 | 153 | -20 | -12.8% |
| | | SBT | 333 | 361 | 336 | 367 | 2.0 | 1.3 | 0.7 | 53.8% | Α | Α | 1 | 1 | 0 | 27.7% | 432 | 134 | 153 | -20 | -12.8% |
| | | WBL | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 295 | | 0 | | |
| | | WBR | | | 0 | 0 | ļ | 0.0 | | | | Α | | 510 | | | 295 | | 615 | | |
| | | WBT | | | 0 | 0 | | 0.0 | | | | Α | | 0 | | | 295 | | 0 | | |
| | | All | 841 | 1011 | 818 | 1037 | 82.3 | 85.8 | -3.5 | -4.0% | F | F | 221 | 213 | 8 | 3.8% | | 553 | 615 | -61 | -10.0% |
| | | EBL | 175 | 178 | 168 | 172 | 48.8 | 49.1 | -0.4 | -0.8% | D | D | 57 | 53 | 4 | 7.5% | 198 | 310 | 311 | 0 | -0.1% |
| | | EBT | 443 | 449 | 440 | 446 | 37.3 | 37.8 | -0.5 | -1.2% | D | D | 117 | 118 | -1 | -0.8% | 323 | 331 | 334 | -3 | -0.8% |
| | | NBL | 247 | 246 | 274 | 274 | 13.4 | 13.9 | -0.5 | -3.4% | В | В | 20 | 25 | -5 | -19.5% | 204 | 401 | 408 | -7 | -1.6% |
| 8 | Duke Street at Main Street ¹ | NBR | 27 | 27 | 29 | 28 | 14.6 | 12.8 | 1.8 | 14.2% | В | В | 74 | 64 | 10 | 15.0% | 300 | 403 | 400 | 3 | 0.7% |
| | | NBT | 1181 | 1167 | 1143 | 1133 | 14.7 | 14.1 | 0.6 | 4.1% | В | В | 83 | 73 | 10 | 13.3% | 300 | 426 | 423 | 3 | 0.7% |
| | | WBR | 26 | 27 | 23 | 24 | 27.9 | 28.9 | -1.0 | -3.5% | С | С | 54 | 53 | 1 | 1.8% | 221 | 253 | 255 | -2 | -0.9% |
| | | WBT | 285 | 276 | 278 | 270 | 34.8 | 35.2 | -0.4 | -1.2% | С | D | 65 | 64 | 1 | 1.3% | 221 | 271 | 273 | -2 | -0.8% |
| | | All | 2383 | 2370 | 2355 | 2347 | 23.8 | 23.6 | 0.2 | 0.8% | C | С | 67 | 64 | 3 | 4.3% | | 429 | 425 | 4 | 0.9% |
| | | EBL | 30 | 28 | 31 | 28 | 14.4 | 16.0 | -1.6 | -10.1% | В | C | 0 | 1 | 0 | -43.3% | 390 | 53 | 56 | -4 | -6.5% |
| | | EBT | 12 | 11 | 16 | 15 | 18.3 | 20.6 | -2.3 | -11.3% | C | C | 0 | 1 | 0 | -43.3% | 390 | 53 | 56 | -4 | -6.5% |
| | Duke Street at Peabody | NBL | 103 | 102 | 105 | 104 | 0.8 | 0.8 | 0.0 | 4.1% | A | A | 0 | 0 | 0 | 0.0% | 140 | 0 | 0 | 0 | 0.0% |
| 9 | Street ¹ | NBR | 3 | 3 | 4 | 4 | 0.8 | 3.1 | -2.2 | -73.3% | A | A | 12 | 17 | -5 - | -29.0% | 140 | 157 | 272 | -115 | -42.2% |
| | (Unsignalized) | NBT | 1415 | 1405 | 1407 | 1399 | 6.0 | 6.2 | -0.2 | -3.9% | A | A | 12 | 17 | -5 | -29.0% | 140 | 157 | 272 | -115 | -42.2% |
| | | WBR | 7 | 7 | 8 | 8 | 16.0 | 13.2 | 2.8 | 21.0% | С | В | 0 | 0 | 0 | -60.9% | 543 | 26 | 38 | -13 | -33.2% |
| | | WBT | 29 | 27 | 31 | 30 | 16.0 | 17.1 | -1.0 | -6.1% | С | С | 0 | 0 | 0 | -60.9% | 543 | 26 | 38 | -13 | -33.2% |
| | <u> </u> | All | 1599 | 1583 | 1601 | 1588 | 6.1 | 6.4 | -0.3 | -5.0% | Α | Α | 4 | 5 | -2 | -29.8% | | 157 | 272 | -115 | -42.2% |



| | | | Volume (| VPH) | Volume | (VPH) | | Dela | ay (Seconds) | | L | os | | Avg C | Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|------------------------------------------------|----------|----------|--------|--------|--------|-------|-------|--------------|-----------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|-------|-------------|------------|
| Node | Intersection | Movement | Build | d . | No-B | uild | | No- | | | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | Difference % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL1 | 1 | 0 | 1 | 0 | 5.2 | 3.5 | 1.7 | 48.0% | Α | Α | 7 | 0 | 7 | 115900.0% | 370 | 343 | 3 | 340 | 10907.6% |
| | | EBL2 | 9 | 10 | 13 | 15 | 14.8 | 15.5 | -0.7 | -4.2% | В | С | 22 | 0 | 22 | 346000.0% | 370 | 372 | 3 | 368 | 11839.0% |
| 10 | Memorial Street at Duke Street ¹ | NBL | 9 | 10 | 10 | 10 | 8.3 | 6.8 | 1.5 | 22.6% | Α | Α | 29 | 22 | 8 | 35.2% | 213 | 292 | 287 | 4 | 1.5% |
| 10 | (Unsignalized) | NBT1 | 103 | 1500 | 104 | 1492 | 9.6 | 8.4 | 1.2 | 14.2% | Α | Α | 7 | 22 | -14 | -66.4% | 213 | 343 | 287 | 55 | 19.2% |
| | (0.10.8.14.1204) | NBT2 | 1404 | 1300 | 1394 | 1432 | 8.2 | 6.9 | 1.3 | 18.3% | Α | Α | 22 | 22 | 0 | 0.3% | 213 | 372 | 287 | 84 | 29.3% |
| | | All | 1526 | 1520 | 1522 | 1517 | 8.3 | 7.1 | 1.2 | 17.2% | Α | Α | 17 | 13 | 4 | 34.3% | | 381 | 287 | 93 | 32.4% |
| | | EBL | 152 | 149 | 163 | 161 | 48.1 | 61.5 | -13.5 | -21.9% | D | Е | 43 | 67 | -23 | -35.0% | 220 | 343 | 350 | -7 | -2.0% |
| | | EBT | 366 | 365 | 389 | 388 | 16.7 | 17.0 | -0.3 | -2.0% | В | В | 33 | 35 | -2 | -4.7% | 336 | 345 | 365 | -20 | -5.5% |
| | | NBL | 222 | 221 | 189 | 189 | 38.5 | 38.0 | 0.5 | 1.3% | D | D | 158 | 147 | 11 | 7.5% | 455 | 569 | 520 | 50 | 9.6% |
| 11 | Chapel Hill Street at Duke | NBR | 113 | 113 | 111 | 111 | 9.0 | 7.7 | 1.2 | 15.8% | Α | Α | 142 | 131 | 11 | 8.5% | 455 | 550 | 500 | 50 | 10.0% |
| 11 | Street ¹ | NBT | 1341 | 1343 | 1320 | 1318 | 41.2 | 40.8 | 0.3 | 0.7% | D | D | 158 | 147 | 11 | 7.5% | 455 | 569 | 520 | 50 | 9.6% |
| | | WBR | 18 | 18 | 23 | 23 | 20.4 | 15.7 | 4.7 | 30.2% | С | В | 177 | 121 | 56 | 46.6% | 275 | 398 | 397 | 1 | 0.4% |
| | | WBT | 712 | 717 | 747 | 749 | 22.7 | 17.2 | 5.5 | 31.9% | С | В | 197 | 140 | 57 | 40.9% | 275 | 428 | 427 | 1 | 0.3% |
| | | All | 2925 | 2926 | 2943 | 2939 | 32.4 | 31.3 | 1.1 | 3.6% | С | С | 130 | 112 | 17 | 15.5% | | 569 | 520 | 50 | 9.6% |
| | | EBR | 59 | 57 | 55 | 52 | 5.9 | 1.3 | 4.6 | 358.5% | Α | Α | 12 | 0 | 12 | 2782.6% | 275 | 304 | 72 | 232 | 322.8% |
| | | EBT | 420 | 421 | 446 | 447 | 11.4 | 1.6 | 9.9 | 629.1% | В | Α | 12 | 0 | 12 | 2782.6% | 275 | 304 | 72 | 232 | 322.8% |
| | Chapel Hill Street at Willard | NBL | 42 | 43 | 40 | 42 | 130.7 | 47.4 | 83.3 | 175.9% | F | E | 102 | 18 | 84 | 477.0% | 460 | 301 | 203 | 99 | 48.7% |
| 12 | Street ¹ | NBR | 120 | 118 | 97 | 93 | 100.1 | 26.3 | 73.8 | 280.3% | F | D | 102 | 18 | 84 | 477.0% | 460 | 301 | 203 | 99 | 48.7% |
| | (Unsignalized) | WBL | 81 | 79 | 59 | 57 | 4.5 | 4.0 | 0.5 | 11.2% | Α | Α | 24 | 6 | 18 | 330.6% | 142 | 240 | 271 | -31 | -11.4% |
| | | WBT | 688 | 692 | 729 | 730 | 18.1 | 9.5 | 8.6 | 90.5% | С | Α | 47 | 20 | 27 | 133.8% | 205 | 237 | 278 | -41 | -14.8% |
| | | All | 1410 | 1410 | 1426 | 1421 | 25.1 | 8.7 | 16.4 | 188.8% | D | Α | 50 | 10 | 40 | 385.1% | | 310 | 284 | 26 | 9.2% |
| | | EBR | 137 | 141 | 164 | 167 | 6.3 | 3.3 | 3.0 | 93.5% | Α | Α | 51 | 3 | 48 | 1728.3% | 206 | 277 | 193 | 84 | 43.4% |
| | | EBT | 402 | 398 | 379 | 373 | 7.8 | 4.1 | 3.7 | 91.4% | Α | Α | 57 | 9 | 48 | 528.1% | 206 | 293 | 240 | 54 | 22.3% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | Pettigrew Street at Chapel | NBL | | | 248 | 246 | | 47.3 | | | | D | | 78 | | | 377 | | 384 | | <u> </u> |
| 13 | Hill Street ¹ | NBR | | | 40 | 41 | | 36.5 | | | | D | | 58 | | | 377 | | 355 | | <u> </u> |
| | | WBL | 24 | 25 | 38 | 37 | 36.7 | 15.1 | 21.6 | 143.6% | D | В | 119 | 33 | 86 | 257.1% | 222 | 300 | 244 | 56 | 23.1% |
| | | WBT | 770 | 771 | 542 | 541 | 38.7 | 13.9 | 24.7 | 177.4% | D | В | 119 | 33 | 86 | 257.1% | 275 | 300 | 244 | 56 | 23.1% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.7 | N/A | N/A | N/A | Α | N/A | 10 | N/A | N/A | N/A | | 247 | N/A | N/A | N/A |
| | | All | 1345 | 1335 | 1410 | 1405 | 25.8 | 16.6 | 9.2 | 55.6% | С | В | 59 | 36 | 24 | 66.1% | | 301 | 387 | -87 | -22.4% |



| | | | Volume (| (VPH) | Volume (| (VPH) | | Del | ay (Seconds) | | L/ | .os | | Avg (| Queue Length | ı (ft) | | Мах | Queue | Length (ft) | |
|----------|-------------------------------|----------|----------------|---------------|-----------------|--------|----------|--------------|--------------|--------------|-----------|--------------|-------|--------------|--------------|-----------------|-------------------------------|----------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Build Model | Demand Demand | No-Bui Model | Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 16 | 15 | 25 | 26 | 27.3 | 26.4 | 0.9 | 3.5% | С | С | 28 | 3 | 25 | 902.4% | 150 | 260 | 59 | 201 | 338.6% |
| ' | 1 | EBR | 104 | 107 | 53 | 53 | 17.1 | 11.9 | 5.2 | 43.8% | В | В | 17 | 10 | 7 | 76.1% | 785 | 232 | 198 | 34 | 17.0% |
| | | EBT | 106 | 108 | 142 | 143 | 26.6 | 18.1 | 8.5 | 46.7% | С | В | 28 | 17 | 11 | 65.1% | 785 | 260 | 223 | 37 | 16.8% |
| ' | | EBT LRT | 6 | 6 | N/A | N/A | 2.3 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 175 | N/A | N/A | N/A |
| | | NBL | <u> </u> | | 42 | 43 | <u> </u> | 20.1 | <u> </u> | <u> </u> | <u> </u> | С | | 4 | <u>'</u> | | 100 | | 142 | | <i>'</i> |
| | | NBR | 68 | 67 | 49 | 47 | 8.1 | 12.1 | -4.0 | -32.8% | Α | В | 7 | 16 | -8 | -52.5% | 148 | 135 | 176 | -41 | -23.3% |
| | Blackwell Street at | NBT | 210 | 204 | 206 | 200 | 16.7 | 16.2 | 0.5 | 3.1% | В | В | 16 | 22 | -5 | -24.2% | 148 | 159 | 190 | -31 | -16.5% |
| 14 | Pettigrew Street ² | SBL | 29 | 29 | 72 | 74 | 13.3 | 12.8 | 0.5 | 4.0% | В | В | 30 | 10 | 20 | 188.0% | 98 | 159 | 96 | 63 | 65.0% |
| | | SBR | | | 43 | 44 | <u> </u> | 2.4 | <u> </u> ' | <u> </u> ' | ' | Α | | 10 | ' | <u> </u> | 98 | | 96 | <u> </u> | <i>'</i> |
| ' | | SBT | 216 | 219 | 185 | 187 | 7.4 | 7.1 | 0.3 | 4.3% | Α | Α | 30 | 10 | 20 | 188.0% | 98 | 159 | 96 | 63 | 65.0% |
| | | WBL | 4 | | 35 | 35 | <u> </u> | 5.8 | <u> </u> ' | <u> </u> ' | <u> </u> | Α | | 1 | ' | <u> </u> | 143 | <u> </u> | 30 | <u> </u> | ' |
| ' | | WBR | | | 48 | 49 | <u> </u> | 10.9 | <u> </u> ' | <u> </u> ' | ' | В | | 2 | ' | <u> </u> | 375 | | 103 | <u> </u> | ' |
| ' | | WBT | + | | 130 | 126 | <u> </u> | 6.3 | <u> </u> | <u> </u> | <u> </u> | Α | | 5 | | | 375 | | 117 | | <u> </u> |
| ' | | WBT LRT | 6 | 6 | N/A | N/A | 0.2 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 71 | N/A | N/A | N/A |
| <u> </u> | | All | 778 | 749 | 1029 | 1027 | 14.3 | 12.2 | 2.2 | 17.9% | В | В | 18 | 9 | 9 | 93.5% | | 260 | 230 | 30 | 13.0% |
| ' | | EBL | 38 | 40 | 107 | 111 | 16.2 | 18.6 | -2.4 | -12.9% | В | В | 28 | 31 | -3 | -9.9% | 1081 | 168 | 192 | -24 | -12.5% |
| | 1 | EBR | 185 | 186 | 185 | 190 | 19.0 | 14.3 | 4.8 | 33.5% | В | В | 28 | 59 | -31 | -52.9% | 263 | 170 | 260 | -90 | -34.6% |
| ' | | EBT | 348 | 348 | 376 | 371 | 14.9 | 17.0 | -2.1 | -12.2% | В | В | 28 | 31 | -3 | -9.9% | 1081 | 168 | 192 | -24 | -12.5% |
| 15 | Blackwell Street at Ramseur | NBR | 91 | 88 | 59 | 57 | 1.6 | 2.7 | -1.1 | -41.3% | Α | Α | 0 | 11 | -11 | -99.4% | 98 | 18 | 129 | -111 | -86.2% |
| 13 | Street ¹ | NBT | 134 | 131 | 220 | 218 | 4.2 | 6.8 | -2.6 | -38.9% | Α | Α | 3 | 24 | -21 | -88.8% | 98 | 47 | 195 | -148 | -75.7% |
| ' | | SBL | 41 | 42 | 80 | 81 | 12.9 | 14.7 | -1.8 | -12.5% | В | В | 5 | 13 | -8 | -59.4% | 200 | 103 | 171 | -68 | -39.7% |
| ' | | SBT | 61 | 62 | 114 | 115 | 10.7 | 13.3 | -2.6 | -19.9% | В | В | 5 | 13 | -8 | -59.4% | 200 | 103 | 171 | -68 | -39.7% |
| | 1 | All | 897 | 897 | 1141 | 1143 | 12.5 | 13.5 | -1.0 | -7.3% | В | В | 14 | 26 | -12 | -46.5% | | 170 | 263 | -93 | -35.4% |



| | | | Volume (| VPH) | Volume | (VPH) | | Dela | y (Seconds) | | L | OS | | Avg C | Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|---------------------------------------------|----------|----------------|--------|--------|----------------|-------|--------------|-------------|-----------------|-------|--------------|-------|--------------|--------------|-----------------|-------------------------------|-------|--------------|-------------|-----------------|
| Node | Intersection | Movement | Build Model | Demand | No-B | uild Demand | Build | No- Build | Difference | Difference % | Build | No- Build | Build | No- Build | Difference | Difference % | Storage Space Available | Build | No- Build | Difference | Difference % |
| | | EBL | 48 | 46 | 43 | 41 | 34.4 | 33.3 | 1.1 | 3.4% | С | С | 66 | 57 | 9 | 16.4% | 158 | 348 | 353 | -5 | -1.4% |
| | | EBR | 10 | 10 | 23 | 24 | 22.6 | 24.7 | -2.1 | -8.5% | С | С | 55 | 46 | 9 | 19.6% | 158 | 332 | 337 | -5 | -1.5% |
| | | EBT | 262 | 253 | 231 | 223 | 32.9 | 31.6 | 1.3 | 4.1% | С | С | 66 | 57 | 9 | 16.4% | 158 | 348 | 353 | -5 | -1.4% |
| | | NBL | 13 | 14 | 38 | 38 | 10.5 | 9.8 | 0.7 | 6.9% | В | Α | 7 | 16 | -9 | -57.0% | 202 | 114 | 182 | -67 | -37.0% |
| | | NBR | 6 | 7 | 15 | 16 | 10.4 | 7.4 | 3.1 | 41.3% | В | Α | 4 | 12 | -8 | -70.1% | 202 | 105 | 172 | -67 | -39.0% |
| | Maria Charatast Casasas | NBT | 152 | 150 | 274 | 275 | 7.4 | 8.8 | -1.3 | -15.3% | Α | Α | 7 | 16 | -9 | -57.0% | 202 | 114 | 182 | -67 | -37.0% |
| 16 | Main Street at Corcoran Street ² | SBL | 75 | 72 | 56 | 57 | 16.3 | 14.9 | 1.4 | 9.2% | В | В | 11 | 13 | -2 | -16.4% | 172 | 169 | 188 | -19 | -10.1% |
| | Street | SBR | 34 | 33 | 37 | 35 | 7.7 | 8.0 | -0.4 | -4.4% | Α | Α | 6 | 8 | -2 | -22.5% | 172 | 149 | 168 | -19 | -11.4% |
| | | SBT | 86 | 82 | 158 | 154 | 11.1 | 11.0 | 0.2 | 1.5% | В | В | 11 | 13 | -2 | -16.4% | 172 | 169 | 188 | -19 | -10.1% |
| | | WBL | 7 | 12 | 13 | 18 | 33.8 | 32.8 | 1.0 | 3.1% | С | С | 38 | 30 | 8 | 26.3% | 310 | 312 | 279 | 32 | 11.6% |
| | | WBR | 78 | 122 | 46 | 66 | 25.6 | 21.2 | 4.4 | 20.7% | С | С | 29 | 21 | 7 | 34.4% | 310 | 290 | 258 | 32 | 12.6% |
| | | WBT | 123 | 190 | 118 | 165 | 31.6 | 30.8 | 0.7 | 2.4% | С | С | 38 | 30 | 8 | 26.3% | 310 | 312 | 279 | 32 | 11.6% |
| | | All | 893 | 991 | 1053 | 1112 | 22.9 | 19.1 | 3.7 | 19.6% | С | В | 28 | 27 | 2 | 5.7% | | 383 | 381 | 1 | 0.4% |
| | | EBR | 32 | 29 | 25 | 24 | 38.8 | 36.9 | 1.9 | 5.2% | D | D | 68 | 48 | 20 | 41.8% | 311 | 390 | 357 | 33 | 9.2% |
| | | EBT | 309 | 303 | 278 | 272 | 36.0 | 31.8 | 4.2 | 13.2% | D | С | 81 | 61 | 21 | 33.9% | 311 | 408 | 375 | 33 | 8.7% |
| | | SBL | 78 | 84 | 92 | 92 | 78.8 | 34.5 | 44.3 | 128.7% | Е | С | 380 | 135 | 245 | 182.2% | 166 | 540 | 510 | 30 | 5.8% |
| 17 | Mangum Street at Main | SBR | 15 | 15 | 14 | 14 | 23.4 | 8.7 | 14.7 | 168.4% | С | Α | 362 | 120 | 242 | 202.0% | 166 | 521 | 491 | 30 | 6.1% |
| 1 | Street ¹ | SBT | 919 | 974 | 982 | 985 | 71.9 | 33.4 | 38.5 | 115.1% | Е | С | 380 | 135 | 245 | 182.2% | 166 | 540 | 510 | 30 | 5.8% |
| | | WBL | 189 | 298 | 200 | 281 | 178.8 | 179.1 | -0.3 | -0.2% | F | F | 279 | 282 | -3 | -1.1% | 185 | 374 | 375 | -1 | -0.2% |
| | | WBT | 193 | 309 | 162 | 235 | 72.0 | 79.9 | -8.0 | -9.9% | E | E | 63 | 57 | 6 | 10.4% | 342 | 366 | 361 | 5 | 1.3% |
| | | All | 1734 | 2012 | 1752 | 1903 | 76.3 | 53.6 | 22.7 | 42.3% | E | D | 230 | 120 | 111 | 92.8% | | 540 | 512 | 28 | 5.4% |
| | | EBR | 151 | 147 | 176 | 176 | 54.3 | 46.6 | 7.7 | 16.6% | D | D | 56 | 54 | 2 | 3.5% | 318 | 240 | 224 | 16 | 7.2% |
| | Mangum Street at Ramseur | EBT | 327 | 331 | 335 | 333 | 9.7 | 9.4 | 0.3 | 3.1% | Α | Α | 56 | 54 | 2 | 3.5% | 318 | 240 | 224 | 16 | 7.2% |
| 18 | Street ¹ | SBL | 62 | 73 | 56 | 61 | 41.5 | 29.3 | 12.2 | 41.7% | D | С | 245 | 213 | 32 | 15.1% | 225 | 331 | 335 | -4 | -1.2% |
| | | SBT | 1076 | 1228 | 1151 | 1229 | 39.3 | 28.2 | 11.1 | 39.5% | D | С | 245 | 213 | 32 | 15.1% | 225 | 331 | 335 | -4 | -1.2% |
| | | All | 1617 | 1779 | 1718 | 1799 | 34.9 | 26.5 | 8.4 | 31.7% | С | С | 150 | 133 | 17 | 12.8% | | 333 | 335 | -2 | -0.5% |



| | 1 | | Volume (| VPH) | Volume (| VPH) | | Dela | ay (Seconds) | | LC | os | | Avg C | Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|-----------------------------|----------|----------|--------|----------|--------|-------|-------|--------------|-----------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|-------|-------------|------------|
| Node | Intersection | Movement | Build | 1 | No-Bui | ild | | No- | | | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | Difference % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | 1 | EBR | 100 | 101 | 119 | 122 | 5.0 | 15.8 | -10.7 | -68.1% | Α | В | 5 | 15 | -9 | -63.4% | 375 | 157 | 254 | -97 | -38.1% |
| | 1 | EBT | 104 | 103 | 143 | 142 | 19.9 | 23.5 | -3.6 | -15.4% | В | С | 12 | 29 | -17 | -59.0% | 375 | 178 | 290 | -112 | -38.8% |
| | 1 | EBT LRT | 6 | 6 | N/A | N/A | 7.9 | N/A | N/A | N/A | Α | N/A | 2 | N/A | N/A | N/A | | 187 | N/A | N/A | N/A |
| | 1 | SBL | 42 | 47 | 56 | 58 | 2.0 | 0.6 | 1.4 | 216.0% | Α | Α | 2 | 0 | 2 | 3712.5% | 82 | 118 | 44 | 75 | 171.1% |
| 19 | 8 | SBR | | | 28 | 29 | | 0.3 | | | | Α | | 0 | | | 82 | | 34 | | |
| 13 | Street ¹ | SBT | 1182 | 1328 | 1243 | 1318 | 0.8 | 0.3 | 0.6 | 195.6% | Α | Α | 2 | 0 | 2 | 3712.5% | 82 | 118 | 44 | 75 | 171.1% |
| | 1 | WBL | 100 | 101 | 122 | 123 | 5.0 | 68.3 | -63.2 | -92.6% | Α | E | 5 | 55 | -50 | -90.3% | 353 | 157 | 302 | -145 | -47.9% |
| | 1 | WBT | | | 185 | 181 | | 33.7 | | | | С | | 36 | | | 400 | | 241 | | |
| | 1 | WBT LRT | 6 | 6 | N/A | N/A | 0.7 | N/A | N/A | N/A | Α | N/A | 3 | N/A | N/A | N/A | | 112 | N/A | N/A | N/A |
| | | All | 1456 | 1579 | 1897 | 1973 | 2.7 | 10.7 | -8.0 | -74.7% | Α | В | 4 | 19 | -15 | -78.8% | | 218 | 382 | -163 | -42.8% |
| | 1 | EBL | 154 | 155 | 25 | 26 | 16.8 | 11.6 | 5.2 | 44.7% | В | В | 15 | 2 | 13 | 744.4% | 153 | 186 | 57 | 130 | 229.1% |
| | 1 | EBR | 9 | 9 | 27 | 27 | 6.9 | 9.7 | -2.7 | -28.2% | Α | Α | 1 | 4 | -3 | -83.3% | 917 | 67 | 150 | -82 | -55.1% |
| | 1 | EBT | 99 | 103 | 195 | 197 | 11.0 | 12.2 | -1.2 | -9.8% | В | В | 5 | 12 | -7 | -58.7% | 917 | 105 | 179 | -74 | -41.5% |
| | 1 | EBT LRT | 6 | 6 | N/A | N/A | 0.9 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 125 | N/A | N/A | N/A |
| | 1 | NBL | | | 53 | 51 | | 25.0 | | | | С | | 6 | | | 155 | | 89 | | |
| | 1 | NBR | 4 | 4 | 72 | 69 | 19.4 | 14.1 | 5.3 | 37.5% | В | В | 19 | 21 | -2 | -8.6% | 822 | 212 | 231 | -19 | -8.1% |
| | Pettigrew Street at Dillard | NBT | 193 | 188 | 251 | 251 | 23.0 | 16.6 | 6.4 | 38.6% | С | В | 26 | 28 | -2 | -6.8% | 822 | 224 | 245 | -21 | -8.5% |
| 20 | Street ² | SBL | 137 | 133 | 97 | 96 | 35.5 | 24.6 | 10.9 | 44.6% | D | С | 64 | 46 | 18 | 39.8% | 264 | 292 | 252 | 40 | 15.8% |
| | 1 | SBR | | | 16 | 16 | | 13.4 | | | | В | | 33 | | | 264 | | 225 | | |
| | | SBT | 221 | 217 | 244 | 238 | 23.5 | 16.9 | 6.7 | 39.4% | С | В | 64 | 46 | 18 | 39.8% | 264 | 292 | 252 | 40 | 15.8% |
| | | WBL | 9 | 9 | 67 | 69 | 21.8 | 17.8 | 4.0 | 22.6% | С | В | 9 | 10 | -2 | -15.7% | 695 | 133 | 183 | -49 | -27.0% |
| | | WBR | 87 | 89 | 32 | 32 | 23.3 | 11.7 | 11.6 | 99.5% | С | В | 9 | 6 | 2 | 39.3% | 695 | 133 | 168 | -35 | -20.7% |
| | | WBT | | | 78 | 78 | | 16.3 | | | | В | | 10 | | | 695 | | 183 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 5.2 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 932 | 907 | 1158 | 1150 | 22.3 | 16.5 | 5.8 | 35.4% | С | В | 23 | 19 | 4 | 22.7% | | 296 | 277 | 19 | 6.9% |



| | | | Volume (| VPH) | Volume | (VPH) | | Dela | ay (Seconds) | | L | OS | | Avg C | Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|----------------------------------|----------|----------|--------|--------|--------|-------|-------|--------------|-----------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|-------|-------------|------------|
| Node | Intersection | Movement | Build | | No-B | uild | | No- | | | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | Difference % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 5 | 5 | 10 | 10 | 42.9 | 38.7 | 4.3 | 11.0% | D | D | 1 | 2 | -1 | -41.7% | 210 | 25 | 38 | -13 | -33.3% |
| | | EBR | 67 | 66 | 126 | 124 | 10.4 | 29.3 | -18.9 | -64.6% | В | С | 0 | 17 | -17 | -99.7% | 273 | 12 | 156 | -144 | -92.3% |
| | | EBT | 124 | 125 | 180 | 180 | 42.0 | 45.2 | -3.2 | -7.1% | D | D | 30 | 48 | -18 | -38.0% | 696 | 233 | 281 | -47 | -16.9% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 5.1 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | 6 | 6 | 20 | 19 | 8.8 | 5.2 | 3.7 | 70.9% | Α | Α | 7 | 2 | 5 | 232.2% | 70 | 138 | 64 | 74 | 115.6% |
| | | NBR | 146 | 146 | 128 | 133 | 0.4 | 0.5 | -0.1 | -27.7% | Α | Α | 8 | 2 | 6 | 322.4% | 70 | 133 | 64 | 69 | 107.2% |
| | Fayetteville Street at | NBT | 364 | 372 | 429 | 436 | 2.4 | 1.1 | 1.3 | 118.6% | Α | Α | 7 | 2 | 5 | 232.2% | 70 | 138 | 64 | 74 | 115.6% |
| 21 | Pettigrew Street ¹ | SBL | 76 | 75 | 43 | 42 | 61.1 | 25.8 | 35.4 | 137.4% | Е | С | 36 | 6 | 30 | 538.7% | 250 | 384 | 148 | 236 | 160.0% |
| | | SBR | 2 | 2 | 4 | 4 | 47.4 | 24.9 | 22.5 | 90.4% | D | С | 190 | 91 | 99 | 107.9% | 400 | 414 | 405 | 10 | 2.4% |
| | | SBT | 693 | 692 | 670 | 667 | 63.7 | 27.0 | 36.6 | 135.5% | E | С | 190 | 91 | 99 | 107.9% | 400 | 414 | 405 | 10 | 2.4% |
| | | WBL | 119 | 125 | 123 | 131 | 72.4 | 143.1 | -70.7 | -49.4% | Е | F | 49 | 133 | -84 | -63.5% | 100 | 299 | 474 | -176 | -37.0% |
| | | WBR | 62 | 60 | 39 | 40 | 23.4 | 65.4 | -41.9 | -64.2% | С | E | 19 | 62 | -42 | -69.0% | 1570 | 210 | 378 | -168 | -44.4% |
| | | WBT | 47 | 46 | 84 | 83 | 48.0 | 64.0 | -16.0 | -25.1% | D | E | 19 | 62 | -42 | -69.0% | 1570 | 210 | 378 | -168 | -44.4% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 1723 | 1720 | 1855 | 1869 | 39.7 | 31.1 | 8.6 | 27.7% | D | С | 40 | 43 | -3 | -8.1% | | 415 | 500 | -85 | -17.0% |
| | | NBL | 381 | 385 | 309 | 308 | 43.3 | 17.8 | 25.6 | 144.2% | D | В | 120 | 29 | 92 | 321.1% | 277 | 375 | 275 | 100 | 36.5% |
| | | NBT | 511 | 519 | 560 | 567 | 26.4 | 10.8 | 15.6 | 144.4% | С | В | 78 | 20 | 58 | 287.6% | 286 | 381 | 240 | 141 | 58.8% |
| | | SBR | 4 | 5 | 30 | 31 | 3.6 | 6.9 | -3.2 | -46.9% | Α | Α | 21 | 40 | -19 | -47.1% | 70 | 178 | 195 | -17 | -8.7% |
| 22 | Fayetteville Street at Jackie | SBT | 875 | 878 | 889 | 891 | 6.1 | 7.2 | -1.0 | -14.4% | Α | Α | 27 | 40 | -13 | -31.8% | 70 | 198 | 195 | 3 | 1.7% |
| | Robinson Drive ¹ | WBL | 158 | 155 | 157 | 151 | 45.2 | 43.9 | 1.3 | 3.1% | D | D | 45 | 44 | 0 | 0.9% | 345 | 241 | 239 | 2 | 0.7% |
| | | WBR | 5 | 5 | 17 | 21 | 8.1 | 41.5 | -33.4 | -80.4% | Α | D | 35 | 44 | -9 | -21.4% | 345 | 228 | 239 | -11 | -4.7% |
| | | WBT | 5 | 5 | 8 | 8 | 38.7 | 42.9 | -4.3 | -9.9% | D | D | 45 | 44 | 0 | 0.9% | 603 | 241 | 239 | 2 | 0.7% |
| | | All | 1940 | 1952 | 1970 | 1977 | 22.1 | 13.2 | 8.8 | 66.8% | С | В | 53 | 37 | 16 | 41.9% | | 381 | 288 | 93 | 32.4% |
| | | EBL | 120 | 123 | 129 | 130 | 54.6 | 54.5 | 0.0 | 0.1% | D | D | 39 | 43 | -4 | -9.4% | 1260 | 205 | 214 | -9 | -4.2% |
| | | EBR | 0 | 0 | 18 | 17 | 0.0 | 6.7 | -6.7 | -100.0% | Α | Α | 18 | 21 | -3 | -14.6% | 1195 | 172 | 181 | -9 | -5.0% |
| | | EBT | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 39 | 43 | -4 | -9.4% | 1260 | 205 | 214 | -9 | -4.2% |
| 23 | Morehead Avenue at | NBR | 0 | 0 | 3 | 3 | 0.0 | 2.6 | -2.6 | -100.0% | Α | Α | 5 | 3 | 2 | 84.6% | 389 | 120 | 101 | 19 | 18.8% |
| | Fayetteville Street ¹ | NBT | 774 | 781 | 739 | 745 | 7.4 | 3.2 | 4.2 | 133.0% | Α | Α | 9 | 6 | 3 | 55.9% | 389 | 138 | 119 | 19 | 16.0% |
| | | SBL | 131 | 131 | 147 | 146 | 11.6 | 6.2 | 5.4 | 86.9% | В | Α | 6 | 2 | 3 | 160.4% | 255 | 171 | 86 | 86 | 100.1% |
| | | SBT | 903 | 902 | 899 | 896 | 5.7 | 2.4 | 3.3 | 136.0% | Α | Α | 17 | 5 | 12 | 233.7% | 275 | 355 | 109 | 246 | 225.9% |
| | | All | 1927 | 1937 | 1935 | 1937 | 9.9 | 6.5 | 3.3 | 51.2% | Α | Α | 19 | 18 | 1 | 8.0% | | 355 | 214 | 141 | 66.1% |



| | | | Volume (| VPH) | Volume | (VPH) | | Dela | y (Seconds) | | LC | os | | Avg C | Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|---------------------------|----------|-----------|-----------|-----------|-----------|-------------|-------------|-------------|-----------------|--------|----------|-------|-----------|--------------|----------------|--------------------|-----------|------------|--------------|--------------|
| Node | Intersection | Movement | Build | | No-B | uild | | No- | | -166 | | No- | | No- | -166 | Difference | Storage | | No- | - 166 | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | Difference % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 37 | 39 | 25 | 27 | 16.6 | 17.5 | -0.9 | -5.0% | В | В | 3 | 32 | -30 | -91.9% | 155 | 59 | 291 | -232 | -79.9% |
| | | EBR | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 17 | 0 | 17 | 0.0% | 1570 | 210 | 0 | 210 | 0.0% |
| | | EBT | 308 | 307 | 324 | 328 | 11.0 | 15.9 | -4.9 | -31.0% | В | В | 17 | 32 | -15 | -47.0% | 1570 | 210 | 291 | -80 | -27.6% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | NBL | 59 | 58 | 53 | 54 | 28.6 | 25.5 | 3.2 | 12.4% | С | С | 31 | 44 | -13 | -30.0% | 625 | 255 | 306 | -51 | -16.5% |
| | | NBR | 97 | 97 | 188 | 185 | 18.6 | 21.4 | -2.8 | -13.1% | В | С | 23 | 35 | -11 | -33.0% | 625 | 241 | 290 | -49 | -17.0% |
| | Pettigrew Street at Grant | NBT | 87 | 83 | 123 | 119 | 27.8 | 25.0 | 2.8 | 11.3% | С | С | 31 | 44 | -13 | -30.0% | 625 | 255 | 306 | -51 | -16.5% |
| 24 | Street ² | SBL | 123 | 118 | 137 | 134 | 35.4 | 25.9 | 9.6 | 37.0% | D | С | 47 | 23 | 23 | 99.1% | 266 | 315 | 255 | 60 | 23.6% |
| | | SBR | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 | 0.0% | Α | Α | 47 | 14 | 33 | 236.6% | 266 | 315 | 241 | 75 | 31.0% |
| | | SBT | 109 | 107 | 61 | 59 | 32.5 | 21.4 | 11.1 | 52.1% | С | C | 47 | 23 | 23 | 99.1% | 266 | 315 | 255 | 60 | 23.6% |
| | | WBL | 214 | 215 | 137 | 140 | 17.0 | 16.2 | 0.8 | 4.9% | В | В | 16 | 9 | 7 | 82.8% | 70 | 184 | 118 | 66 | 56.1% |
| | | WBR | 92 168 | 92 173 | 92 193 | 92 200 | 10.7 | 8.3 | 2.4 | 29.2% | В | A | 12 | 7 | 5 | 76.1% 20.7% | 193 193 | 197 | 140 | 57 48 | 40.7% |
| | | WBT LRT | 6 | 6 | N/A | N/A | 11.1 5.1 | 11.0 N/A | 0.2 N/A | 1.6% N/A | В | B N/A | 13 | 11 N/A | 2 N/A | N/A | 193 | 199 | 151 N/A | 48 N/A | 32.0% N/A |
| | | All | 1306 | 1289 | 1334 | 1338 | 18.7 | 18.0 | 0.6 | 3.5% | A B | В | 22 | 23 | -1 | -5.5% | | 330 | 332 | -2 | -0.7% |
| | | EBR | 157 | 157 | 121 | 121 | 4.0 | 2.9 | 1.1 | 37.1% | A | Δ | 0 | 0 | 0 | 0.0% | 206 | 33U /l | 0 | - <u>-</u> Z | 0.0% |
| | | EBT | 413 | 410 | 501 | 496 | 4.3 | 2.8 | 1.5 | 52.2% | A | Δ | 0 | 0 | 0 | 0.0% | 206 | 4 | 0 | 4 | 0.0% |
| | Gann Street at Pettigrew | NBL | 125 | 128 | 169 | 172 | 15.6 | 15.7 | -0.1 | -0.4% | С | C | 3 | 3 | 0 | -0.2% | 248 | 125 | 122 | 3 | 2.5% |
| 25 | Street ² | NBR | 88 | 87 | 44 | 43 | 13.4 | 13.1 | 0.3 | 1.9% | В | В | 3 | 3 | 0 | -0.2% | 248 | 125 | 122 | 3 | 2.5% |
| | (Unsignalized) | WBL | 27 | 26 | 64 | 63 | 8.8 | 10.1 | -1.3 | -13.2% | Α | В | 0 | 0 | 0 | -100.0% | 367 | 13 | 39 | -26 | -66.7% |
| | | WBT | 414 | 420 | 350 | 357 | 0.6 | 0.5 | 0.1 | 21.5% | Α | Α | 0 | 0 | 0 | 0.0% | 367 | 0 | 0 | 0 | 0.0% |
| | | All | 1225 | 1228 | 1249 | 1252 | 4.9 | 4.7 | 0.3 | 5.4% | Α | Α | 1 | 1 | 0 | -0.6% | | 125 | 122 | 3 | 2.5% |
| | | EBL | 33 | 34 | 30 | 31 | 52.8 | 56.0 | -3.2 | -5.8% | D | Е | 10 | 10 | 0 | -3.9% | 196 | 130 | 156 | -26 | -16.8% |
| | | EBR | 176 | 175 | 188 | 186 | 6.9 | 7.2 | -0.3 | -4.4% | Α | Α | 4 | 6 | -2 | -28.6% | 196 | 119 | 151 | -33 | -21.5% |
| | | NBL | 128 | 128 | 136 | 137 | 19.0 | 18.6 | 0.4 | 2.1% | В | В | 45 | 47 | -2 | -4.9% | 300 | 426 | 395 | 31 | 7.8% |
| | | NBT | 1474 | 1484 | 1490 | 1500 | 8.9 | 9.7 | -0.8 | -8.2% | Α | Α | 45 | 47 | -2 | -4.9% | 528 | 426 | 395 | 31 | 7.8% |
| 26 | Alston Avenue at Gann | SBR | 21 | 20 | 23 | 22 | 13.1 | 10.2 | 2.9 | 28.5% | В | В | 70 | 51 | 19 | 36.1% | 190 | 521 | 208 | 313 | 150.3% |
| 20 | Street ¹ | SBT | 1359 | 1346 | 1360 | 1355 | 14.9 | 13.4 | 1.5 | 10.8% | В | В | 72 | 59 | 13 | 22.4% | 1037 | 524 | 223 | 301 | 134.7% |
| | | WBL | 154 | 153 | 151 | 150 | 39.4 | 55.3 | -16.0 | -28.8% | D | E | 36 | 52 | -16 | -31.2% | 188 | 234 | 300 | -67 | -22.2% |
| | | WBR | 153 | 150 | 150 | 147 | 11.6 | 11.9 | -0.3 | -2.8% | В | В | 1 | 1 | 0 | 9.2% | 1000 | 78 | 80 | -2 | -2.1% |
| | | WBT | 1 | 1 | 1 | 1 | 34.2 | 24.4 | 9.7 | 39.8% | С | С | 4 | 4 | 0 | 12.7% | 1000 | 102 | 103 | -1 | -0.6% |
| | | All | 3500 | 3491 | 3529 | 3529 | 13.4 | 13.8 | -0.4 | -2.9% | В | В | 32 | 31 | 1 | 3.4% | | 534 | 409 | 125 | 30.6% |



| | | | Volume (| VPH) | Volume | (VPH) | | Dela | y (Seconds) | | LC | OS | | Avg C | Queue Length | (ft) | | Max | Queue | Length (ft) | |
|------|----------------------------------------|----------|----------|--------|--------|--------|-------|-------|-------------|-----------------|-------|-------|-------|-------|--------------|------------|--------------------|-------|-------|-------------|------------|
| Node | Intersection | Movement | Build | | No-Bu | ıild | | No- | | | | No- | | No- | | Difference | Storage | | No- | | Difference |
| | | | Model | Demand | Model | Demand | Build | Build | Difference | Difference % | Build | Build | Build | Build | Difference | % | Space Available | Build | Build | Difference | % |
| | | EBL | 35 | 36 | 77 | 77 | 29.9 | 26.4 | 3.5 | 13.3% | С | С | 15 | 15 | 0 | 0.7% | 220 | 165 | 139 | 26 | 18.6% |
| | | EBT | 111 | 114 | 122 | 123 | 24.3 | 14.7 | 9.6 | 65.2% | С | В | 15 | 15 | 0 | 0.7% | 288 | 165 | 139 | 26 | 18.6% |
| | | EBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 0 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | , | NBL | | | 206 | 205 | | 20.9 | | | | С | | 110 | | | 541 | | 474 | | |
| 27 | Roxboro Street at Pettigrew | NBR | 151 | 153 | 127 | 127 | 17.7 | 7.9 | 9.8 | 124.8% | В | Α | 83 | 99 | -16 | -15.8% | 541 | 273 | 458 | -185 | -40.5% |
| 27 | Street ¹ | NBT | 1561 | 1577 | 1228 | 1244 | 18.3 | 20.5 | -2.2 | -10.8% | В | С | 94 | 110 | -16 | -14.6% | 541 | 290 | 474 | -184 | -38.9% |
| | | WBR | | | 46 | 46 | | 19.5 | | | | В | | 13 | | | 916 | | 163 | | |
| | , | WBT | | | 101 | 99 | | 28.5 | | | | С | | 20 | | | 916 | | 178 | | |
| | | WBT LRT | 6 | 6 | N/A | N/A | 0.0 | N/A | N/A | N/A | Α | N/A | 1 | N/A | N/A | N/A | | 0 | N/A | N/A | N/A |
| | | All | 1883 | 1880 | 1907 | 1921 | 18.7 | 20.0 | -1.3 | -6.5% | В | В | 43 | 54 | -11 | -20.7% | | 290 | 474 | -184 | -38.9% |
| | | EBT LRT | 6 | 6 | | | 0.0 | | | | Α | | 0 | | | | | 0 | | | |
| | ! | NBT | 452 | 462 | | | 51.6 | | | | F | | 128 | | | | | 215 | | | |
| 28 | LRT at Buchanan Boulevard ² | SBT | 345 | 361 | | | 3.4 | | | | Α | | 7 | | | | | 299 | | | |
| | ! | WBT LRT | 6 | 6 | | | 5.1 | | | | Α | | 9 | | | | | 235 | | | |
| | | All | 809 | 823 | | | 30.3 | | | | D | | 36 | | | | | 301 | | | |
| | Downtown Durham Corridor | EB LRT | 6 | 6 | | | 19.0 | | | | | | | | | | | | | | |
| | Downtown Durham Corridor | WB LRT | 6 | 6 | | | 22.0 | | | | | | | | | | | | | | |
| | | All | 46659 | 49803 | 46792 | 50848 | 29.5 | 27.7 | | | С | С | 77 | 88 | -10 | -11.6% | | 845 | 851 | -6 | -0.7% |

1 - NCDOT Traffic Impact Criteria is applied

2 - City of Durham Traffic Impact Criteria is applied

Indicates LRT Movement
Indicates Traffic Impact

Indicates Traffic Impact below Mid-D

Build Max Queue length exceeds No-Build and Storage Space by more than 10 feet



Table 13: D-O LRT: Downtown Durham – Synchro Intersection Analysis - 2040 Build One-Way Pettigrew VS 2040 No-Build AM Peak Hour 8:00 AM – 9:00 AM

| | | | | Del | ay (Seconds) | | | LOS | | V/C | | | 95% Queue | e Length | |
|------|---------------------------------|----------|-------|----------|--------------|-----------------|-------|----------|-------|----------|------------------|-------|-----------|------------|-----------------|
| Node | Intersection | Movement | Build | No-Build | Difference | Difference % | Build | No-Build | Build | No-Build | Storage Space | Build | No-Build | Difference | Difference % |
| | | EBT | 4.2 | 9.3 | -5.1 | -54.8% | Α | Α | 0.16 | 0.38 | 239 | 28 | 188 | -160 | -85.1% |
| | | EBR | 0.1 | 0.1 | 0 | 0.0% | Α | Α | 0.09 | 0.06 | 239 | 0 | 0 | 0 | - |
| 1 | Downtown Loop at | WBLT | 3.8 | 5.9 | -2.1 | -35.6% | Α | Α | 0.04 | 0.11 | 232 | 11 | 43 | -32 | -74.4% |
| _ | Chapel Hill Street ¹ | SBT | 16.4 | 16.5 | -0.1 | -0.6% | В | В | 0.13 | 0.25 | 185 | 26 | 43 | -17 | -39.5% |
| | | SBR | 0.9 | 1.8 | -0.9 | -50.0% | Α | Α | 0.22 | 0.25 | 185 | 23 | 76 | -53 | -69.7% |
| | | Overall | 4.8 | 8.2 | -3.4 | -41.5% | Α | А | | | | | | | |
| | | SBLTR | 17.2 | 16.6 | 0.6 | 3.6% | В | В | 0.33 | 0.29 | 441 | 111 | 97 | 14 | 14.4% |
| | Great Jones Street at | EBT | 10.6 | 10.6 | 0 | 0.0% | В | В | 0.24 | 0.24 | 306 | 108 | 108 | 0 | 0.0% |
| 2 | W Main Street ¹ | EBR | 4.6 | 2 | 2.6 | 130.0% | Α | Α | 0.22 | 0.18 | 148 | 51 | 26 | 25 | 96.2% |
| | W Wall Street | WLT | 14.8 | 18.9 | -4.1 | -21.7% | В | В | 0.13 | 0.12 | 298 | 108 | 125 | -17 | -13.6% |
| | | Overall | 14 | 13.7 | 0.3 | 2.2% | В | В | | | | | | | |
| | | WBTR | 7.3 | 5.2 | 2.1 | 40.4% | Α | Α | 0.31 | 0.25 | 557 | 28 | 50 | -22 | -44.0% |
| | Great Jones Street at | NBL | 28.2 | 29.8 | -1.6 | -5.4% | С | С | 0.45 | 0.27 | 360 | 110 | 72 | 38 | 52.8% |
| 3 | Morris Street ¹ | NBT | 26.3 | 29.6 | -3.3 | -11.1% | С | С | 0.30 | 0.26 | 360 | 81 | 73 | 8 | 11.0% |
| | | SBR | 7.8 | 2.4 | 5.4 | 225.0% | Α | Α | 0.41 | 0.36 | 227 | 94 | 31 | 63 | 203.2% |
| | | Overall | 11.7 | 8.8 | 2.9 | 33.0% | В | А | | | | | | | |
| | | EBLTR | 25.7 | 20.3 | 5.4 | 26.6% | С | С | 0.54 | 0.64 | 232 | 242 | 320 | -78 | -24.4% |
| | E Chapel Hill Street/ | WBLTR | 10.9 | 10.7 | 0.2 | 1.9% | В | В | 0.16 | 0.13 | 461 | 66 | 54 | 12 | 22.2% |
| 4 | Main Street at Morris | SBLT | 46.4 | 35.1 | 11.3 | 32.2% | D | D | 0.77 | 0.54 | 298 | 321 | 231 | 90 | 39.0% |
| | Street ² | NBLTR | 14.2 | 9.3 | 4.9 | 52.7% | В | Α | 0.61 | 0.40 | 460 | 241 | 48 | 193 | 402.1% |
| | | Overall | 27 | 20.6 | 6.4 | 31.1% | С | С | | | | | | | |
| | | WBLTR | 4.3 | 4.9 | -0.6 | -12.2% | Α | Α | 0.39 | 0.34 | 454 | 24 | 25 | -1 | -4.0% |
| | Morgan Street at | NBL | 8.1 | 7.9 | 0.2 | 2.5% | Α | А | 0.04 | 0.08 | 360 | 14 | 25 | -11 | -44.0% |
| 5 | Foster Street ¹ | NBT | 10.5 | 9.2 | 1.3 | 14.1% | В | А | 0.22 | 0.31 | 360 | 117 | 132 | -15 | -11.4% |
| | | SBTR | 9.5 | 10.6 | -1.1 | -10.4% | Α | В | 0.31 | 0.33 | 365 | 120 | 137 | -17 | -12.4% |
| | | Overall | 6.3 | 7 | -0.7 | -10.0% | Α | А | | | | | | | |



| | | | | Del | ay (Seconds) | | | LOS | | V/C | | | 95% Queue | e Length | |
|------|------------------------------------------------|----------|-------|----------|--------------|-----------------|-------|----------|-------|----------|------------------|-------|-----------|------------|-----------------|
| Node | Intersection | Movement | Build | No-Build | Difference | Difference % | Build | No-Build | Build | No-Build | Storage Space | Build | No-Build | Difference | Difference % |
| | | EBLTR | 13.2 | 16.1 | -2.9 | -18.0% | В | В | 0.06 | 0.04 | 341 | 28 | 26 | 2 | 7.7% |
| | | EBR | 13.3 | 16.1 | -2.8 | -17.4% | В | В | 0.06 | 0.04 | 341 | 33 | 28 | 5 | 17.9% |
| | | WBL | 1.3 | 1.4 | -0.1 | -7.1% | Α | Α | 0.13 | 0.16 | 750 | 6 | 5 | 1 | 20.0% |
| | Blackwell Street at | WBT | 1.9 | 1.8 | 0.1 | 5.6% | Α | А | 0.38 | 0.31 | 750 | 18 | 10 | 8 | 80.0% |
| 6 | Jackie Robinson | WBR | 1.2 | 1.1 | 0.1 | 9.1% | Α | А | 0.11 | 0.08 | 750 | 6 | 3 | 3 | 100.0% |
| | Drive ¹ | NBL | 25.7 | 26.2 | -0.5 | -1.9% | С | С | 0.32 | 0.34 | 201 | 104 | 112 | -8 | -7.1% |
| | | NBT | 24.6 | 24.5 | 0.1 | 0.4% | С | С | 0.29 | 0.29 | 201 | 126 | 125 | 1 | 0.8% |
| | | SBTR | 25.6 | 31.6 | -6 | -19.0% | С | С | 0.16 | 0.15 | 768 | 85 | 89 | -4 | -4.5% |
| | | Overall | 11.4 | 12.8 | -1.4 | -10.9% | В | В | | | | | | | |
| | | WBLTR | 1.7 | 1.9 | -0.2 | -10.5% | Α | А | 0.34 | 0.30 | 418 | 16 | 15 | 1 | 6.7% |
| 7 | Morgan Street at | NBLT | 16.1 | 17 | -0.9 | -5.3% | В | В | 0.09 | 0.17 | 352 | 47 | 78 | -31 | -39.7% |
| ' | Rigsbee Avenue ¹ | SBTR | 9.5 | 14.4 | -4.9 | -34.0% | Α | В | 0.18 | 0.19 | 314 | 60 | 80 | -20 | -25.0% |
| | | Overall | 3.2 | 4.7 | -1.5 | -31.9% | Α | А | | | | | | | |
| | | NBLT | 24.1 | 23.4 | 0.7 | 3.0% | С | С | 0.64 | 0.59 | 206 | 243 | 213 | 30 | 14.1% |
| 8 | Morgan Street at | WBT | 9.7 | 9.5 | 0.2 | 2.1% | Α | Α | 0.54 | 0.54 | 215 | 235 | 240 | -5 | -2.1% |
| | Mangum Street ¹ | WBR | 6.7 | 6.2 | 0.5 | 8.1% | Α | Α | 0.21 | 0.20 | 215 | 74 | 67 | 7 | 10.4% |
| | | Overall | 16.7 | 15.8 | 0.9 | 5.7% | В | В | | | | | | | |
| | Maria e Charalat | WBLT | 29.3 | 29 | 0.3 | 1.0% | С | С | 0.60 | 0.60 | 506 | 239 | 223 | 16 | 7.2% |
| 9 | Mangum Street at Jackie Robinson | SBT | 13.7 | 11.1 | 2.6 | 23.4% | В | В | 0.24 | 0.24 | 458 | 198 | 182 | 16 | 8.8% |
| | Drive ¹ | SBR | 11.1 | 7.7 | 3.4 | 44.2% | В | Α | 0.21 | 0.18 | 228 | 161 | 111 | 50 | 45.0% |
| | | Overall | 20.7 | 18.8 | 1.9 | 10.1% | С | В | | | | | | | |
| | | WBT | 29.9 | 30.9 | -1 | -3.2% | С | С | 0.65 | 0.64 | 913 | 274 | 269 | 5 | 1.9% |
| 10 | Holloway Street at | WBR | 0.1 | 0.1 | 0 | 0.0% | Α | Α | 0.08 | 0.08 | 913 | 0 | 0 | 0 | - |
| 10 | Roxboro Street ¹ | NBLTR | 10.9 | 10.3 | 0.6 | 5.8% | В | В | 0.22 | 0.22 | 225 | 100 | 99 | 1 | 1.0% |
| | | Overall | 16.3 | 16 | 0.3 | 1.9% | В | В | | | | | | | |
| | | EBL | 33.9 | 33.8 | 0.1 | 0.3% | С | С | 0.46 | 0.46 | 276 | 118 | 116 | 2 | 1.7% |
| | Liborty Loop of | EBT | 32.6 | 32.7 | -0.1 | -0.3% | С | С | 0.33 | 0.34 | 326 | 81 | 81 | 0 | 0.0% |
| 11 | Liberty Loop at Roxboro Street ¹ | NBL | 0.8 | 0.7 | 0.1 | 14.3% | Α | А | 0.21 | 0.15 | 460 | 15 | 11 | 4 | 36.4% |
| | 110/10010 011 000 | NBTR | 0.8 | 0.7 | 0.1 | 14.3% | Α | Α | 0.15 | 0.16 | 460 | 11 | 12 | -1 | -8.3% |
| | | Overall | 8.5 | 9.3 | -0.8 | -8.6% | Α | А | | | | | | | |



| | | | | Del | ay (Seconds) | | | LOS | | V/C | | | 95% Queue | e Length | |
|------|--------------------------------|----------|-------|----------|--------------|-----------------|-------|----------|-------|----------|------------------|-------|-----------|------------|-----------------|
| Node | Intersection | Movement | Build | No-Build | Difference | Difference % | Build | No-Build | Build | No-Build | Storage Space | Build | No-Build | Difference | Difference % |
| | | EBL | 15.9 | 22.2 | -6.3 | -28.4% | В | С | 0.32 | 0.25 | 148 | 55 | 52 | 3 | 5.8% |
| | | EBT | 15.7 | 22.2 | -6.5 | -29.3% | В | С | 0.43 | 0.40 | 293 | 192 | 184 | 8 | 4.3% |
| 12 | Main Street at | WBT | 18.9 | 19 | -0.1 | -0.5% | В | В | 0.45 | 0.42 | 497 | 221 | 208 | 13 | 6.3% |
| 12 | Roxboro Street ¹ | WBR | 6.5 | 6.1 | 0.4 | 6.6% | Α | Α | 0.20 | 0.22 | 108 | 55 | 53 | 2 | 3.8% |
| | | NBLTR | 21.1 | 12.3 | 8.8 | 71.5% | С | В | 0.90 | 0.78 | 386 | 142 | 298 | -156 | -52.3% |
| | | Overall | 19.1 | 14.5 | 4.6 | 31.7% | В | В | | | | | | | |
| | | EBL | 41.4 | 46.8 | -5.4 | -11.5% | D | D | 0.40 | 0.46 | 345 | 59 | 74 | -15 | - |
| | | EBT | 30.4 | 36.2 | -5.8 | -16.0% | С | D | 0.10 | 0.16 | 564 | 38 | 44 | -6 | -13.6% |
| 13 | Dillard Street at | WBTR | 48.1 | 44.1 | 4 | 9.1% | D | D | 0.75 | 0.57 | 826 | 181 | 111 | 70 | 63.1% |
| 15 | Roxboro Street ¹ | NBLT | 5.5 | 3.8 | 1.7 | 44.7% | Α | Α | 0.60 | 0.55 | 465 | 161 | 124 | 37 | 29.8% |
| | | NBR | 0.4 | 0.3 | 0.1 | 33.3% | Α | Α | 0.11 | 0.10 | 307 | 0 | 0 | 0 | - |
| | | Overall | 10 | 7.2 | 2.8 | 38.9% | Α | А | | | | | | | |
| | | WBT | 8.3 | 8 | 0.3 | 3.8% | Α | Α | 0.36 | 0.32 | 1342 | 133 | 116 | 17 | 14.7% |
| | Jackie Robinson Drive | WBR | 79.3 | 80.5 | -1.2 | -1.5% | Е | F | 1.10 | 1.10 | 1342 | 940 | 944 | -4 | -0.4% |
| 14 | at Roxboro Street ¹ | NBL | 4.5 | 4.6 | -0.1 | -2.2% | Α | Α | 0.29 | 0.27 | 265 | 47 | 45 | 2 | 4.4% |
| | | NBT | 30.5 | 30.1 | 0.4 | 1.3% | С | С | 0.74 | 0.73 | 265 | 275 | 268 | 7 | 2.6% |
| | | Overall | 39.5 | 40.8 | -1.3 | -3.2% | D | D | | | | | | | |
| | | EBLTR | 6.9 | 7.4 | -0.5 | -6.8% | Α | Α | 0.22 | 0.22 | 916 | 50 | 54 | -4 | -7.4% |
| | | WBLTR | 13.5 | 13.7 | -0.2 | -1.5% | В | В | 0.47 | 0.48 | 715 | 226 | 228 | -2 | -0.9% |
| 15 | Dillard Street at | NBL | 19.4 | 22.7 | -3.3 | -14.5% | В | С | 0.38 | 0.39 | 485 | 145 | 156 | -11 | -7.1% |
| | Holloway Street ¹ | NBTR | 6.4 | 9 | -2.6 | -28.9% | Α | Α | 0.04 | 0.05 | 485 | 25 | 25 | 0 | 0.0% |
| | | SBLTR | 13.9 | 14.2 | -0.3 | -2.1% | В | В | 0.12 | 0.11 | 310 | 50 | 47 | 3 | 6.4% |
| | | Overall | 13 | 13.9 | -0.9 | -6.5% | В | В | | | | | | | |
| | | NBTR | 17.8 | 18.2 | -0.4 | -2.2% | В | В | 0.07 | 0.10 | 384 | 41 | 51 | -10 | -19.6% |
| | | SBLT | 13.8 | 13.4 | 0.4 | 3.0% | В | В | 0.13 | 0.13 | 486 | 47 | 50 | -3 | -6.0% |
| | | EBL | 1.7 | 2.1 | -0.4 | -19.0% | Α | Α | 0.03 | 0.10 | 378 | 4 | 11 | -7 | -63.6% |
| 16 | Dillard Street at | EBT | 1.7 | 2 | -0.3 | -15.0% | Α | Α | 0.06 | 0.06 | 378 | 7 | 8 | -1 | -12.5% |
| | Liberty Street ¹ | EBR | 0.2 | 0.1 | 0.1 | 100.0% | Α | Α | 0.09 | 0.02 | 378 | 1 | 0 | 1 | - |
| | | WBL | 9.5 | 9.9 | -0.4 | -4.0% | Α | Α | 0.10 | 0.15 | 397 | 40 | 55 | -15 | -27.3% |
| | | WBR | 2.3 | 2.3 | 0 | 0.0% | Α | Α | 0.10 | 0.10 | 397 | 20 | 19 | 1 | 5.3% |
| | | Overall | 8.5 | 9.2 | -0.7 | -7.6% | А | А | | | | | | | |



| | | | | Del | ay (Seconds) | | | LOS | | V/C | | | 95% Queue | e Length | |
|------|------------------------|----------|-------|----------|--------------|-----------------|-------|----------|-------|----------|------------------|-------|-----------|------------|-----------------|
| Node | Intersection | Movement | Build | No-Build | Difference | Difference % | Build | No-Build | Build | No-Build | Storage Space | Build | No-Build | Difference | Difference % |
| | | EBL | 6.7 | 6.8 | -0.1 | -1.5% | Α | А | 0.04 | 0.05 | 100 | 8 | 12 | -4 | -33.3% |
| | | EBT | 7.3 | 7.1 | 0.2 | 2.8% | Α | А | 0.09 | 0.08 | 365 | 51 | 50 | 1 | 2.0% |
| | | EBR | 3.6 | 3.6 | 0 | 0.0% | Α | А | 0.10 | 0.10 | 100 | 28 | 30 | -2 | -6.7% |
| | | WBL | 6.6 | 6.6 | 0 | 0.0% | Α | Α | 0.06 | 0.06 | 555 | 23 | 23 | 0 | 0.0% |
| 17 | Dillard Street at Main | WBTR | 10.1 | 9.9 | 0.2 | 2.0% | В | Α | 0.48 | 0.47 | 555 | 218 | 212 | 6 | 2.8% |
| 17 | Street ² | NBL | 23.3 | 23.8 | -0.5 | -2.1% | С | С | 0.14 | 0.16 | 147 | 41 | 42 | -1 | -2.4% |
| | | NBTR | 16.7 | 17.7 | -1 | -5.6% | В | В | 0.07 | 0.09 | 396 | 35 | 42 | -7 | -16.7% |
| | | SBL | 21 | 17.8 | 3.2 | 18.0% | С | В | 0.15 | 0.17 | 385 | 62 | 60 | 2 | 3.3% |
| | | SBTR | 15.7 | 14.1 | 1.6 | 11.3% | В | В | 0.35 | 0.42 | 385 | 123 | 135 | -12 | -8.9% |
| | | Overall | 11.3 | 11.1 | 0.2 | 1.8% | В | В | | | | | | | |

- 1 NCDOT Traffic Impact Criteria is applied
- 2 City of Durham Traffic Impact Criteria is applied

Indicates Traffic Impact
Indicates Traffic Impact below Mid-D

Build Max Queue length exceeds No-Build and Storage Space by more than 10 feet



Table 14: D-O LRT: Downtown Durham – Synchro Intersection Analysis - 2040 Build One-Way Pettigrew VS 2040 No-Build PM Peak Hour 5:00 PM – 6:00 PM

| | | | | Del | ay (Seconds) | | | LOS | | V/C | | | 95% Queue | e Length | |
|------|-----------------------------------------------------|----------|-------|----------|------------------------|-----------------|-------|----------|-------|----------|------------------|-------|-----------|------------------------|-----------------|
| Node | Intersection | Movement | Build | No-Build | Difference Absolute | Difference % | Build | No-Build | Build | No-Build | Storage Space | Build | No-Build | Difference Absolute | Difference % |
| | | EBT | 5.8 | 7.3 | -1.5 | -20.5% | Α | Α | 0.27 | 0.37 | 239 | 89 | 126 | -37 | -29.4% |
| | | EBR | 0.1 | 0.0 | 0.1 | - | A | Α | 0.07 | 0.00 | 239 | 0 | 0 | 0 | - |
| | Downtown Loop at | WBLT | 14.0 | 6.3 | 7.7 | 122.2% | В | A | 0.19 | 0.15 | 232 | 122 | 47 | 75 | 159.6% |
| 1 | Chapel Hill Street ¹ | SBT | 11.9 | 12.8 | -0.9 | -7.0% | В | В | 0.29 | 0.30 | 185 | 38 | 43 | -5 | -11.6% |
| | | SBR | 4.2 | 1.9 | 2.3 | 121.1% | Α | А | 0.45 | 0.33 | 185 | 185 | 76 | 109 | 143.4% |
| | | Overall | 7.3 | 7.0 | 0.3 | 4.3% | Α | А | | | | | | | |
| | | SBLTR | 15.9 | 14.6 | 1.3 | 8.9% | В | В | 0.47 | 0.40 | 441 | 134 | 108 | 26 | 24.1% |
| | | EBT | 9.8 | 9.8 | 0.0 | 0.0% | Α | А | 0.35 | 0.35 | 306 | 137 | 136 | 1 | 0.7% |
| 2 | Great Jones Street at W Main Street ¹ | EBR | 7.0 | 5.5 | 1.5 | 27.3% | Α | А | 0.25 | 0.25 | 148 | 71 | 62 | 9 | 14.5% |
| | vv iviairi Street | WLT | 9.2 | 9.0 | 0.2 | 2.2% | Α | А | 0.28 | 0.27 | 298 | 88 | 100 | -12 | -12.0% |
| | | Overall | 12.9 | 11.7 | 1.2 | 10.3% | В | В | | | | | | | |
| | | WBTR | 9.7 | 9.4 | 0.3 | 3.2% | Α | Α | 0.33 | 0.31 | 557 | 56 | 51 | 5 | 9.8% |
| | Great Jones Street at | NBL | 36.6 | 32.2 | 4.4 | 13.7% | D | С | 0.49 | 0.36 | 360 | 111 | 86 | 25 | 29.1% |
| 3 | Morris Street ¹ | NBT | 33.1 | 31.8 | 1.3 | 4.1% | С | С | 0.34 | 0.35 | 360 | 80 | 87 | -7 | -8.0% |
| | 11101113 311 661 | SBR | 12.4 | 11.2 | 1.2 | 10.7% | В | В | 0.48 | 0.51 | 227 | 134 | 134 | 0 | 0.0% |
| | | Overall | 14.4 | 13.1 | 1.3 | 9.9% | В | В | | | | | | | |
| | | EBLTR | 20.8 | 87.4 | -66.6 | -76.2% | С | F | 0.61 | 1.07 | 232 | 234 | 324 | -90 | -27.8% |
| | E Chapel Hill Street/ | WBLTR | 17.7 | 15.7 | 2.0 | 12.7% | В | В | 0.58 | 0.33 | 461 | 216 | 81 | 135 | 166.7% |
| 4 | Main Street at Morris | SBLT | 18.4 | 17.3 | 1.1 | 6.4% | В | В | 0.57 | 0.67 | 298 | 112 | 182 | -70 | -38.5% |
| | Street ² | NBLTR | 16.8 | 8.6 | 8.2 | 95.3% | В | Α | 0.34 | 0.35 | 460 | 128 | 89 | 39 | 43.8% |
| | | Overall | 18.5 | 39.7 | -21.2 | -53.4% | В | D | | | | | | | |
| | | WBLTR | 3.8 | 5.7 | -1.9 | -33.3% | Α | Α | 0.34 | 0.28 | 454 | 13 | 28 | -15 | -53.6% |
| | Morgan Street at | NBL | 10.5 | 11.8 | -1.3 | -11.0% | В | В | 0.12 | 0.20 | 360 | 24 | 39 | -15 | -38.5% |
| 5 | Foster Street ¹ | NBT | 12.4 | 13.4 | -1.0 | -7.5% | В | В | 0.39 | 0.46 | 360 | 160 | 194 | -34 | -17.5% |
| | | SBTR | 12.2 | 12.7 | -0.5 | -3.9% | В | В | 0.51 | 0.51 | 365 | 194 | 196 | -2 | -1.0% |
| | | Overall | 7.9 | 9.7 | -1.8 | -18.6% | Α | Α | | | | | | | |



| | | | | Del | ay (Seconds) | | | LOS | | V/C | | | 95% Queue | Length | |
|------|------------------------------------------------|----------|-------|----------|------------------------|-----------------|-------|----------|-------|----------|------------------|-------|-----------|------------------------|-----------------|
| Node | Intersection | Movement | Build | No-Build | Difference Absolute | Difference % | Build | No-Build | Build | No-Build | Storage Space | Build | No-Build | Difference Absolute | Difference % |
| | | EBLTR | 20.2 | 19.4 | 0.8 | 4.1% | С | В | 0.60 | 0.57 | 341 | 234 | 220 | 14 | 6.4% |
| | | EBR | 20.2 | 19.1 | 1.1 | 5.8% | С | В | 0.60 | 0.56 | 341 | 237 | 215 | 22 | 10.2% |
| | | WBL | 20.5 | 19.5 | 1.0 | 5.1% | С | В | 0.49 | 0.46 | 750 | 108 | 104 | 4 | 3.8% |
| | Blackwell Street at | WBT | 13.2 | 12.8 | 0.4 | 3.1% | В | В | 0.21 | 0.16 | 750 | 84 | 67 | 17 | 25.4% |
| 6 | Jackie Robinson | WBR | 12.5 | 12.2 | 0.3 | 2.5% | В | В | 0.12 | 0.09 | 750 | 46 | 37 | 9 | 24.3% |
| | Drive ¹ | NBL | 15.6 | 15.7 | -0.1 | -0.6% | В | В | 0.19 | 0.19 | 201 | 50 | 52 | -2 | -3.8% |
| | | NBT | 14.6 | 14.7 | -0.1 | -0.7% | В | В | 0.16 | 0.17 | 201 | 68 | 69 | -1 | -1.4% |
| | | SBTR | 17.0 | 16.7 | 0.3 | 1.8% | В | В | 0.37 | 0.34 | 768 | 142 | 134 | 8 | 6.0% |
| | | Overall | 18.0 | 17.5 | 0.5 | 2.9% | В | В | | | | | | | |
| | | WBLTR | 11.5 | 11.0 | 0.5 | 4.5% | В | В | 0.37 | 0.30 | 418 | 108 | 86 | 22 | 25.6% |
| 7 | Morgan Street at | NBLT | 12.5 | 13.6 | -1.1 | -8.1% | В | В | 0.23 | 0.32 | 352 | 81 | 111 | -30 | -27.0% |
| ' | Rigsbee Avenue ¹ | SBTR | 9.0 | 9.4 | -0.4 | -4.3% | Α | Α | 0.15 | 0.16 | 314 | 54 | 57 | -3 | -5.3% |
| | | Overall | 11.4 | 11.3 | 0.1 | 0.9% | В | В | | | | | | | |
| | | NBLT | 21.4 | 21.0 | 0.4 | 1.9% | С | С | 0.58 | 0.52 | 206 | 173 | 138 | 35 | 25.4% |
| 8 | Morgan Street at | WBT | 7.5 | 6.8 | 0.7 | 10.3% | Α | Α | 0.45 | 0.44 | 215 | 160 | 163 | -3 | -1.8% |
| 8 | Mangum Street ¹ | WBR | 5.1 | 3.8 | 1.3 | 34.2% | А | Α | 0.15 | 0.13 | 215 | 45 | 35 | 10 | 28.6% |
| | | Overall | 14.5 | 13.2 | 1.3 | 9.8% | В | В | | | | | | | |
| | | WBLT | 23.8 | 22.8 | 1.0 | 4.4% | С | С | 0.55 | 0.57 | 506 | 138 | 154 | -16 | -10.4% |
| 9 | Mangum Street at Jackie Robinson | SBT | 4.7 | 5.9 | -1.2 | -20.3% | Α | А | 0.30 | 0.33 | 458 | 92 | 110 | -18 | -16.4% |
| 9 | Drive ¹ | SBR | 4.1 | 7.3 | -3.2 | -43.8% | Α | Α | 0.28 | 0.41 | 228 | 67 | 143 | -76 | -53.1% |
| | 2,,,,, | Overall | 10.8 | 11.7 | -0.9 | -7.7% | В | В | | | | | | | |
| | | WBT | 34.2 | 32.8 | 1.4 | 4.3% | С | С | 0.76 | 0.74 | 913 | 274 | 249 | 25 | 10.0% |
| 10 | Holloway Street at | WBR | 0.2 | 0.1 | 0.1 | 100.0% | Α | Α | 0.15 | 0.11 | 913 | 0 | 0 | 0 | - |
| 10 | Roxboro Street ¹ | NBLTR | 3.0 | 3.7 | -0.7 | -18.9% | Α | Α | 0.42 | 0.45 | 225 | 82 | 105 | -23 | -21.9% |
| | | Overall | 8.6 | 8.6 | 0.0 | 0.0% | Α | А | | | | | | | |
| | | EBL | 22.8 | 22.8 | 0.0 | 0.0% | С | С | 0.56 | 0.54 | 276 | 147 | 142 | 5 | 3.5% |
| | Liborty Loop of | EBT | 19.7 | 20.3 | -0.6 | -3.0% | В | С | 0.40 | 0.42 | 326 | 95 | 98 | -3 | -3.1% |
| 11 | Liberty Loop at Roxboro Street ¹ | NBL | 1.5 | 1.4 | 0.1 | 7.1% | Α | А | 0.24 | 0.15 | 460 | 16 | 10 | 6 | 60.0% |
| | NOADOIO SIICCI | NBTR | 1.6 | 1.5 | 0.1 | 6.7% | Α | А | 0.38 | 0.43 | 460 | 24 | 26 | -2 | -7.7% |
| | | Overall | 7.2 | 7.2 | 0.0 | 0.0% | Α | Α | | | | | | | |



| | | | | Del | ay (Seconds) | | | LOS | | V/C | | | 95% Queue | e Length | |
|------|---------------------------------------------------------|----------|-------|----------|------------------------|-----------------|-------|----------|-------|----------|------------------|-------|-----------|------------------------|-----------------|
| Node | Intersection | Movement | Build | No-Build | Difference Absolute | Difference % | Build | No-Build | Build | No-Build | Storage Space | Build | No-Build | Difference Absolute | Difference % |
| | | EBL | 21.8 | 17.9 | 3.9 | 21.8% | С | В | 0.53 | 0.42 | 148 | 104 | 84 | 20 | 23.8% |
| | | EBT | 15.3 | 14.7 | 0.6 | 4.1% | В | В | 0.46 | 0.42 | 293 | 179 | 161 | 18 | 11.2% |
| 12 | Main Street at | WBT | 15.0 | 14.2 | 0.8 | 5.6% | В | В | 0.52 | 0.47 | 497 | 212 | 187 | 25 | 13.4% |
| 12 | Roxboro Street ¹ | WBR | 2.5 | 2.5 | 0.0 | 0.0% | Α | Α | 0.19 | 0.21 | 108 | 27 | 28 | -1 | -3.6% |
| | | NBLTR | 45.6 | 35.7 | 9.9 | 27.7% | D | D | 1.01 | 0.97 | 386 | 538 | 504 | 34 | 6.7% |
| | | Overall | 32.6 | 26.5 | 6.1 | 23.0% | С | С | | | | | | | |
| | | EBL | 70.3 | 66.2 | 4.1 | 6.2% | Е | E | 0.92 | 0.87 | 345 | 169 | 143 | 26 | 18.2% |
| | | EBT | 21.9 | 24.0 | -2.1 | -8.8% | С | С | 0.37 | 0.44 | 564 | 105 | 115 | -10 | -8.7% |
| 13 | Dillard Street at | WBTR | 28.9 | 30.5 | -1.6 | -5.2% | С | С | 0.67 | 0.70 | 826 | 182 | 177 | 5 | 2.8% |
| 15 | Roxboro Street ¹ | NBLT | 7.5 | 6.6 | 0.9 | 13.6% | Α | Α | 0.64 | 0.56 | 465 | 131 | 114 | 17 | 14.9% |
| | | NBR | 0.7 | 0.6 | 0.1 | 16.7% | Α | Α | 0.10 | 0.13 | 307 | 0 | 2 | -2 | -100.0% |
| | | Overall | 15.3 | 14.7 | 0.6 | 4.1% | В | В | | | | | | | |
| | | WBT | 7.9 | 8.7 | -0.8 | -9.2% | Α | А | 0.31 | 0.32 | 1342 | 82 | 82 | 0 | 0.0% |
| | | WBR | 21.7 | 19.7 | 2.0 | 10.2% | С | В | 0.83 | 0.79 | 1342 | 351 | 288 | 63 | 21.9% |
| 14 | Jackie Robinson Drive at Roxboro Street ¹ | NBL | 3.8 | 3.6 | 0.2 | 5.6% | Α | Α | 0.32 | 0.33 | 265 | 45 | 47 | -2 | -4.3% |
| | at Noxboro Street | NBT | 20.3 | 18.9 | 1.4 | 7.4% | С | В | 0.61 | 0.56 | 265 | 200 | 195 | 5 | 2.6% |
| | | Overall | 16.3 | 15.1 | 1.2 | 7.9% | В | В | | | | | | | |
| | | EBLTR | 6.4 | 5.9 | 0.5 | 8.5% | Α | А | 0.43 | 0.36 | 916 | 114 | 94 | 20 | 21.3% |
| | | WBLTR | 6.3 | 6.2 | 0.1 | 1.6% | Α | А | 0.36 | 0.35 | 715 | 96 | 93 | 3 | 3.2% |
| 45 | Dillard Street at | NBL | 22.8 | 18.3 | 4.5 | 24.6% | С | В | 0.62 | 0.47 | 485 | 142 | 101 | 41 | 40.6% |
| 15 | Holloway Street ¹ | NBTR | 6.8 | 7.1 | -0.3 | -4.2% | Α | А | 0.13 | 0.19 | 485 | 34 | 41 | -7 | -17.1% |
| | | SBLTR | 12.5 | 13.2 | -0.7 | -5.3% | В | В | 0.10 | 0.11 | 310 | 32 | 33 | -1 | -3.0% |
| | | Overall | 10.2 | 8.7 | 1.5 | 17.2% | В | А | | | | | | | |
| | | NBTR | 13.7 | 11.9 | 1.8 | 15.1% | В | В | 0.17 | 0.15 | 384 | 40 | 35 | 5 | 14.3% |
| | | SBLT | 8.8 | 9.1 | -0.3 | -3.3% | Α | А | 0.15 | 0.11 | 486 | 24 | 22 | 2 | 9.1% |
| | | EBL | 7.2 | 7.7 | -0.5 | -6.5% | Α | А | 0.08 | 0.15 | 378 | 30 | 49 | -19 | -38.8% |
| 1.0 | Dillard Street at | EBT | 8.7 | 9.1 | -0.4 | -4.4% | Α | А | 0.29 | 0.33 | 378 | 92 | 106 | -14 | -13.2% |
| 16 | Liberty Street ¹ | EBR | 2.0 | 2.3 | -0.3 | -13.0% | Α | А | 0.18 | 0.10 | 378 | 22 | 16 | 6 | 37.5% |
| | | WBL | 7.6 | 7.8 | -0.2 | -2.6% | Α | А | 0.10 | 0.12 | 397 | 23 | 25 | -2 | -8.0% |
| | | WBR | 2.4 | 2.5 | -0.1 | -4.0% | Α | А | 0.08 | 0.06 | 397 | 14 | 12 | 2 | 16.7% |
| | | Overall | 8.2 | 8.5 | -0.3 | -3.5% | Α | Α | | | | | | | |



| Node | Intersection | Movement | Delay (Seconds) | | | | LOS | | V/C | | 95% Queue Length | | | | |
|------|-----------------------------------------------|----------|-----------------|----------|------------|------------|-------|----------|-------|----------|------------------|-------|----------|------------|------------|
| | | | Build | No-Build | Difference | Difference | Build | No-Build | Build | No-Build | Storage Space | Build | No-Build | Difference | Difference |
| | | | | | Absolute | % | | | | | | | | Absolute | % |
| 17 | Dillard Street at Main Street ² | EBL | 11.7 | 11.3 | 0.4 | 3.5% | В | В | 0.14 | 0.10 | 100 | 28 | 21 | 7 | 33.3% |
| | | EBT | 14.1 | 14.2 | -0.1 | -0.7% | В | В | 0.44 | 0.45 | 365 | 147 | 150 | -3 | -2.0% |
| | | EBR | 3.7 | 2.6 | 1.1 | 42.3% | Α | Α | 0.08 | 0.05 | 100 | 16 | 11 | 5 | 45.5% |
| | | WBL | 10.7 | 10.8 | -0.1 | -0.9% | В | В | 0.06 | 0.07 | 555 | 15 | 17 | -2 | -11.8% |
| | | WBTR | 13.4 | 13.9 | -0.5 | -3.6% | В | В | 0.46 | 0.49 | 555 | 144 | 156 | -12 | -7.7% |
| | | NBL | 10.8 | 9.6 | 1.2 | 12.5% | В | А | 0.29 | 0.21 | 147 | 61 | 48 | 13 | 27.1% |
| | | NBTR | 7.6 | 6.6 | 1.0 | 15.2% | Α | Α | 0.26 | 0.22 | 396 | 69 | 56 | 13 | 23.2% |
| | | SBL | 8.0 | 8.5 | -0.5 | -5.9% | Α | А | 0.32 | 0.33 | 385 | 66 | 74 | -8 | -10.8% |
| | | SBTR | 2.8 | 2.8 | 0.0 | 0.0% | Α | А | 0.28 | 0.21 | 385 | 18 | 21 | -3 | -14.3% |
| | | Overall | 9.9 | 10.3 | -0.4 | -3.9% | Α | В | | | | | | | |

^{1 -} NCDOT Traffic Impact Criteria is applied

2 - City of Durham Traffic Impact Criteria is applied

Indicates Traffic Impact
Indicates Traffic Impact below Mid-D

Build Max Queue length exceeds No-Build and Storage Space by more than 10 feet



7.1 Analysis of LOS Thresholds in Primary Study Area

Each of the two 2040 Build LRT Options were compared to the respective No-Build scenario at each intersection by overall and individual movement levels. While the LRT is at-grade between Case Street and east of Swift Avenue for Build Option 1 and the LRT is elevated in this section for Build LRT Option 2, both options have a consistent LRT alignment and roadway configuration east of Buchanan Boulevard. Therefore, any MOE differences between the two build options at locations east of Buchanan Boulevard would be due to the change in the LRV travel times. Under LRT Option 2, the LRV would operate at a higher speed along the elevated track section near Swift Avenue, which would cause the train to arrive at the various at-grade intersections at different phases compared to Option 1. As the train generally maintains a consistent travel time, the signal preemption events would occur during the same signal phase at intersections using fixed time signal operations. For the purposes of the traffic impact analysis, the worst LOS, highest delay, and longest maximum queue length among both build options has been selected for discussion below.

The following section discusses the intersections where LRT impacts have been identified. The identified impacts are discussed below in regards to the NCDOT thresholds.

7.1.1 Main Street at 9th Street

The NCDOT traffic impact criteria are applied to the intersection of Main Street and 9th Street as Main Street is under NCDOT jurisdiction. The two Build LRT Options report different delays, LOS, and queue lengths at this intersection. For the 2040 LRT At-Grade Swift Avenue Option 1, the overall intersection delay at Main Street and 9th Street exceeds the NCDOT thresholds in the PM peak hour by experiencing LOS degradation. The 2040 LRT Elevated Swift Avenue Option 2 reports that the overall intersection delays meet NCDOT criteria in both AM and PM peak hours. Similarly, all of the individual intersection movements are expected to meet the NCDOT thresholds in the AM peak hour for both LRT options; however, in the PM peak hour LRT Option 1 reports multiple movements that exceed NCDOT LOS thresholds while Option 2 does not report any movements that would exceed LOS or delay impact criteria.

In the PM peak hour, LRT Option 1 reports that five individual movements are expected to operate with degraded LOS of middle D or worse including the eastbound Main Street right turn, the eastbound Main Street through movement, the southbound 9^{th} Street left turn, the southbound 9^{th} Street right turn, and the southbound 9^{th} Street through movement.

For the 2040 LRT At-Grade Swift Avenue Option 1, the maximum queue length for the following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Northbound 9th Street left turn exceeds storage space by 131 feet in AM and 149 feet in PM
- Northbound 9th Street right turn exceeds the shared through/right lane storage space by 107 feet in AM and 125 feet in PM
- Northbound 9th Street through movement exceeds the shared through/right lane storage space by 131 AM and 149 feet in PM
- Southbound 9th Street left turn exceeds storage space by 184 feet in AM and 279 feet in PM



- Southbound 9th Street right turn exceeds the shared through/right lane storage space by 154 in AM and 250 feet in PM
- Southbound 9th Street through movement exceeds the shared through/right lane storage space by 184 feet in AM and 279 feet in PM
- Westbound Main Street left turn exceeds storage space by 36 feet in AM
- Westbound Main Street right turn exceeds the shared through/right lane storage space by 65 feet in AM only
- Westbound Main Street through movement exceeds the shared through/right lane storage space by 87 feet in AM only

Under the LRT At-Grade Swift Avenue Option 1, the southbound 9th Street approach would be impacted due to the traffic detoured from the closed section of Pettigrew Street. Due to significant right-of-way constraints including the NCRR corridor to the south, there are no practical geometric mitigations that could resolve the movement delay and maximum queue impacts for Option 1.

For the 2040 LRT Elevated Swift Avenue Option 2, there are no queue impacts at the intersection of Main Street and 9th Street in the AM and PM peak hours.

7.1.2 Main Street at Iredell Street

The NCDOT traffic impact criteria are applied to the intersection of Main Street and Iredell Street, as Main Street is under NCDOT jurisdiction. For both 2040 Build LRT Options, the overall intersection delays at Main Street and Iredell Street meet the NCDOT thresholds in both AM and PM peak hours. All movements are expected to meet the NCDOT thresholds as well in both LRT options and peak hours.

The two Build LRT Options report different delays, LOS, and queue lengths at this intersection.

For the 2040 LRT At-Grade Swift Avenue Option 1, the maximum queue length for the following movements will exceed both their available storage space and their AM peak hour No-Build maximum queue length by more than 10 feet:

- Eastbound Main Street left turn exceeds storage space by 108 feet in AM
- Westbound Main Street right turn exceeds the shared through/right lane storage space by 26 feet in AM
- Westbound Main Street through movement exceeds the shared through/right lane storage space by 26 feet in AM

In AM peak hour under Option 1, the maximum queues along the eastbound and westbound movements would increase due to the diverted traffic from the Pettigrew Street closure between Case Street and Swift Avenue. The average queues are within the available storage space, except for the westbound Main Street left turn. Due to significant right-of-way constraints including the NCRR corridor to the south, there are no practical geometric mitigations that could resolve the movement delay and maximum queue impacts for Option 1.

For the LRT Option 2, Pettigrew Street is open between Case Street and east of Swift Avenue, and therefore all movements' maximum queues are expected to meet the NCDOT thresholds in both AM and PM peak hours.



7.1.3 Main Street at Broad Street

The NCDOT traffic impact criteria are applied to the intersection of Main Street and Broad Street, as Main Street is under NCDOT jurisdiction. For both 2040 LRT Options, the overall intersection delays at Main Street and Broad Street meet the NCDOT thresholds in both AM and PM peak hours.

The two Build LRT Options report different delays, LOS, and queue lengths at this intersection. Under the LRT At-Grade Swift Avenue Option 1, several individual movements are expected to operate with degraded LOS of middle D or worse including the eastbound Main Street left turn in the AM and PM peak hours, the westbound Main Street left turn in the AM and PM peak hours, the westbound Main Street right turn in the AM peak hour only, and the westbound Main Street through movement in the AM and PM peak hours. For Option 2, the following movements reported a degraded LOS: the eastbound Main Street left turn during the AM peak hour only and the northbound Broad Street left turn in the PM peak hour only.

In the AM peak hour under Option 1, the delays for the eastbound left and westbound left and through movements would increase due to the detoured traffic from a closed Pettigrew Street between Case Street and east of Swift Avenue. In the PM peak hour under Option 1, the delay has increased for eastbound and westbound Main Street left turns due to the same traffic diversions expected in the AM.

In the AM peak hour under Option 2, although the eastbound Main Street left turn LOS degrades, this movement's volume is forecasted to be less than 15 vehicles per hour. During the PM peak hour under Option 2, the northbound Broad Street left turn movement would experience an LOS degradation as a result of signal timing changes that were made to favor the east/west coordination of streets along the LRT project, which has an east/west alignment in Downtown Durham. The signal offset or phase times could potentially be modified to alleviate the northbound left movement degradation, however, these changes would potentially cause more significant impacts to the adjacent intersections. Overall, this intersection operates slightly better under Option 2 when compared to the No-Build PM due to signal timing modifications.

For the 2040 LRT At-Grade Swift Avenue Option 1, the maximum queue length for the following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Westbound Main Street left turn exceeds storage space by 265 feet in AM and by 264 feet in PM
- Westbound Main Street right turn exceeds the shared through/right lane storage space by 16 feet in AM
- Westbound Main Street through movement exceeds the shared through/right lane storage space by 97 feet in AM

Under the 2040 LRT Elevated Swift Avenue Option 2, only the northbound Broad Street right turn would experience a maximum queue length that would exceed the storage space and No-Build maximum queue space, with a maximum queue in excess of the available storage space by 42 feet in the AM peak hour only. However, this maximum queue is considered a very rare occurrence as the average queue for this movement is only 2 feet. For the LRT Option 2, Pettigrew Street is open between Case Street and east of Swift Avenue, and therefore the majority of vehicular movements are expected to meet the NCDOT thresholds in both AM and PM peak hours.



7.1.4 Pettigrew Street at 9th Street

The NCDOT traffic impact criteria are applied to the unsignalized intersection of Pettigrew Street and 9th Street, as this section of 9th Street is under NCDOT jurisdiction. For both 2040 LRT Build Options, the overall intersection delays at Pettigrew Street and 9th Street meet the NCDOT thresholds in the AM peak hour. However, under the PM peak hour in Option 1, the overall intersection experiences an increase in delay greater than 25% thereby exceeding NCDOT criteria. During the PM peak hour, Option 2 meets the NCDOT criteria for overall intersection delay.

The two Build LRT Options report different delays, LOS, and queue lengths at this intersection. Under the LRT At-Grade Swift Avenue Option 1, two individual movements are expected to operate with degraded LOS of middle D or worse including the westbound Pettigrew Street left turn in the PM peak hour and the westbound Pettigrew Street right turn in the PM peak hour. For Option 2, all movements meet the NCDOT delay and LOS criteria for both AM and PM peak hours.

For the 2040 LRT At-Grade Swift Avenue Option 1, the maximum queue length for the following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Westbound Pettigrew Street left turn exceeds the shared left/right turn lane storage space by 138 feet in PM
- Westbound Main Street right turn exceeds the shared left/right lane storage space by 138 feet in PM

In PM peak hour under Option 1, both delays and the maximum queues are expected to increase beyond NCDOT thresholds for the westbound approach due to the detoured traffic. These westbound movements have relatively low forecast volumes with 87 vehicles per hour expected for the westbound Pettigrew Street left turn and only 15 vehicles per hour expected for the westbound right turn. Due to significant right-of-way constraints including the NCRR corridor to the north, there are no practical geometric mitigations that could resolve the movement delay and maximum queue impacts for Option 1.This location is also physically constrained by the NCRR bridge over Erwin Road/9th Street.

For the 2040 LRT Elevated Swift Avenue Option 2, there are no maximum queue length impacts expected at any movement.

7.1.5 Pettigrew Street at Swift Avenue

The NCDOT traffic impact criteria are applied to the unsignalized intersection of Pettigrew Street and Swift Avenue, as this section of Swift Avenue is under NCDOT jurisdiction. In 2040 LRT Option 1, due to the closure of Pettigrew Street between Case Street and east of Swift Avenue, only the northbound and southbound Swift Avenue through movements are allowed. The LRT crossing at Swift Avenue would be controlled by gates. For LRT Option 2, the LRT is elevated and the intersection would remain the same as the No-Build Conditions.

For 2040 LRT At-Grade Swift Avenue Option 1, the overall intersection delay at Pettigrew Street and Swift Avenue exceeds the NCDOT thresholds in the AM peak hour. The additional delay experienced is partially caused by the LRT crossing, and added congestion at the intersection of Main Street and Broad Street to the north caused by the detoured traffic from the Pettigrew Street closure.



The 2040 LRT Option 2 meets the NCDOT criteria for overall intersection and all individual movement delays in both AM and PM peak hours.

In 2040 LRT Option 1 during the AM peak hour, the Vissim model indicates the northbound through movement will degrade LOS.

For the 2040 LRT At-Grade Swift Avenue Option 1, the maximum queue length for the following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Northbound Swift Avenue through movement exceeds storage space by 408 feet in AM
- Southbound Swift Avenue through movement exceeds storage space by 64 feet in AM

The queuing and delays experienced in Option 1 are primarily due to the increased congestion at the intersection of Main Street and Broad Street to the north. Due to the right-of-way constraints and adjacent NCRR corridor, there are no practical mitigations to reduce delays and queues for the northbound and southbound Swift Avenue approaches.

In Build Option 2 due to elevated LRT tracks, there are no traffic impacts in either peak hour.

7.1.6 Main Street at Buchanan Boulevard

The NCDOT traffic impact criteria are applied to the intersection of Main Street and Buchanan Boulevard, as Main Street is under NCDOT jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. For both 2040 LRT Options, the overall intersection delays at Main Street and Buchanan Boulevard meet the NCDOT thresholds in both AM and PM peak. None of the movements experience delay or LOS impacts in either LRT Option.

For both 2040 LRT Options during the AM and PM peak hours, the southbound Buchanan Boulevard right turn maximum queue exceeds the available storage space. For both Build Options, the maximum queue length exceeds the right turn bay storage space by 60 feet in the AM and 161 feet in the PM peak hour, but the maximum queue is contained within the southbound approach and would not reach the upstream intersection. Additionally, average queue lengths are well below the available storage length for both peak hours under both options with an average length of 5 feet in the AM and 9 feet in the PM peak hour. The Build Options' maximum queue exceeds the respective No-Build movement by only 14 feet in the AM and 36 feet in the PM peak hour

7.1.7 Memorial Street at Duke Street

The NCDOT traffic impact criteria are applied to the intersection of Memorial Street and Duke Street, as Duke Street is under NCDOT jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. For both 2040 LRT options, there are no overall intersection or movement delay impacts at Memorial Street and Duke Street.

For both 2040 LRT options, the maximum queue length for the following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:



- Eastbound Memorial Street left turn exceeds the storage space by 31 feet in PM only
- Northbound Duke Street left turn exceeds storage space by 54 feet in AM only
- Northbound Duke Street through movement to the northbound left turn bay at Peabody Street exceeds storage space by 96 feet in AM peak and 130 feet in PM
- Northbound Duke Street through movement exceeds storage space by 148 feet in AM peak and 188 feet in PM

The average queue lengths for the movements above are all expected to be 30 feet or less, which are well below the available storage length for both peak hours in both Build options. There are no practical mitigations due to right-of-way constraints and proximity of the adjacent signalized intersections.

7.1.8 Chapel Hill Street at Duke Street

The NCDOT traffic impact criteria are applied to the intersection of Chapel Hill Street and Duke Street, as both roadways are under NCDOT jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. For both 2040 LRT options, there are no overall intersection or movement delay impacts at Chapel Hill Street and Duke Street.

For both 2040 LRT options, the maximum queue lengths are generally consistent between alternatives. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Eastbound Chapel Hill Street left turn exceeds the left turn bay storage space by 106 feet for in AM only, however, the movement maximum queue length will be contained by the eastbound approach
- Northbound Duke Street left turn exceeds the shared left/through lane storage space by 127 feet in PM only
- Northbound Duke Street right turn exceeds storage space by 108 feet in PM only
- Northbound Duke Street through movement exceeds the shared left/through lane storage space by 127 feet in PM only
- Westbound Chapel Hill Street right turn exceeds the shared through/right turn lane storage space by 103 feet in AM only
- Westbound Chapel Hill Street through movement exceeds the shared through/right turn lane storage space by 133 feet in AM only

The maximum queue length events are considered to occur infrequently and the average queue lengths are well below the available storage length for both peak hours in both scenarios, and there are no practical mitigations due to right-of-way constraints and proximity of the adjacent signalized intersections.

7.1.9 Chapel Hill Street at Willard Street

The NCDOT traffic impact criteria are applied to the intersection of Chapel Hill Street and Willard Street, as Chapel Hill Street is under NCDOT jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. For both 2040 LRT Options, the overall intersection delays at Chapel Hill Street and Willard Street meet the NCDOT thresholds in both the AM and PM peak hours.



Under both LRT Options, several movements are expected to operate with degraded LOS of middle D or worse including the northbound Willard Street left turn in the PM peak hour and the northbound Willard Street right turn in the PM peak hour.

For both 2040 LRT Options, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Eastbound Chapel Hill Street right turn exceeds the shared through/right lane storage space by 65 feet in AM and by 29 feet in PM
- Eastbound Chapel Hill Street through movement exceeds the shared through/right lane storage space by 65 feet in AM and 29 feet in PM

For both 2040 Build Options during the AM peak hour, the eastbound maximum queue length would extend longer than the available storage space. However the average queue lengths are well below the storage length.

7.1.10 Pettigrew Street at Chapel Hill Street

The NCDOT traffic impact criteria are applied to the intersection of Pettigrew Street and Chapel Hill Street, as Chapel Hill Street is under NCDOT jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. For both 2040 LRT Options, the overall intersection delays at Pettigrew Street and Chapel Hill Street meet the NCDOT thresholds in both the AM and PM peak hours. Under both LRT options, Pettigrew Street would be converted to one-way eastbound operation for vehicular traffic between Chapel Hill Street and Dillard Street. Although the removal of the westbound Pettigrew Street approach would eliminate vehicular conflicts with the north and southbound Chapel Hill Street movements, the traffic signal will be maintained to provide for the safe crossing of pedestrians across Chapel Hill Street.

For both LRT options in both peak hours, the overall intersection and all movement delays and LOS at Pettigrew Street and Chapel Hill Street meet the NCDOT thresholds.

For both 2040 LRT scenarios, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Eastbound Chapel Hill Street right turn exceeds the shared through/right lane storage space by 78 feet in AM and 72 feet in PM
- Eastbound Chapel Hill Street through movement exceeds the shared through/right lane storage space by 95 feet in AM and 89 feet in PM
- Westbound Chapel Hill Street left turn exceeds storage space by 70 feet in AM and 78 feet in PM
- Westbound Chapel Hill Street through movement exceeds storage space by 17 feet in AM and 25 feet in PM

The maximum queue lengths along eastbound and westbound Chapel Hill Street approaches have increased due to detoured westbound traffic from Pettigrew Street. However, the average queues are well below the available storage lengths for these affected movements.



7.1.11 Pettigrew Street at Blackwell Street

The City of Durham traffic impact criteria are applied to the intersection of Pettigrew Street and Blackwell Street, as both roadways are under city jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. Under both LRT options, Pettigrew Street would be converted to one-way eastbound operation for vehicular traffic between Chapel Hill Street and Dillard Street. For both 2040 LRT options, the LRT crosses Blackwell Street at the north side of the intersection of Pettigrew Street and Blackwell Street.

For both 2040 LRT Options, the overall intersection and individual movement delays at Pettigrew Street and Blackwell Street meet the City of Durham thresholds in both the AM and PM peak hours.

For both 2040 LRT Options, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Eastbound Pettigrew Street left turn exceeds the shared left/through/right lane storage space by 103 feet in AM and 113 feet in PM for both Options
- Southbound Blackwell Street left turn exceeds storage space by 66 feet in PM only
- Southbound Blackwell Street through movement exceeds storage space by 66 feet in PM only

The maximum queue lengths at this intersection are primarily due to the LRT signal preemption events. However, the average queue lengths are well below the storage length. The LRT crossing of Blackwell Street does not cause significant impacts to this intersection.

7.1.12 Main Street at Corcoran Street

The City of Durham traffic impact criteria are applied to the intersection of Main Street and Corcoran Street, as both roadways are under city jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. Under both LRT options, Pettigrew Street would be converted to one-way eastbound operation for vehicular traffic between Chapel Hill Street and Dillard Street. For both 2040 LRT options, the LRT crosses Blackwell Street at the north side of the intersection of Pettigrew Street and Blackwell Street, which is located to the south of Main Street and Corcoran Street.

For both 2040 LRT options, the overall intersection and individual movement delays at Main Street and Corcoran Street meet the City of Durham thresholds in both the AM and PM peak hours.

For both 2040 LRT options, the maximum queue lengths are generally consistent between options. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Eastbound Main Street left turn exceeds the shared left/through/right lane storage space by 167 feet in AM only
- Eastbound Main Street right turn exceeds the shared left/through/right lane storage space by 151 feet in AM only
- Eastbound Main Street through movement exceeds the shared left/through/right lane storage space by 167 feet in AM only



The increased maximum queue lengths at this intersection are primarily due to the LRT signal preemption events occurring two intersections to the south at Pettigrew Street. However, the average queue lengths are well below the available storage length. Additionally, the Build maximum queues are expected to be slightly longer than the No-Build maximum queue length by 24 feet for all three of the impacted eastbound Main Street movements.

7.1.13 Main Street at Mangum Street

The NCDOT traffic impact criteria are applied to the intersection of Main Street and Mangum Street, as Mangum Street is under NCDOT jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. For both 2040 LRT Options, the overall intersection delay at Main Street and Mangum Street exceeds the NCDOT thresholds in the PM peak hour by experiencing degradation of LOS. The LRV travel times have an impact at this intersection due to the poor operations expected in the No-Build PM peak hour. Therefore, due to alignment differences at Swift Avenue there are MOE variations between Build Option 1 and Build Option 2.

Under the LRT At-Grade Swift Avenue Option 1, several individual movements are expected to operate with degraded LOS of middle D or worse including the eastbound Main Street through movement in the AM peak hour, the southbound Mangum Street left turn in the PM peak hour, the southbound Mangum Street through movement in the PM peak hour, and the westbound Main Street through movement in the PM peak hour. For Option 1, the eastbound Main Street right turn movement will maintain its LOS but experiences an increase in delay greater than 25% thereby exceeding NCDOT criteria.

For Build Option 2, the following movements are expected to operate with a degraded LOS of middle D or worse: the eastbound Main Street right turn in the AM peak hour only, the southbound Mangum Street left turn in the PM peak hour only, and the southbound Mangum Street through movement in the PM peak hour only.

For both 2040 LRT options, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Eastbound Main Street right turn exceeds the shared through/right lane storage space by 65 feet in AM and by 79 feet in PM
- Eastbound Main Street through movement exceeds the shared through/right lane storage space by 83 feet in AM and by 97 feet in PM
- Southbound Mangum Street left turn exceeds the shared left/through lane storage space by 367 feet in AM and 374 feet in PM
- Southbound Mangum Street right turn exceeds the storage space by 348 feet in AM and 355 feet in PM
- Southbound Mangum Street right turn exceeds the shared left/through storage space by 367 feet in AM and by 374 feet in PM

The maximum queue lengths along eastbound Main Street and Southbound Chapel Hill Street approaches would increase due to detoured westbound traffic from Pettigrew Street and LRT signal preemption activities occurring to the south. The average queue lengths for the eastbound Main Street are contained within the available storage space; however, the southbound average queues will also exceed the storage



space and extend beyond the upstream signalized intersection of Parrish Street and Mangum Street. Compared to the No-Build PM, the Build PM maximum queue lengths are only 30 feet longer. Due to right-of-way constraints and the close proximity of adjacent signalized intersections, the only practical mitigation would require the removal of parking along the western curbface of Mangum Street between Parrish Street and Ramseur Street to provide a third southbound through lane. With approval from the City of Durham, this mitigation can be analyzed during the Engineering phase of the project.

7.1.14 Pettigrew Street at Magnum Street

The NCDOT traffic impact criteria are applied to the intersection of Pettigrew Street and Mangum Street, as Mangum Street is under NCDOT jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. Under both LRT options, Pettigrew Street would be converted to one-way eastbound operation for vehicular traffic between Chapel Hill Street and Dillard Street. For both 2040 Build Conditions, the LRT crosses Magnum Street at the north side of the intersection with Pettigrew Street.

For both 2040 LRT options during both peak hours, the overall intersection delays and all vehicular movements meet the NCDOT thresholds in both AM and PM peak hours.

For both 2040 LRT options, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Southbound Mangum Street left turn exceeds the shared left/through lane storage space by 22 feet in AM and by 44 feet in PM
- Southbound Mangum Street through movement exceeds the shared left/through lane storage space by 22 feet in AM and by 44 feet in PM

For both 2040 LRT options during both peak hours, the maximum queue length along southbound approach would be increased due to the extra delay caused by the LRT signal preemption events. However, the average queue length is well below the storage length. The overall intersection operates at LOS A in both peak hours under both LRT Alternatives due to the reduced conflicts from the westbound Pettigrew Street closure.

7.1.15 Pettigrew Street at Dillard Street

The City of Durham traffic impact criteria are applied to the intersection of Pettigrew Street and Dillard Street, as both roadways are under city jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. Under both LRT options, Pettigrew Street would be converted to one-way eastbound operation for vehicular traffic between Chapel Hill Street and Dillard Street. For both 2040 LRT options, the LRT crosses Dillard Street at the north side of the intersection with Pettigrew Street.

For both 2040 LRT options, the overall intersection and all vehicular movements meet the City of Durham LOS thresholds in both AM and PM peak hours.

For both 2040 LRT options, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:



- Eastbound Pettigrew Street left turn exceeds storage space by 62 feet in PM only
- Southbound Dillard Street left turn exceeds storage space by 28 feet in PM only
- Southbound Dillard Street through movement exceeds storage space 28 feet in PM only

In the PM peak hour, the maximum queue length along the southbound Dillard Street approach would be increased due to the extra delay caused by the LRT crossing. However the average queue lengths are well below the storage length. The eastbound Pettigrew Street left turn maximum queue would be contained within the eastbound approach storage space and would not spill back to the upstream intersection.

7.1.16 Pettigrew Street at Fayetteville Street

The NCDOT traffic impact criteria are applied to the intersection of Pettigrew Street and Fayetteville Street, as Fayetteville Street is under NCDOT jurisdiction. Under both LRT options, Pettigrew Street would be converted to one-way eastbound operation for vehicular traffic between Chapel Hill Street and Dillard Street. For both 2040 Build Options, the LRT crosses Fayetteville Street at the north side of the intersection with Pettigrew Street. For both 2040 LRT options during both peak hours, the overall intersection delays meet the NCDOT thresholds in both AM and PM peak hours.

Under the LRT Option 1, the southbound Fayetteville left turn, through movement and right turn all experience degradation of LOS in the PM peak hour. For Option 1, the eastbound Pettigrew Street left turn would also experience an increase in delay greater than 25%; however, this movement's demand is only 5 vehicles per hour.

For LRT Option 2, the southbound Fayetteville left turn and right turn would experience degradation of LOS in the PM peak hour.

For both 2040 LRT Options, the maximum queue length for the following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Northbound Fayetteville Street left turn exceeds storage space by 68 feet in PM only
- Northbound Fayetteville Street right turn exceeds the shared through/right storage space by 63 feet in PM only
- Northbound Fayetteville Street through movement exceeds the shared through/right storage space by 68 feet in PM only
- Southbound Fayetteville Street left turn exceeds storage space by 159 feet in the PM only; however the maximum queue would be contained by the southbound approach
- Westbound Pettigrew Street left turn exceeds storage space by 114 feet in AM; however, the maximum queue length would be contained by the eastbound approach

The eastbound Pettigrew Street left turn and southbound Fayetteville Street right turn are impacted in the PM peak hour under Option 1 only, however, the volume for both of these movements are 5 and 2 vehicles per hour, respectively. During the PM peak hour for both LRT options, the maximum queue lengths would be increased on the northbound and southbound approaches. However the average queue lengths are well below the storage length.



7.1.17 Jackie Robinson Drive at Fayetteville Street

The NCDOT traffic impact criteria are applied to the intersection of Jackie Robinson Drive and Fayetteville Street, as both roadways are under NCDOT jurisdiction.

For both 2040 LRT options during both peak hours, the overall intersection delays and all vehicular movements meet the NCDOT thresholds in both AM and PM peak hours.

For both 2040 LRT options, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Northbound Fayetteville Street left turn exceeds storage space by 98 feet in PM only
- Northbound Fayetteville Street through movement exceeds storage space by 95 feet in PM only

In the PM peak hour, the maximum queue length along the northbound Fayetteville Street approach would be increased due to the extra delay caused by the LRT crossing to the north and the close proximity of signalized intersections. However the average queue lengths for these impacted movements are well below the storage length.

7.1.18 Morehead Avenue at Fayetteville Street

The NCDOT traffic impact criteria are applied to the intersection of Morehead Avenue and Fayetteville Street, as both roadways are under NCDOT jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. For both 2040 LRT options, the overall intersection delays and individual movements at Morehead Avenue and Fayetteville Street meet the NCDOT thresholds in both the AM and PM peak hours.

The maximum queue length for the southbound Fayetteville Street through movement is expected to exceed the available storage space by 85 feet in the PM peak hour only under both LRT options. However, the maximum queue events are infrequent, and the average queue length is well below the available storage space.

7.1.19 Pettigrew Street at Grant Street

The City of Durham traffic impact criteria are applied to the intersection of Pettigrew Street and Grant Street, as both roadways are under city jurisdiction. The alignment and roadway configurations for LRT At-Grade Swift Avenue Option 1 and LRT Elevated Swift Avenue Option 2 are consistent at this intersection. For both 2040 LRT options, the LRT crosses Grant Street at the north side of the intersection with Pettigrew Street.

For both 2040 LRT options, the overall intersection and individual movement delays meet the City of Durham thresholds in both AM and PM peak. The LRT crossing does not bring significant impacts to the intersection, as the overall intersection maintains LOS B in both future LRT options.

For both 2040 LRT options, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

 Southbound Grant Street left turn exceeds the shared left/through/right storage space by 50 feet in PM only



- Southbound Grant Street right turn exceeds the shared left/through/right storage space by 50 feet in PM only
- Southbound Grant Street through movement exceeds the shared left/through/right storage space by 50 feet in PM only
- Westbound Pettigrew Street left turn exceeds the storage space by 137 feet in PM only
- Westbound Pettigrew Street right turn exceeds the shared through/right lane storage space by 110 feet in the AM only
- Westbound Pettigrew Street through movement exceeds the shared through/ right lane storage space by 112 feet in the AM only

During the AM peak, the westbound maximum queue lengths would be increased due to volume increase along that approach. During the PM peak, the southbound maximum queue lengths would be extended due to the delays caused by the LRT crossing. However, for both approaches the average queues are well below the storage length.

7.1.20 Alston Avenue at Gann Street

The NCDOT traffic impact criteria are applied to the intersection of Alston Avenue and Gann Street, as Alston Avenue is under NCDOT jurisdiction.

For both 2040 LRT options during both peak hours, the overall intersection and all vehicular movement delays meet the NCDOT thresholds in both AM and PM peak hours.

For both 2040 LRT options, the maximum queue lengths are generally consistent. The following movements will exceed both their available storage space and their respective peak hour No-Build maximum queue length by more than 10 feet:

- Northbound Alston Avenue left turn exceeds the storage space by 114 feet in PM only
- Southbound Alston Avenue right turn exceeds storage space by 360 feet in PM only

During the PM peak hour for both LRT options, the maximum queue lengths would be increased on the northbound and southbound approaches. However, the average queue lengths are well below the storage lengths. Additionally, the northbound and southbound Alston Avenue left turns' maximum queue lengths would be contained by the northbound and southbound approaches storage space, respectively, which would avoid blocking of the upstream intersections.

7.2 Analysis of LOS Thresholds in Secondary Study Area

Based on the secondary study 2040 Synchro models, all intersections that lie outside of the primary LRT corridor that may be affected by the detoured westbound Pettigrew Street traffic are expected to operate at LOS E or better which meets the threshold set forth by the City of Durham. In addition, after optimizing the signal timing, the delays would be reduced at many intersections. Most overall intersections operate at delays of LOS C or better under the LRT options.

There are three lane groups that would experience minor traffic impacts. The only movement expected to experience an impact in delay would be the northbound Roxboro Street shared left/through/right lane at the intersection of Main Street and Roxboro Street during the PM peak hour. This lane group reports a Build condition increase in delay greater than 25% when compared to the No-Build, however, the resulting delay is barely over 45 seconds with an exact value of 45.6 seconds of delay in the PM peak hour.



The following lane groups 95% queue length will exceed both their available storage space and their respective peak hour No-Build 95% queue length by more than 10 feet:

- At the intersection of Chapel Hill Street/Main Street and Morris Street, the southbound Main Street shared left/through lane exceeds the storage space by 23 feet in the AM only
- At the intersection of Morgan Street and Rigsbee Avenue, the northbound Rigsbee Avenue shared left/through lane exceeds the storage space by 30 feet in the AM only
- At the intersection of Main Street and Roxboro Street, the northbound Roxboro Street shared left/through/right lane group by 34 feet in the PM only

The future build traffic impacts expected in the secondary study area do not represent a significant difference in operations from the No-Build conditions. The single lane group that would report a delay increase of 25% would still have a delay just barely over 45 seconds and would maintain the same LOS D in the No-Build scenario. For the three lane groups that would experience 95% queue lengths in excess of their storage space the corresponding No-Build 95% queue lengths, the excess queue length would be less than 35 feet.



8. Conclusions/Recommendations

When comparing the Build options to the No-Build Alternative, it was observed that although the LRT atgrade crossings may cause extra delay to the north/south aligned streets, generally the future roadway capacities are sufficient to accommodate the additional delays under the future LRT Build conditions. The additional LRT delays were also mitigated by the reduced number of conflicts at the intersections where Pettigrew Street would be converted to a one-way eastbound operation.

Under the 2040 LRT At-Grade Swift Avenue Option 1, traffic impacts were observed in the area bounded by Main Street, Pettigrew Street, 9th Street and Broad Street. As this subarea is composed of short blocks arranged in a grid network that would already experience significant congestion under No-Build Conditions, several movements would be impacted significantly in Option 1. These traffic impacts are due to the at-grade crossing of the LRT at Broad Street/Swift Avenue which causes additional delays to the north/south running streets. The closure of Pettigrew Street between Case Street and east of Swift Avenue requires traffic to be rerouted to these already congested roadways to reach their destinations. In Option 2, when the LRT is elevated and Pettigrew Street is open between Case Street and east of Swift Avenue, most of these impacts would be removed. At Main Street and Broad Street under Option 2, the northbound Broad Street left turn would experience a degradation of LOS from D to E due to network signal timing changes.

In the downtown area east of Swift Avenue for both Build Options, all intersections would operate in accordance with applicable level of service thresholds with the exception of the following locations:

- Mangum Street and Main Street would experience an overall LOS degradation in the PM peak hour by worsening from LOS D to E.
- Pettigrew Street & Fayetteville Street would meet the overall delay/LOS intersection criteria, however, two movements would experience degradation of LOS in the PM peak hour with the southbound Pettigrew Street left and through movements both worsening from LOS C to E.
- Chapel Hill Street &Willard Street, which is an unsignalized intersection, would meet the overall/delay LOS intersection criteria; however, the stop-controlled Willard Street approach would degrade from LOS E to LOS F in the PM peak hour.

All three intersections would experience LOS impacts due to LRV signal preemption events and the network signal timing changes aimed at providing better east/west progression for the LRT. Mangum Street and Main Street is expected to operate at a high LOS D in the No-Build PM peak hour, and with preemption events the overall delay increases to LOS E. If the loss of parking along Mangum Street is deemed acceptable, a third southbound Mangum Street travel lane could be tested during the Engineering phase of the project to determine if traffic impacts would be mitigated at Mangum Street and Main Street.

The LOS movement impacts at Pettigrew Street and Fayetteville cannot be practically mitigated with roadway modifications due to right-of-way constraints and the location of the NCRR corridor that crosses the southbound approach upstream of the stop bar.

Due to preemption events, there are fewer acceptable gaps for vehicles on the stop-controlled Willard Street approach at Chapel Hill Street. The signalization of Willard Street and Chapel Hill Street was



discussed with the City of Durham. However, due to the proximity of signals along Chapel Hill Street at Duke Street and Pettigrew Street, the city requested that the intersection remain stop-controlled.

Maximum queues would exceed available storage in several locations; however this is an infrequent occurrence and additional roadway modifications are not recommended at these locations due to the limited operational benefits that would require large capital expenditures via impractical right-of-way acquisitions and the reconstruction of bridges. Many of the turn bay maximum queues would also be contained within their overall approaches' storage space and therefore would not impact upstream intersections.

The expected average queues would be accommodated by the available storage at all locations except the southbound approach of Main Street at Mangum Street. The addition of a third southbound travel lane can be studied during the Engineering phase of the project if the City of Durham were to allow the existing parking lane to be rededicated as a travel lane.



D-O LRT: Downtown Durham Traffic Simulation Report Appendices